

TECHNICAL GUIDE







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TECHNICAL GUIDE

Thermal Conductivity

THERMAL CONDUCTIVITY OF PYROGEL XT ACCORDING TO ASTM C 177

Third-party validation of the thermal conductivity of Pyrogel XT was acquired at temperatures ranging from 0° – 650° C (32° – 1200° F) under a compressive load of 2 psi. The final report displaying the full thermal conductivity curve is shown in **Appendix A**.

Non-Combustibility and Fire Performance

ASTM E 84 – SURFACE BURNING CHARACTERISTICS

Pyrogel XT was tested in accordance with ASTM E 84, the Standard Test Method for Surface Burning Characteristics of Building Materials, and is given in **Appendix B**. Pyrogel XT exhibited no ignition during testing and thus satisfies the criteria for a Class A rating with a flame spread index: 0, smoke developed index: 5, and fuel contribution: 0.

ASTM E 1354 – STANDARD TEST METHOD FOR HEAT AND VISIBLE SMOKE RELEASE RATES FOR MATERIALS AND PRODUCTS USING AN OXYGEN CONSUMPTION CALORIMETER

Pyrogel XT was tested in accordance with ASTM E 1354 at an incident heat flux equivalent to a cellulosic fire (50 kW/m²). The testing was performed in triplicate with no signs of ignition for all samples, resulting in a total heat release of zero and effective heat of combustion of 730 J/q. These third-party test results can be found in **Appendix C**.

BS EN 13501-1:2007 - REACTION TO FIRE PERFORMANCE

The reaction to fire performance of Pyrogel XT was evaluated via **BS EN 13501-1:2007**. Pyrogel XT (5-10 mm) achieved a reaction to fire classification of A2-s1, d0 for construction applications and as a suspended ceiling membrane. **EN ISO 1716** and **EN 13823** were carried out as part of this testing, and all results were compliant for Class A2 classification. Third-party test results can be found in **Appendix L**. (Click bolded text to jump to specific section.)



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Non-Combustibility and Fire Performance

BSS 7239:88 – TEST METHOD FOR TOXIC GAS GENERATION BY MATERIALS ON COMBUSTION

Quantitative analysis of potential toxic combustion gases was determined for Pyrogel XT via Boeing Support Specification 7239. Specifically, representative production samples were exposed to flaming combustion conditions (25 kW/m²) as dictated by ASTM E 662. The levels of CO, HF, HCl, NO_{χ} , SO_{2} and HCN were determined via Drager colorimetric gas analyses. All of the gases were below the detection limits with the exception of CO and NO_{χ} , which exhibited levels of 100 and 5.0 ppm, respectively. While no specific pass/fail criteria exists for BSS 7239, the measured levels of CO and NO_{χ} are significantly below the accepted transportation industry standards of 3500 and 100 ppm, respectively. The third-party test results for BSS 7239 can be found in **Appendix E**.

ISO 1182:1990 – TEST FOR NON-COMBUSTIBILITY

The non-combustibility of Pyrogel XT was assessed via the methods outlined in ISO 1182. The mean duration of flaming, average specimen temperature and average furnace temperature for a representative sample of Pyrogel XT was 0 sec, 32°C and 27°C (90°F and 81°F), respectively. This performance meets the criteria for non-combustibility as set forth in the 1990 edition of ISO 1182 and is consistent with a Euroclass A2 Fire classification. Third-party ISO 1182 test results can be found in **Appendix D**.

UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL (Pyrogel XTF only)

Testing was conducted on Pyrogel XTF to evaluate its fire resistance. Testing was conducted in accordance with UL 1709-05 Standard for Rapid Rise Fire Tests of Protection Materials for Structural Steel. Results were as follows:

12 mm \longrightarrow 68 min 30 mm \longrightarrow 132 min 48 mm \longrightarrow 184 min 66 mm \longrightarrow >240 min

The third-party test results for UL 17090-05 can be found in **Appendix F**.





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Dimensional Stability

ASTM C 356 – LINEAR SHRINKAGE UNDER FULL THERMAL SOAK

The dimensional stability of Pyrogel XT at elevated temperatures was ascertained by testing according to the methods outlined in ASTM C 356. A linear shrinkage of 1.3% and a total mass loss of 1.1% was observed for Pyrogel XT after a 24-hour exposure at 650°C (1200°F). Third-party ASTM C 356 test results can be found in **Appendix H**.

ASTM C 411 – HOT SURFACE PERFORMANCE (FLAT PLATE CONFIGURATION)

The maximum use temperature of Pyrogel XT was confirmed by testing material according to ASTM C 411 in a flat plate configuration. Specifically, a 60 mm stack-up of Pyrogel XT was exposed to a hot surface at 650°C for a period of 96 hours. The maximum midpoint temperature of the stack-up was measured at 463°C with a cold face temperature of 65.6°C, indicating the absence of any unusual exothermic heat rise. After testing, Pyrogel XT retained structural integrity and exhibited no signs of warping, delamination, or cracking. Third-party test results for ASTM C 411 can be found in **Appendix H**.

ASTM C 411/C 447 – ESTIMATION OF MAXIMUM USE TEMPERATURE AND HOT SURFACE PERFORMANCE (PIPE CONFIGURATION)

The maximum use temperature of Pyrogel XT was assessed using the methods outlined in ASTM C 447 using material shrinkage and degradation in thermal performance during ASTM C 411 testing as the main criteria. Specifically, 60 mm of Pyrogel XT was installed on a 3.5" pipe and subjected to heating to 650°C (1200°F) for a period of 96 hours. The average percent shrinkage across the leading edge (i.e. hot face) was measured at 1.77%. Interply thermoucouples located between layers 2-3, 4-5, 6-7, 8-9, and 10-11 were stable throughout the test, indicating the absence of any exothermic heat rise. Third-party ASTM C 411/C 447 test results are found in **Appendix G**.





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Water Resistance/Permeability

ASTM C 1104 – WATER VAPOR SORPTION

The amount of water absorbed upon exposure to high humidity conditions was determined via the methods outlined in ASTM C 1104. Specifically, Pyrogel XT exhibits an average weight gain of 2.25% upon exposure to 95% RH at 49°C for 96 hours. Pyrogel XT exceeds the requirements for water vapor sorption as outlined in ASTM C 547, the Standard Specification for Mineral Fiber Pipe Insulation. Third party test results can be found in **Appendix I, Table 2**.

ASTM C 1511 – DETERMINATION OF WATER RETENTION

Water retention test results for Pyrogel XT are given in **Appendix I, Table 3**. The average weight gain for a $10'' \times 10''$ sample was 16.3 grams, which translates to a water uptake of 4.2 vol %. It was estimated that a significant majority of this water uptake was attributed to the presence of microscopic water droplets adhered to the surface of the insulation and not solely from bulk absorption. We have thus conducted testing using a modified ASTM C1511 procedure that includes the removal of these surface species via contact with saturated paper towel. The results of this testing indicated that the bulk water uptake of Pyrogel XT was consistently <0.5 vol %.

ASTM C 1559 – WATER WICKING

The propensity for Pyrogel XT to wick water was determined by the methods outlined in ASTM C 1559. Pyrogel XT is hydrophobic and exhibits no water wicking for the duration of the test (168 hours). Third-party test results are shown in **Appendix I, Table 5**.





(Bolded text linked) TECHNICAL GUIDE

Other

ASTM C 165 - COMPRESSIVE STRENGTH

The compressive resistance of Pyrogel XT was acquired according to the methods outlined in ASTM C 165. Specifically, the compressive resistance was determined at 10% and 25% strain for Pyrogel XT. The compressive stress at 10% and 25% strain for a single ply of Pyrogel XT was determined to be 102.9 kPa and 182.9 kPa, respectively. Similar results were obtained for a 5-ply specimen, which exhibited a compressive resistance of 103.1 kPa and 217.4 kPa at a 10% and 25% strain, respectively. Third party results are shown in **Appendix I, Table 4**.

ASTM C 592-04 – HEAT AND VIBRATION AGING

The heat and vibration aging characteristics of Pyrogel XT were tested via ASTM C592-04 (Section 11.11, Modified). The specimen was thermally soaked at 400°C for 96 hours and then vibrated horizontally for 6 hours (12 Hz, displacement of 3 mm peak to peak). Pyrogel XT showed a -0.19% mass change after vibration. Third-party test results can be found in **Appendix K**.

ASTM C 795 – CORROSION TEST

This report details the results of a 28-day corrosion test (ASTM C 692) and the pH and chemical testing of water extraction (ASTM C 871) of Pyrogel XT BLKT 1205 as determined by ASTM C 795, standard specification for thermal insulation for use in contact with austenitic stainless steel. Pyrogel XT BLKT 1205 met the chemical requirements of ASTM C 795, falling within the "Acceptable" range of the "Acceptability Curve." Third party results are shown in **Appendix J**.

ASTM D 5034 – TENSILE STRENGTH

The tensile strength of Pyrogel XT was determined for a single ply of 5 mm material according to the methods outlined in ASTM D 5034, Standard Test Method for Breaking Strength and Elongation of Textile Fabrics. The average tensile strength for Pyrogel XT was determined to be 490 N in the machine direction and 370 N in the cross-direction. Third-party test results can be found in **Appendix I, Table 6**.



TECHNICAL GUIDE

Appendix A ASTM C 177 – THERMAL CONDUCTIVITY



Report on the

THERMAL CONDUCTIVITY and THERMAL RESISTANCE of AEROGEL MAT

Prepared for:

Aspen Aerogels Inc. 30 Forbes Road Northborough, Massachusetts 01532

Prepared by:

NETZSCH Instruments, Inc. **Testing Services**

Report Number: 621001443

Work Performed Under Purchase Order Number: 306132

Submitted By:

Applications Laboratory Manager

May 2008



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Appendix A ASTM C 177 – THERMAL CONDUCTIVITY



May 2008

9

Report on the

Apparent Thermal Conductivity and Thermal Resistance of Aerogel Mat

NETZSCH Instruments was contracted by Aspen Aerogels to evaluate one aerogel mat insulation material for apparent thermal conductivity at nominal mean temperatures of 0, 50, 100, 200, 350, 500 and 600°C by the guarded hot plate method.

The material was identified as given in Table 1 and was submitted as a pair dimensioned approximately 305 mm square by 6 mm thickness. The samples were cut to 200 mm diameter for testing.

The specimens were positioned horizontally with heat flow up and down during the tests. The test results are given in Table 1 after a description of equipment and procedure.

Thermal Conductivity

Thermal conductivity is the material property that determines the amount of heat that will flow through an object when a temperature difference exits across the object. Thermal conductivity is a steady state property; it can only be directly measured under conditions in which the temperature distribution is not changing and all heat flows are steady. The fundamental equation that governs steady-state heat flow in a slab geometry is:

 $Q = (\lambda \times \Delta T \times A) / \Delta x \quad (1)$

where

Q = the rate of heat flow through the slab (W or Btu/h)

 λ = the thermal conductivity of the slab material (W/m K or Btu/h-ft-°F)

 ΔT = the temperature difference across the slab (°C or °F)

 $\Delta x =$ the thickness (m or ft)

A =the cross sectional area (m^2 or ft^2)

Reference: Report No. 621001443



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Appendix A ASTM C 177 – THERMAL CONDUCTIVITY



Materials that have low values of thermal conductivity allow only a small amount of heat flow and are called thermal insulators. Materials with large values of thermal conductivity allow more heat to flow across the slab with the same temperature difference. Thermal conductivity is a material property and does not depend upon the geometry of the sample. In general, thermal conductivity is a function of the mean sample temperature. The material comprising the slab is often a mixture of materials. It could be a layered composite or a material containing gas cells in which heat can be transferred by convection and radiation as well as by conductivity through the material. In these cases the parameter, λ , defined in Equation (1) is an "effective" or "apparent" thermal conductivity for the heterogeneous material.

Experimental Procedure for Testing by ASTM C 177-97

Testing was performed in accordance with ASTM C 177-97, Steady-State Heat Flux Measurements and Thermal Transmission Properties by Means of the Guarded Hot Plate Apparatus, utilizing a Holometrix Model TCFGM guarded hot plate instrument (SN GHP-3). A schematic diagram of the test facility is shown in Figure 1. Two samples sandwiched a heating unit, which consisted of a central metering section and an annular guard section. This composite stack was mounted between two cooling units and surrounded with an environmental heater unit, a fluid-cooled shroud, and edge insulation. The metering section of the heating unit consisted of a metering area heater and metering area surface plates, while the guard section was comprised of a single guard heater and guard surface plates. The cooling units consisted of a cooling plate, a cooling unit heater, and a cooling surface plate. All surface plates were fabricated of 10 mm (0.38 inch) thick steel, were smoothly finished to conform to a true plane to within 0.025 percent, and were treated to have a total hemispherical emittance of 0.82 at 24 °C (75 °F).

The heating unit was fabricated by sandwiching a two-element mica heater unit between two thin sheets of ceramic fiber paper and two surface plates. The overall geometry of the heating unit was 200 mm (8 inches) in diameter, with the metering area being the central 100 mm (4 inch) round section. The unit was bolted together at four points, one being in the metering section. The two sections of the heater unit were separated by a 3 mm (0.125 inch) gap around the perimeter of the metering section. The specific area of the metering section was $8.36 *10^{-3} m^2 (9.00 *10^{-2} ft^2)$. The area of the gap represented 3.3 percent of the total metering section area. The area of the metering section was determined by measurements to the centers of the gap. A 16-junction differential thermopile was installed between the mica heating unit and the surface plates such that alternate junctions

Reference: Report No. 621001443 2 May 2008



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Appendix A ASTM C 177 – THERMAL CONDUCTIVITY



were in the metering and guard sections respectively and close to the annular gap between the sections. This thermopile was fabricated of 32-gauge Type-K Chromel/Alumel wire. The sensitivity of this thermopile was approximately 0.33 mV/°C (0.18 mV/°F) at 24 °C (75 °F).

The metering area heater was connected to a Sorenson DC Power Supply. A 0.001 Ω precision resistor was connected in series with the heater and the voltage drop across this resistor (0.001 times the current) was monitored. The voltage across the heater was measured directly. The output of the differential thermopile was connected to a differential temperature controller which supplied power to the guard heater such that the thermopile output was minimized.

The cooling units consisted of a 10 mm (0.38 inch) thick copper plate which had a series of interconnected 6 mm (0.25 inch) diameter copper tubes soldered to the plate and foamed in place with a spray urethane foam, a mica electric resistance heater unit, and a surface plate. The plates and heater were similar in cross section to the heating unit. The tubing was connected to a temperature controlled circulating chiller unit and a control thermocouple was attached to the underside of the surface plate and connected to a temperature controller. Temperature control at the surface plates was accomplished by operating the circulating chiller continuously and reheating with the electrical resistance heaters.

The environmental heating unit consisted of a sheathed electric resistance cable heater sandwiched between two tightly fitting passivated stainless steel rings 300 mm (12 inches) in diameter by 100 mm (4 inches) high. The electric resistance heater was connected to a temperature controller. The environmental heating unit and test stack were enclosed by a bell jar. The approximate dimensions of the bell jar were 457mm (18 inches) in diameter by 711mm (28 inches) high. The temperature of the environmental heating unit was controlled and monitored by thermocouples attached to its inner surface. The interspaces between the test stack, environmental heating unit, and bell jar were filled with loose-fill insulation material.

Temperature measurements were performed by utilizing Type-K Chromel/Alumel thermocouples calibrated to the special limits of error specified in ASTM E 230, *Temperature-Electromotive Force (EMF) Tables for Standardized Thermocouples*. All thermocouple sensors were fabricated with #30 AWG wire. The thermocouples were fixed to the surface plates by cementing them into 1.6 mm (0.062 inch) square grooves that had been machine-cut into all the surface plates. A total of two thermocouples were cemented into each working surface; one in the metering section and one in the guard section. The temperature sensors

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Appendix A ASTM C 177 – THERMAL CONDUCTIVITY



were referenced to an Acromag Model 320 Electronic Ice Reference. The setpoint accuracy for the reference is \pm 0.5 °C (\pm 0.9 °F) with a 0.1 °C (0.2 °F) stability over an eight-hour period. The voltage drops, current, and thermopile output were metered with a Hewlett Packard Data Aquisition Unit, Model 3497, having a range of \pm 1 μ V to 300V. The resolution of the meter is 1 microvolt with a maximum error of 0.01 percent of the output and \pm 2 microvolts over an eight-hour period.

In operation, a steady temperature equilibrium was established in the test system. The temperatures of the cooling surface plates were set to their required levels. The required temperature difference across each sample was maintained by the adjustment of the power to the metering area heater. If no specific temperature difference was required, a 40 °C (75 °F) difference was used. The temperature of the environmental heating unit was controlled to the mean sample temperature level. The differential output was checked and adjusted such that the thermopile output was maintained between $\pm~0.01~\rm mV$. At equilibrium, established after ensuring that during twenty-one regular sets of ten – one minute readings, the apparent thermal conductivity did not change by more than 0.5 percent and that there was no consistent drift, the power to the metering area heater was measured with the precision resistor network and the temperatures of the working surfaces were evaluated from thermocouple readings.

The apparent thermal conductivity was calculated from

$$\lambda = \frac{Q \times L}{A \times \Delta T}$$

and the thermal resistance was calculated from

$$R = \frac{A \times \Delta T}{Q}$$

where

 λ = apparent thermal conductivity, W/m-K (Btu-in/hr-ft²-°F)

Q = power dissipation in the metering heater, W (Btu/hr)

L = total thickness of both test specimens, m (inches)

A =the metering surface area taken twice, m^2 (ft²)

ΔT = total temperature difference across both specimens, °C (°F)

R = thermal resistance, m²-K/W (hr-ft²-°F/Btu)

Reference: Report No. 621001443

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Appendix A ASTM C 177 – THERMAL CONDUCTIVITY



The instrument performance was verified using the National Institute of Standards and Technology Standard Reference Material 1450b. The calibration specimen is a high-density fibrous glass material, 25.4 mm (1.00 inch) thick, having a thermal resistance of approximately 0.803 m²-K/W (4.56 hr-ft²-°F/Btu) at 24 °C (75 °F). The overall uncertainty of the thermal resistance of the standard is estimated by NIST to be 2 percent. The instrumentation is verified every six months and after any repair or modification.

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Appendix A ASTM C 177 – THERMAL CONDUCTIVITY



Test Results

The test results are given in Table 1 and are plotted in Figure 2. The results reported apply only to the specimens that were tested.

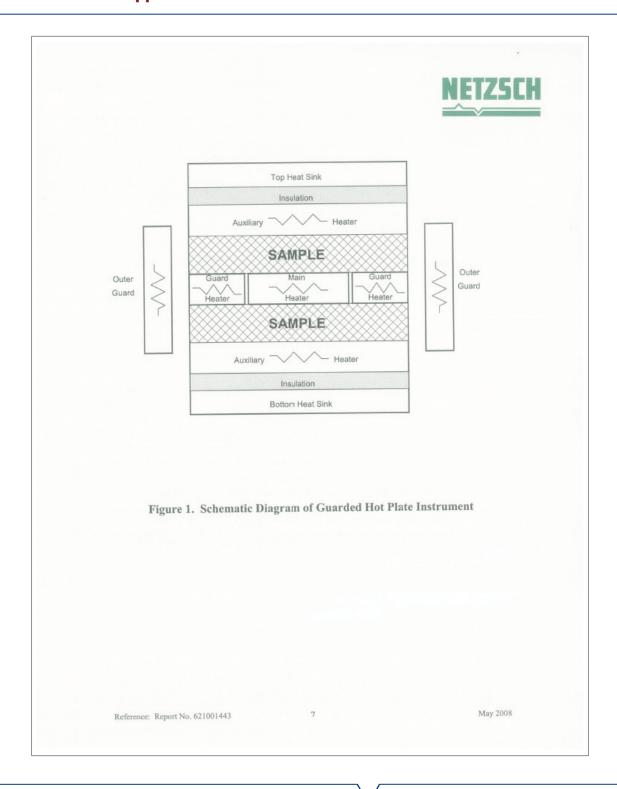
A load of approximately 2 PSI was applied to the stack during testing. Prior to testing, the average compression of several extra pieces of the material under a load of 2 PSI was measured with a Satec T500 mechanical tester to be about 6%. Rigid spacers were cut for each sample to a thickness 6% lower than the sample thickness measured with a drop gauge. Under the stack load, the instrument plates made contact with the spacers to ensure a known and uniform plate gap and sample thickness.

The thermal conductivity and resistance results are estimated to be accurate to within $\pm 5\%$.

Reference: Report No. 621001443 6 May 2008



Appendix A ASTM C 177 – THERMAL CONDUCTIVITY



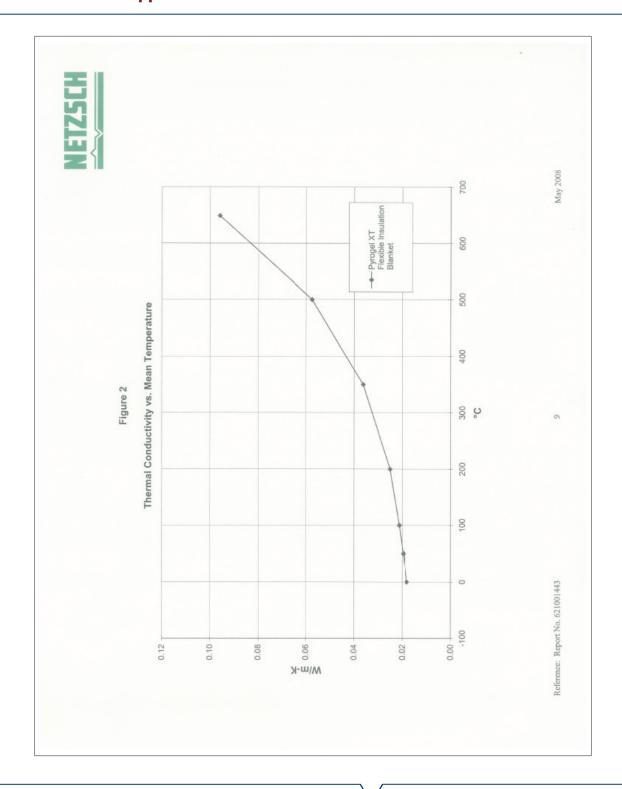


Appendix A ASTM C 177 – THERMAL CONDUCTIVITY

	nal	British	1.83 1.71 1.57	0.919 0.579 0.347		
	Thermal Resistance	SI	0.322 0.301 0.276 0.234	0.162		
	Thermal tivity	British	0.126 0.135 0.147 0.173	0.251	24	
ASTM C177 THERMAL CONDUCTIVITY TEST RESULTS	Apparent Thermal Conductivity	IS	0.0182 0.0195 0.0212 0.0250	0.0362 0.0574 0.0959	W/m-K Btu-in/hr-°F-ft² m²-K/W hr-°F-ft²/Btu	
	,	°F	73 72 73 73	74 73 76		
	Temperature	Avg. Delta	04 04 14	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	Units: tish Unit nits: sh Units	
		Mean C °F	32 122 212 212 391 661 931 1200 1200 1200 1200 1200 1200 1200	tivity SI I tivity Brit nce SI U nce Britis		
Table 1		O. C.	0 50 100 200	350 500 649	Conduct	
T ERMAL CC	st sity	lbs/ft ³	4.		Thermal Conductivity SI Units: Thermal Conductivity British Units: Thermal Resistance SI Units: Thermal Resistance British Units:	
I C177 TH	Test	kg/m³	183			
ASTM	st	inch	0.231			
	Test	MM	5.86			
	Specimen		Pyrogel XT Flexible Insulation Blanket			



Appendix A ASTM C 177 – THERMAL CONDUCTIVITY





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Appendix B ASTM E 84 – SURFACE BURNING CHARACTERISTICS



Fire Testing Laboratory



Accredited Testing Laboratory TL-216

Page 1 of 5

TEST REPORT

for

ASPEN AEROGELS

30 Forbes Road Northborough, MA 01532

Surface Burning Characteristics of Building Materials

ASTM E-84-07

Test Report No: FH-1814

Assignment No: H-513

Test Date: 3/7/2008

Report Date: 3/11/2008

Subject Material: Pyrogel XT

Prepared by:

Richard A. Costolnick Senior Test Engineer

Reviewed by:

Robert J. Menchetti Director, Laboratory Facilities and Testing Services

The results reported in this document apply to specific samples submitted for measurement. No responsibility is assumed for performance of any other specimen. This report may not be reproduced, except in full, without the written approval of the laboratory. The laboratory's test records in no way constitutes or implies product participation, approval.

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Appendix B ASTM E 84 – SURFACE BURNING CHARACTERISTICS



FH-1814 Aspen Aerogels 3/11/2008 Page 2 of 5

MATERIAL TESTED:

Material submitted by Aspen Aerogels, Northborough, MA, was described by the client as:

PYROGEL XT

Flexible Insulation Blanket

The submitted samples consisted of a single continuous roll, 24 in. wide and cut to the required 24 ft. length.

METHOD OF SUPPORT:

The test specimen was supported by 2.0 in. galvanized steel poultry netting, placed over 1/4 in. diameter steel rods spaced 24 in. on center.

RESULTS:

The results can be found on page 3 of this report.

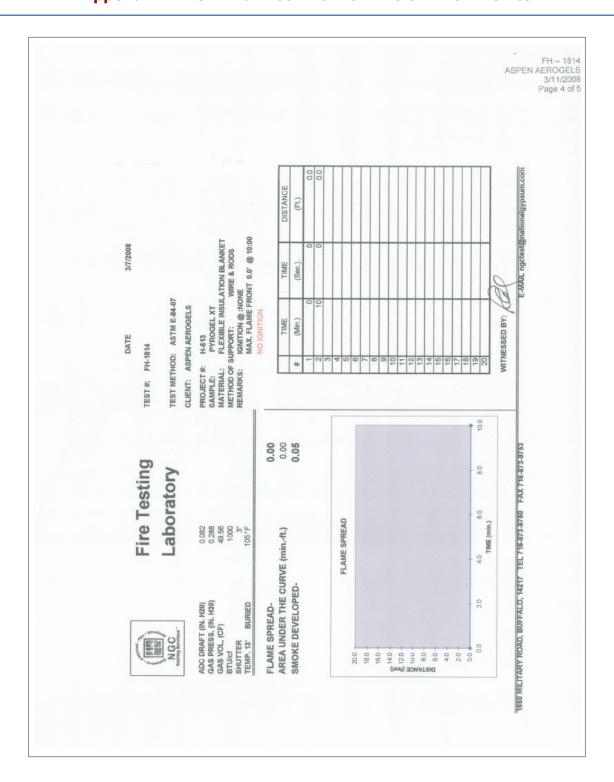


Appendix B ASTM E 84 – SURFACE BURNING CHARACTERISTICS

4 (0 to 10	22	П					
FH-1814 ASPEN AEROGELS 3/11/2008 Page 3 of 5	CALCULATED SMOKE DEVELOPED	0.05	SMOKE DEVELOPED INDEX*	100	0	SDI 0-450 0-450 0-450	arest
AS	CALCULATED FLAME SPREAD	0.00	FLAME SPREAD INDEX*	100	0	FSI <25 26-75 76-200	its), rounded to the nea
	SIDE	SYMMETRICAL	SIDE	NA	SYMMETRICAL	CLASS "A" CLASS "B" CLASS "C"	esults of multiple tes
	SUPPORT	WIRE & RODS	SUPPORT	DECKS	WIRE & RODS		(or average of the r
	TEST NO.	-		П			ed Index is the result
	RESULTS: MATERIAL TESTED	PYROGEL XT	MATERIAL TESTED	RED OAK FLOORING (CALIB.) CEMENT BOARD (CALIB.)	PYROGEL XT		* Flame Spread/Smoke Developed Index is the result (or average of the results of multiple tests), rounded to the nearest multiple of 5.

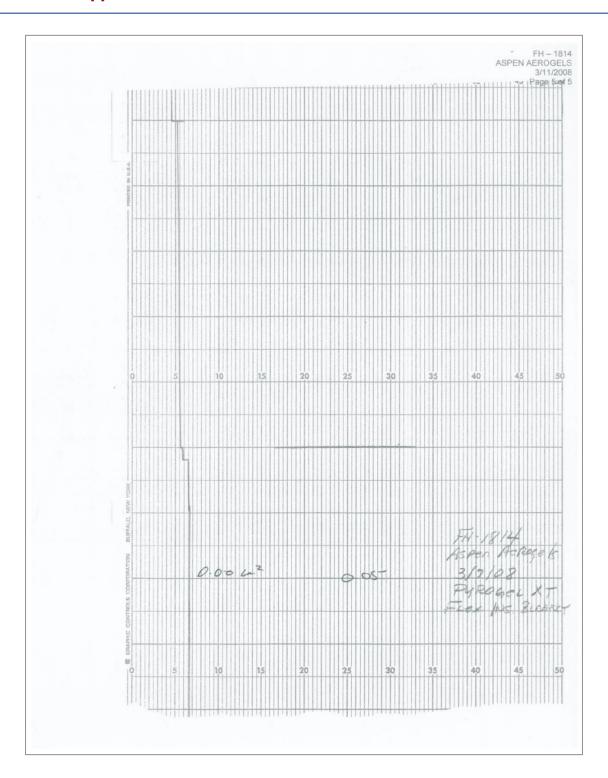


Appendix B ASTM E 84 – SURFACE BURNING CHARACTERISTICS



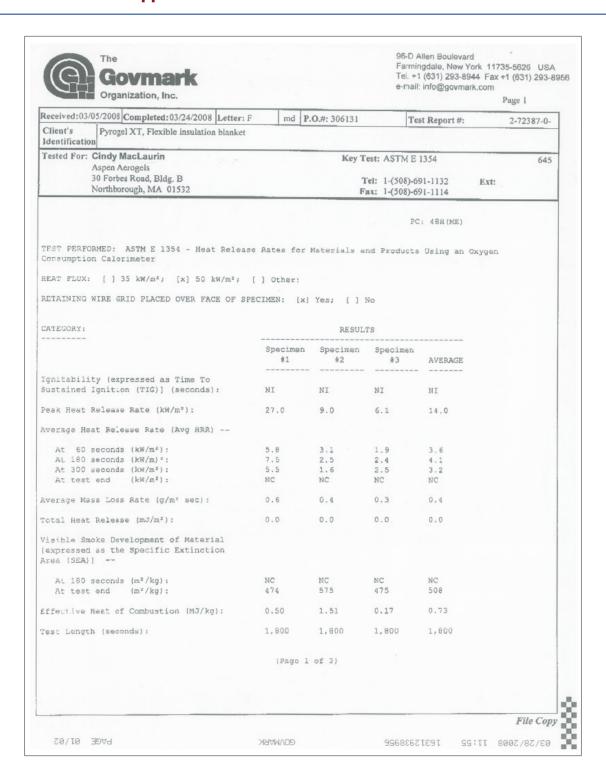


Appendix B ASTM E 84 – SURFACE BURNING CHARACTERISTICS





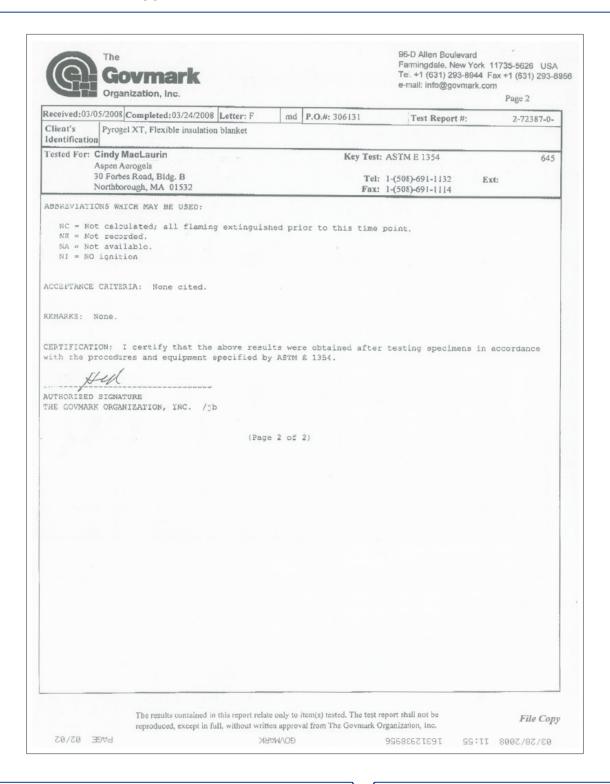
Appendix C ASTM E 1354 – CONE CALORIMETRY





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Appendix C ASTM E 1354 – CONE CALORIMETRY







Appendix D ISO 1182:1990 – NON-COMBUSTIBILITY





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Appendix D ISO 1182:1990 – NON-COMBUSTIBILITY

Project No. 3148592SAT-001	March 31, 2008
Aspen Aerogels	Page 2 of 5
AE	BSTRACT
The specimens submitted by Aspen Asp	ogels and identified as "Pyrogel XT" were
tested in accordance with ISO 1182 Non	n-combustibility test.
Intertek and its Client, Intertek's responsibility and li	nt and is provided pursuant to the agreement between liability are limited to the terms and conditions of the
agreement. Intertek assumes no liability to any paragreement, for any loss, expense or damage occa	arty, other than to the Client in accordance with the
authorized to copy or distribute this report and then o	only in its entirety. Any use of the Intertek name or one ed material, product or service must first be approved
in writing by Intertek. The observations and test re	esults in this report are relevant only to the sample
an Intertek certification program.	naterial, product, or service is or has ever been under
This report contains	s a total of 5 pages.
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John Gutierrez	and the second s
Tethnician	
Reviewed and approved:	
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772	March 31, 2008
	March 31, 2006
Servando Romo	
Servando Romo Project Manager	
Project Manager	
Project Manager	ETL SEMKO
Project Manager	ETL SEMKO



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Appendix D ISO 1182:1990 – NON-COMBUSTIBILITY

Project No. 3148592SAT-001 Aspen Aerogels

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I. INTRODUCTION

This report describes the results of the ISO 1182 Non-combustibility test.

It may be important to ascertain whether a material will or will not contribute directly to fire development and this test has been designed to allow this to be done. Its results will provide information from which regulating authorities will be assisted in deciding whether the material in question may be used without undue hazard in certain locations in buildings. From a technical point of view, the test gives no absolute statement concerning "non-combustibility".

The test results relate only to the behavior of the test specimens of a material under the particular conditions of the test; they are not intended to be the sole criterion for assessing the potential fire hazard of the material in use.

II. PURPOSE

The results of the ISO 1182 test method may be used for the determination of the combustibility performance of a building material under specified conditions. (750°C). The method is intended for the testing of building materials but is not applicable to the testing of products which are coated, faced or laminated.

III. TEST SPECIMENS

Five specimens of materials were tested. The specimens were cylindrical with a diameter of 45 mm and a height of 52 mm. The volume of the specimens was 82.6 cm³. The specimens consisted of flexible insulation blanket.

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Appendix D ISO 1182:1990 – NON-COMBUSTIBILITY

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IV. TEST PROCEDURE

Prior to testing, the specimens were conditioned at $60^{\circ} \pm 5^{\circ}\text{C}$ for twenty-four hours, then stored in a desiccator and cooled to ambient temperature. When the power to the furnace is adjusted so that the average furnace temperature is $750 \pm 5^{\circ}\text{C}$ for at least ten minutes, the samples are placed on the specimen holder and instrumented with thermocouples. The thermocouples are placed on the outer surface at mid-height and the geometric center of the specimen. Once the specimen has been instrumented, the holder (with the specimen) is placed in the furnace and the timing device is started. The furnace and specimen temperatures are recorded during the test. The specimen is kept in the furnace until final temperature equilibrium. The mass of the specimens is recorded before and after testing.

V. RESULTS AND OBSERVATIONS

Specimens submitted by: Aspen Aerogels

Date received: March 26, 2008 (This specimen was received in good condition.)

Date tested: March 28, 2008

Specimen ID: Pyrogel XT

Description of specimen: Flexible Insulation Blanket

Environmental Conditions: 70°F and 63% r.h.

This Test Witnessed by: Owen Evans and Chris Abeles

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Appendix D ISO 1182:1990 – NON-COMBUSTIBILITY

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The results of these tests are presented in the following tables:

Specimen Number	1	2	3	4	5
Initial Furnace Temp. (°C)	746	748	755	754	751
Mass Before Test (grams)	14.75	15.18	14.16	13.99	14.42
Sustained Flaming (sec.)	None	None	None	None	None
Mass After Test (grams)	14.14	14.59	13.51	13.43	13.91
Percent Mass Loss	4.14	3.89	4.59	4.00	3.54
Average Percent Mass Loss of F	Average Percent Mass Loss of Five Specimens				
Mean Duration of Sustained					

FURNACE TEMPERATURES

Specimen Number	1	2	3	4	5
Max. Furnace Temperature (°C)	809.9	811.0	819.0	799.9	808.9
Final Furnace Temperature (°C)					
Furnace Temperature Rise (°C)	34.1	28.0	26.7	22.9	23.6
Average Furnace Temperature R	Rise of F	ive Spe	cimens	27.1	

SPECIMEN SURFACE TEMPERATURES

Specimen Number	1	2	3	4	5
Max. Surface Temperature (°C)	828.8	823.7	832.1	826.2	814.6
Final Surface Temperature (°C)	788.2	796.4	801.6	793.2	787.9
Surface Temperature Rise (°C)	40.6	27.3	30.5	33.0	26.7
Average Surface Temperature R					

SPECIMEN CENTER TEMPERATURES

Specimen Number	1	2	3	4	5
Max. Center Temperature (°C)	922.7	917.7	903.6	901.8	908.3
Final Center Temperature (°C)	762.7	776.0	770.2	761.6	767.3
Center Temperature Rise (°C)	160.0	141.7	133.4	140.2	141.0
Average Center Temperature R					

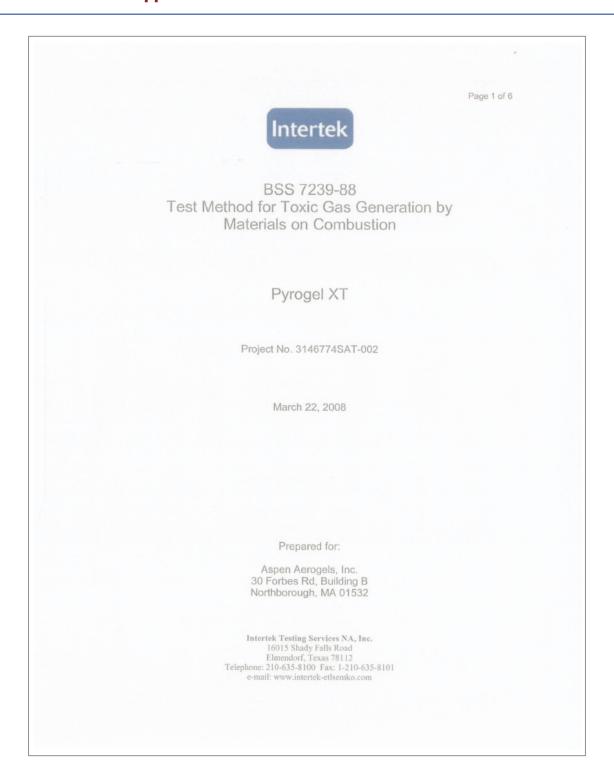
Test Notes: (Time in Min: Sec. Top View Only)
Sample #1 had glowing flash spots at 0:59 (min:sec), no flame ignition visible.
Sample #2 had glowing flash spots at 0:58 (min:sec), no flame ignition visible.
Sample #3 had glowing flash spots at 1:01 (min:sec), no flame ignition visible.
Sample #4 had glowing flash spots at 1:22 (min:sec), no flame ignition visible.
Sample #5 had glowing flash spots at 1:15 (min:sec), no flame ignition visible.

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Appendix E BSS 7239 – TOXIC GAS GENERATION





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Appendix E BSS 7239 – TOXIC GAS GENERATION

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Abstract

Specimens submitted by Aspen Aerogels, Inc. and identified as "Pyrogel XT", were tested in accordance with BSS 7239-88 by the procedures reported herein. Concentrations of the gases CO, HF, HCl, NO_X, SO₂, and HCN were determined. For results see page 6, table 2

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This report contains a total of 6 pages.

John Gutierrez Technician March 22, 2008

Reviewed and approved:

Servando Romo Project Manager March 22, 2008

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Appendix E BSS 7239 – TOXIC GAS GENERATION

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INTRODUCTION

The determination of the gaseous products of smoke (often called "fire gases"), including those due to either pyrolysis or combustion, is a difficult problem. The composition of the smoke from most products is affected by the nature of the fire test procedure that created the smoke (i.e., flaming or nonflaming conditions, specimen size and configuration, external applied heat flux, etc.). Gas sampling considerations include the time at which sampling of the atmosphere was initiated and the duration of the sampling (smoke concentrations can change with time); the position of the sampling probe (concentrations can change with location in a chamber); the method of sampling (a major cause of error in fire gas analysis); and the actual method of analysis. Sampling and analysis of fire gases are described in some detail in ASTM E800 ("Standard Guide for Measurement of Gases Present or Generated During Fires"), to which the reader is referred.

One of the common test methods for creating "smoke" is the ASTM E662 smoke chamber (a method fundamentally the same as BSS 7238), which provides for both flaming and nonflaming combustion of 76 mm x 76 mm (3-in. x 3-in.) specimens exposed to an external radiant heat flux of 25 kW/m². The smoke is retained within the confines of the 500-L chamber. For this test procedure, analysis of gaseous components is performed starting at four minutes into the test run. Only the flaming exposure is specified. Actual analysis of the gases of interest may be performed directly using Dräger® colorimetric gas analysis tubes; by trapping the gases in solution impingers (bubblers) and subsequently analyzing the anions by ion-selective electrodes, itration or liquid chromatography; or by instruments designed to measure the specific gas(es) of interest (e.g., gas chromatographic methods, NDIR or FTIR analyzers).

The following gases are required to be measured by this test standard:

CO carbon monoxide HF hydrogen fluoride HCI hydrogen chloride

NO_x nitrogen oxides (both NO, nitric oxide, and NO₂, nitrogen dioxide, are

detected) sulfur dioxide

SO₂ sulfur dioxide HCN hydrogen cyanide





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Appendix E BSS 7239 – TOXIC GAS GENERATION

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In our test procedures, Dräger® colorimetric gas analysis tubes are used. These devices are small glass tubes containing one or more chemical indicators/absorbents that change color when a specific gas reacts with the chemical inside the tube. The length of the coloration is proportional to the concentration of the gas when a fixed volume of the test atmosphere is drawn through the tube (which is accomplished by a hand pump). These tubes have several distinct advantages over other analytical methods for fire gases under the conditions of this test procedure. They are precalibrated; they are relatively simple to operate; there is nothing between the gas of interest and the analysis tube; the results are straight-forward and immediate; and this single technique can be used for each of the gases specified (plus several other common gases). Other procedures require more extensive instrumentation with calibration by standard solutions or gases; they introduce additional sampling concerns (which are different for each gas); and no single technique can be used for the six gases specified.

Information is available on each of the Dräger tubes describing the potential interferences for each tube and the range of concentrations over which the tube is calibrated. The stated accuracy of these tubes is in the range of 10-15 percent; however, the combination of sampling errors and analytical uncertainty in other methods could also approach this. In our procedure, we burn several test specimens and take an average of these readings in an effort to minimize the uncertainty in the results.

This standard is intended to measure and describe the properties of materials or products in response to heat and flame under controlled laboratory conditions and is not intended to describe or appraise the fire hazard or fire risk of materials, products, or assemblies under actual fire conditions.

TEST PROCEDURE

Specimens were exposed to flaming conditions in the smoke chamber, in accordance with the procedures in ASTM E662. Gas analyses for the species listed below were performed using Dräger[®] gas detector tubes. Specimens were exposed to flaming conditions for four minutes; then the igniter was extinguished, the specimen was displaced from the radiant heat flux, any excess pressure within the chamber was released, and the analyses were started within one minute.





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Appendix E BSS 7239 – TOXIC GAS GENERATION

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Gas samples were extracted using the gas analysis tubes from points approximately six inches from the top of the chamber and four inches from either side wall. Although this is not the same location as given in BSS 7239

(i.e., 12 in. from the ceiling, in the center of the chamber), our sampling location was determined after considerable reflection on the advantages and disadvantages of various sampling schemes using these tubes. It is our belief that there would be no difference in the two sampling locations using our method of specimen exposure and sampling methodology.

Different tubes were drawn simultaneously from two different locations at opposite sides of the chamber in order to reduce the total time required for sampling. For replicate tests, tubes were drawn by a different operator from the other location. The gases more likely to change concentration due to reaction with moisture or soot in the chamber (i.e., HCI, HCN, HF) are drawn first in order to minimize their residence time in the chamber; while CO is sampled last, since its concentration will not change with time.

Table 1 is a listing of the specific gas detector tubes used in this study

Table 1. Identification of Gas Analysis Tubes used

Gas	Draeger Tube No.	Concentration Range, ppm	Number of Strokes
CO	5/c	10-300	10
HF	1.5/b	1.5 - 15	20
HCI	1/a	1-10	10
NOx	2/a	5-100	5
SO ₂	0.5/a	1 - 25	10
HCN	2/a	2 - 30	5

CRITERIA

In general the airline industry limits (in ppm) are as follows: CO=3500, HF=200, HCI=500, HCI=5

Other limits may be required depending on the end use of the product so it is recommended that the proper governing organizations be contacted.

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Appendix E BSS 7239 – TOXIC GAS GENERATION

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RESULTS

Specimens submitted by: Aspen Aerogels, Inc.

Date received: March 3, 2008 (This specimen was received in good condition.)

Date tested: March 21, 2008

Specimen ID: Pyrogel XT

Description of specimen: Flexible Insulation Blanket

Environmental conditions: 70°F and 60% r.h.

Specimen preparation and mounting method

The sample was prepared by the client and consisted of a 3 in. \times 3 in. \times 0.23 in. sheet insulation. The specimen was subjected to the standard conditioning and mounting methods.

Table 2. Test Results with notations (concentrations in ppm unless otherwise noted)

No.	HCI	HCN	HF	NOx	SO ₂	CO
1 Flaming	<1	N.D.	N.D.	5	N.D.	100
2 Flaming	<1	N.D.	N.D.	5	N.D.	100
Average	NA	N.D.	N.D.	5.00	N.D.	100

NOTES:

N.D. = "none detected" N/A = Not Available

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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

ST REPORT



REPORT NUMBER: 3159033 ORIGINAL ISSUE DATE: August 28, 2008 REVISED DATE: N/A

EVALUATION CENTER

16015 Shady Falls Road Elmendorf, TX 78112 (voice) 210-635-8100 (fax) 210-635-8101 www.intertek-etlsemko.com

RENDERED TO

Aspen Aerogels, Inc. 30 Forbes Road Building B NORTHBOROUGH MA 01532

PRODUCT EVALUATED: Pyrogel® XTF Insulation Material EVALUATION PROPERTY: Safety Fire Resistance

Report of Testing Pyrogel® XTF Insulation Material for compliance with the applicable requirements of the following criteria: UL 1709-05 Standard for Safety Rapid Rise Fire Tests of Protection Materials for Structural Steel

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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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2 Introduction

Intertek Testing Services NA (Intertek) has conducted testing for Aspen Aerogels, Inc. on Pyrogel® XTF Insulation Material, to evaluate its fire resistance. Testing was conducted in accordance with UL 1709-05 Standard for Safety Rapid Rise Fire Tests of Protection Materials for Structural Steel. This evaluation took place on August 21, 2008.

3 Test Samples

3.1. SAMPLE SELECTION

Samples of Pyrogel® XTF were submitted to Intertek directly from the client. Samples were not independently selected for testing. Samples were received at the Evaluation Center on August 18, 2008

3.2. SAMPLE AND ASSEMBLY DESCRIPTION

Intertek technicians installed 14 thermocouples onto the web on each of six W10 X 49 standard columns, 8' long. The thermocouples were installed across 4 zones: A-A, 5; B-B, 3; C-C, 3; and D-D, 3 (see Appendix A).

Representatives from Aspen Aerogels, Inc. installed the Pyrogel® XTF insulation onto the columns. Each of the column web cavities were filled with 19 -21 strips of Pyrogel® XTF (8.9" X 98" X nominal 6mm) to provide a nominal 120mm of insulation on each side of the web. The strips were held in place with 2-3 bands of 0.047" O.D. stainless steel wire (see Appendix C).

Courses (sections) of the Pyrogel® XTF insulation, either 32" or 48" wide and of varying lengths, were wrapped around the web-filled columns in layers (2, 5, 8, 8, 12, 14) alternating the 32" and 48" width insulation to stagger circumferential seams without telescoping. For the thicker, multilayered columns (P5 – 14) some courses were "double length" and wrapped around twice – 2 layers per course. Some of the columns started with the 32" width and some with the 48" (see configuration table, next page). Each course of insulation overlapped itself by nominally 5", but butted up to the course above and/or below it on the column. If the first course consisted of 32" insulation, the second course was 48" insulation and *visa versa*, staggering the butt joints of the layer beneath it. A 48" course of insulation was the preferred outermost layer on a column to reduce the number of circumferential seams closest to the heat of the furnace. Each course was held in place with 2-3 bands of 0.047" O.D. stainless steel wire, then secured with ½" 0.02 stainless steel bands with ½" stainless steel wing seals, applied 12" o.c. but no closer than 2" from the edge of a seam, tightened with a pistol-grip banding tool (see Appendix A).

The installation process started with the application of a thin film of spray adhesive (3M Hi-Strength 90 Spray Adhesive or Foster Fos-Stik Clear Adhesive Spray 85-45) in a 3 - 4" strip down the leading edge of the section of insulation and the corresponding area of the web-fill strip where the installation would begin. The first course was always installed at the bottom of the column. The leading edge was attached to the edge of the web-fill layers (NOT on the





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metal beam) and wrapped counterclockwise, overlapping itself to a point half way across the web where it started (approx 5") and was held in place with 0.047" O.D wire. Another course was applied above that one, and one above that (if using 32" widths), butting the seams, completing the first course on the column.

The second course was installed in the same fashion as the first but used the alternate width of insulation to overlap the circumferential seams of the previous layer, and was started at the edge of the web-fill on the <u>opposite</u> side of the column (staggering longitudinal seams). Additional courses followed the same process, alternating the width of insulation used as well as the side of the beam as its starting point. The stainless steel bands were applied after each 2 layers (not courses) of wrapping.

The 96" tall columns were covered with 3 strips of 36" wide, 0.02 stainless steel cladding, each strip overlapping itself 3" and overlapping the one below it by 6". The cladding was installed with a slip-joint when overlapping an adjacent piece and each section was secured with $\frac{1}{2}$ " 0.02 stainless steel bands and wing seals, installed 12"o.c. Finally, #42 blind rivets with 2 #8 flat stainless steel washers were installed 6" o.c. down the longitudinal seam and in 4 equidistant places around the overlapping circumferential seams (see Appendix A).

4 Testing and Evaluation Methods

The completed column assemblies were placed in the Laboratory's full scale horizontal furnace in two rows of 3 each. The test was initiated at 10:55 a.m. on Thursday, August 21, 2008. Representatives from Aspen Aerogels, Inc. were in attendance. The ambient temperature and humidity at the time were 84°F and 76%RH. The outputs of all test specimens and furnace probes were monitored by a 300 channel Yokogawa, Inc., Model Darwin Data Acquisition The computer was programmed in LabVIEW to send the commands to the data acquisition systems to sample the data input lines and to convert the raw data into a usable format (i.e., degrees Fahrenheit) for display on screen and storage as an ASCII tab-delimited text file. The data was saved at 60-second intervals. Following the test, the files were imported into MS Excel for tabular and graphical display. The maximum allowed temperature for any one thermocouple on a column was 1200°F and for the TC Average within a section was 1000 °F.

4.1. TEST STANDARD

Testing was conducted in accordance with UL 1709-05 Standard for Safety Rapid Rise Fire Tests of Protection Materials for Structural Steel.





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5 Testing and Evaluation Results

5.1. RESULTS AND OBSERVATIONS

The test was initiated at 10:55 A.M. on August 21, 2008 and ran for 240 minutes. The observations made during the test are listed below:

Time (min:sec)	Observation
0:00	Test initiated
10:00	Smoke from the furnace, around the lid
21:00	Flame from around the samples
72:54	TC #11 from P2 exceeds max allowed temp
152:00	TC #11 from P5 exceeds max allowed temp
205:00	TC #9 from P8A exceeds max allowed temp
209:00	TC #3 from P8B exceeds max allowed temp
241:00	Test terminated

The test results for each column are presented below.

Column P2 (12mm):

Though the first thermocouple to exceed the 1200°F maximum occurred during the 72nd minute of the test (TC #11) the maximum allowable TC average (1000°F) was exceeded at the 68-minute mark.

In accordance with the UL 1709 test standard, a calculation for any correction to the indicated fire resistance period was done. The correction factor was then mathematically added to the indicated fire resistance period, yielding the fire resistance period achieved by this specimen:

ITEM	DESCRIPTION	TEST VALUE
С	correction factor	-0.53 minutes -32 seconds
1	indicated fire-resistance period	68 minutes
Α	area under the curve of indicated average furnace temperature for the first three fourths of the indicated period	89134 (°F•min)
As	area under the standard furnace curve for the same part of the indicated period	90188 (°F•min)
	FIRE RESISTANCE PERIOD ACHIEVED BY THIS SPECIMEN ==>	67 minutes





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Note: The standard specifies that the fire resistance be determined to the nearest integral minute. Consequently, if the correction factor is less than 30 seconds, and the test specimen met the criteria for the full indicated fire resistance period, no correction is deemed necessary.

Column P5 (30mm):

Though the first thermocouple to exceed the 1200°F maximum occurred during the 152nd minute of the test (TC #11), the maximum allowable TC average (1000°F) was exceeded at the 131-minute mark.

In accordance with the UL 1709 test standard, a calculation for any correction to the indicated fire resistance period was done. The correction factor was then mathematically added to the indicated fire resistance period, yielding the fire resistance period achieved by this specimen:

ITEM	DESCRIPTION	TEST VALUE
С	correction factor	-0.47 minutes -28 seconds
1	indicated fire-resistance period	131 minutes
Α	area under the curve of indicated average furnace temperature for the first three fourths of the indicated period	176129 (°F•min)
As	area under the standard furnace curve for the same part of the indicated period	177091 (°F•min)
	FIRE RESISTANCE PERIOD ACHIEVED BY THIS SPECIMEN ==>	131 minutes

Note: The standard specifies that the fire resistance be determined to the nearest integral minute. Consequently, if the correction factor is less than 30 seconds, and the test specimen met the criteria for the full indicated fire resistance period, no correction is deemed necessary.

Column P8A (48mm):

Though the first thermocouple to exceed the 1200°F maximum occurred during the 205th minute of the test (TC #9) the maximum allowable TC average (1000°F) was exceeded at the 184-minute mark.

In accordance with the UL 1709 test standard, a calculation for any correction to the indicated fire resistance period was done. The correction factor was then mathematically added to the indicated fire resistance period, yielding the fire resistance period achieved by this specimen:





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ITEM	DESCRIPTION	TEST VALUE
С	correction factor	-0.37 minutes -22 seconds
1	indicated fire-resistance period	184 minutes
Α	area under the curve of indicated average furnace temperature for the first three fourths of the indicated period	250286 (°F•min)
As	area under the standard furnace curve for the same part of the indicated period	251051 (°F•min)
	FIRE RESISTANCE PERIOD ACHIEVED BY THIS SPECIMEN ==>	184 minutes

Note: The standard specifies that the fire resistance be determined to the nearest integral minute. Consequently, if the correction factor is less than 30 seconds, and the test specimen met the criteria for the full indicated fire resistance period, no correction is deemed necessary.

Column P8B (48mm):

Though the first thermocouple to exceed the 1200°F maximum occurred during the 209th minute of the test (TC #3) the maximum allowable TC average (1000°F) was exceeded at the 175-minute mark.

In accordance with the UL 1709 test standard, a calculation for any correction to the indicated fire resistance period was done. The correction factor was then mathematically added to the indicated fire resistance period, yielding the fire resistance period achieved by this specimen:

ITEM	DESCRIPTION	TEST VALUE
С	correction factor	-0.40 minutes -24 seconds
1	indicated fire-resistance period	175 minutes
Α	area under the curve of indicated average furnace temperature for the first three fourths of the indicated period	237294 (°F•min)
As	area under the standard furnace curve for the same part of the indicated period	238108 (°F•min)
	FIRE RESISTANCE PERIOD ACHIEVED BY THIS SPECIMEN ==>	175 minutes

Note: The standard specifies that the fire resistance be determined to the nearest integral





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minute. Consequently, if the correction factor is less than 30 seconds, and the test specimen met the criteria for the full indicated fire resistance period, no correction is deemed necessary.

Column P11 (66mm):

Neither the individual nor the average thermocouple maximums were exceeded during the 240-minute test.

In accordance with the UL 1709 test standard, a calculation for any correction to the indicated fire resistance period was done. The correction factor was then mathematically added to the indicated fire resistance period, yielding the fire resistance period achieved by this specimen:

ITEM	DESCRIPTION	TEST VALUE
С	correction factor	-0.37 minutes -22 seconds
1	indicated fire-resistance period	240 minutes
A	area under the curve of indicated average furnace temperature for the first three fourths of the indicated period	327951 (°F•min)
As	area under the standard furnace curve for the same part of the indicated period	328709 (°F•min)
	FIRE RESISTANCE PERIOD ACHIEVED BY THIS SPECIMEN ==>	240 minutes

Note: The standard specifies that the fire resistance be determined to the nearest integral minute. Consequently, if the correction factor is less than 30 seconds, and the test specimen met the criteria for the full indicated fire resistance period, no correction is deemed necessary.

Column P14 (84mm):

Neither the individual nor the average thermocouple maximums were exceeded during the 240-minute test.

In accordance with the UL 1709 test standard, a calculation for any correction to the indicated fire resistance period was done. The correction factor was then mathematically added to the indicated fire resistance period, yielding the fire resistance period achieved by this specimen:

ITEM	DESCRIPTION	TEST VALUE
С	correction factor	-0.37 minutes -22 seconds
I A	indicated fire-resistance period area under the curve of indicated average	240 minutes





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	furnace temperature for the first three fourths of the indicated period	327951 (°F•min)
As	area under the standard furnace curve for the same part of the indicated period	328709 (°F•min)
	FIRE RESISTANCE PERIOD ACHIEVED BY THIS SPECIMEN ==>	240 minutes

Note: The standard specifies that the fire resistance be determined to the nearest integral minute. Consequently, if the correction factor is less than 30 seconds, and the test specimen met the criteria for the full indicated fire resistance period, no correction is deemed necessary.

Summary of fire resistance achieved by each column:

P2 (12mm)	67 minutes
P5 (30mm)	131 minutes
P8A (48mm)	184 minutes
P8B (48mm)	175 minutes
P11 (66mm)	240 minutes
P14 (84mm)	240 minutes

6 Conclusion

Intertek Testing Services NA (Intertek) conducted testing for Aspen Aerogels, Inc., on Pyrogel® XTF Insulation Material, to evaluate its fire resistance. Testing was conducted in accordance with UL 1709-05 Standard for Safety Rapid Rise Fire Tests of Protection Materials for Structural Steel. The P2 (12mm) column received a fire resistance rating of 67 minutes, the P5 (30mm) column received a fire resistance rating of 184 minutes, the P8B (48mm) column received a fire resistance rating of 175 minutes, the P11 (66mm) column received a fire resistance rating of 240 minutes, and the P14 (84mm) column received a fire resistance rating of 240 minutes. This evaluation was completed on August 21, 2008.

The conclusions of this test report may not be used as part of the requirements for Intertek product certification. Authority to Mark must be issued for a product to become certified.

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Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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INTERTEK TESTING SERVICES NA

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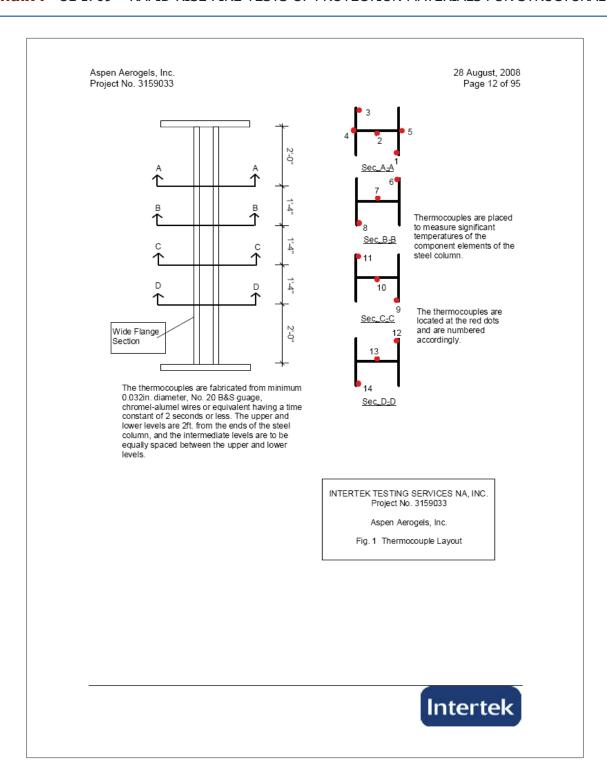
Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerogels, Inc. Project No. 3159033 28 August, 2008 Page 11 of 95 APPENDIX A Assembly Drawings Intertek





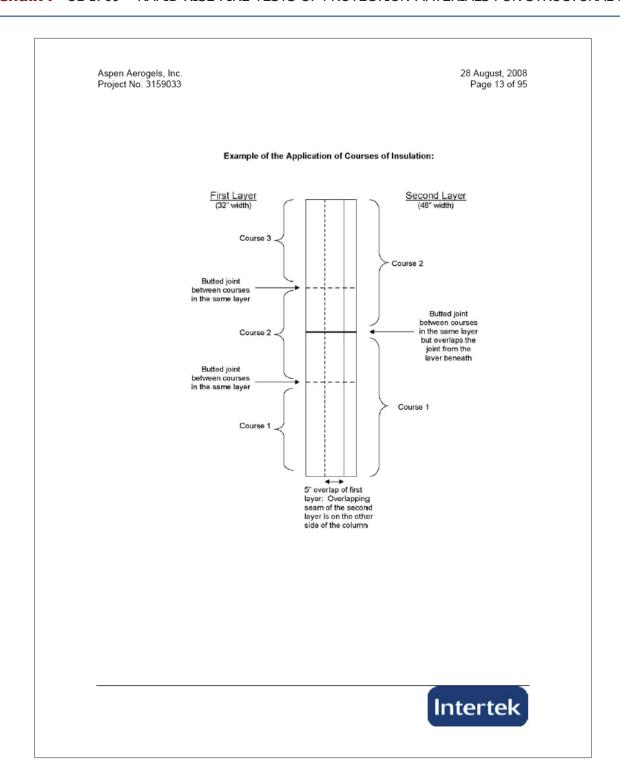
Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL







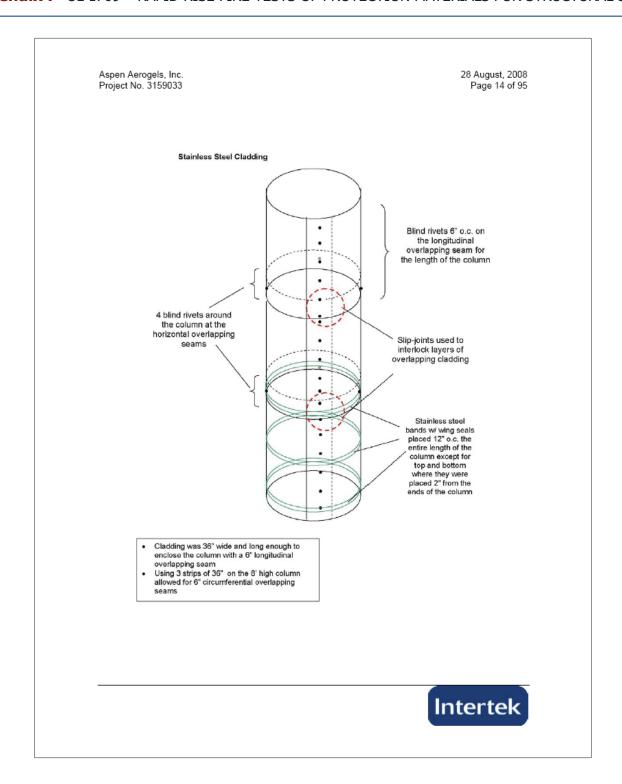
Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL







Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL





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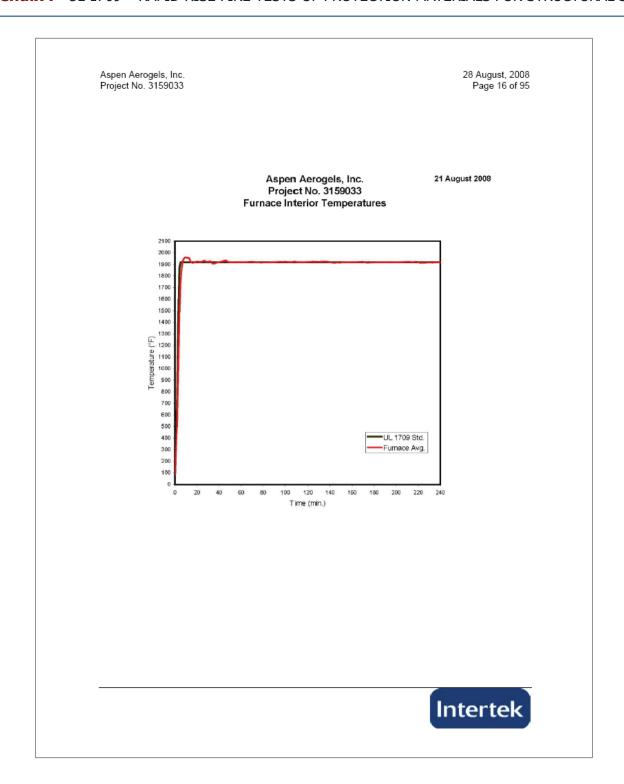
Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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	APPENDIX B Temperature Data		
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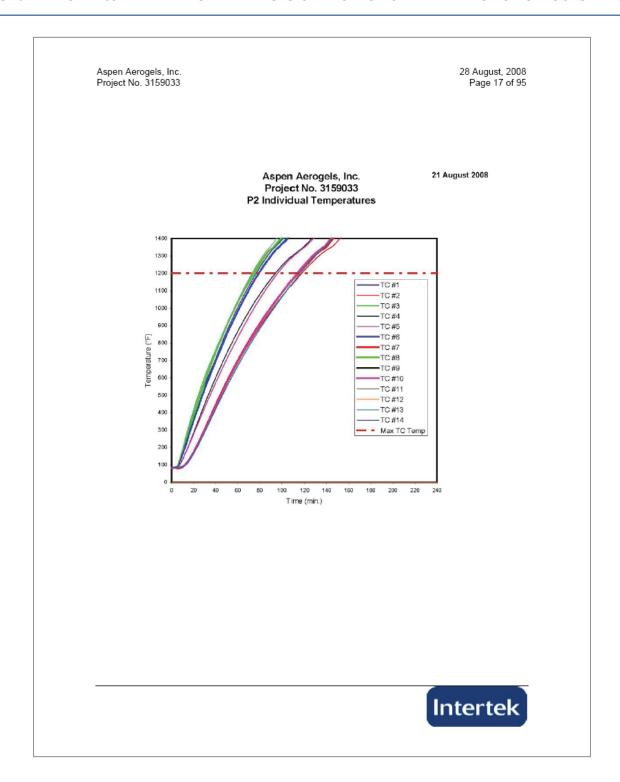
Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL







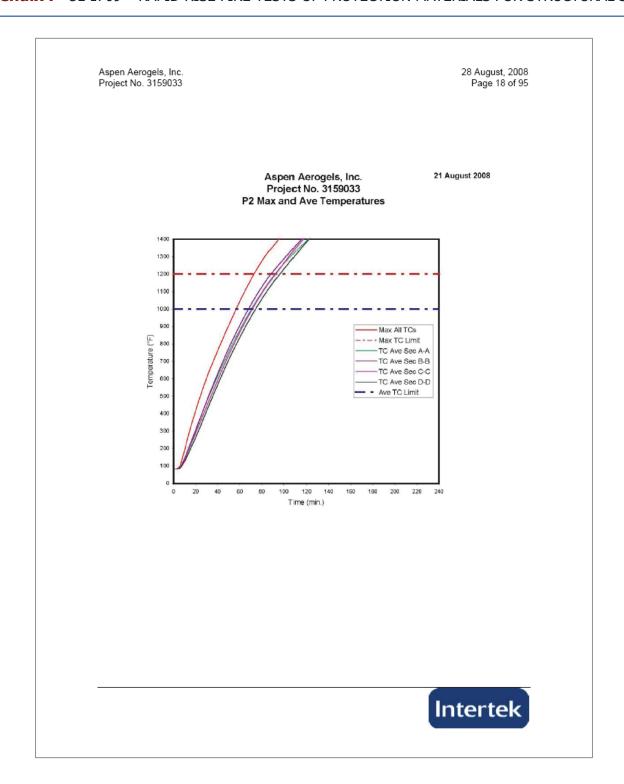
Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL







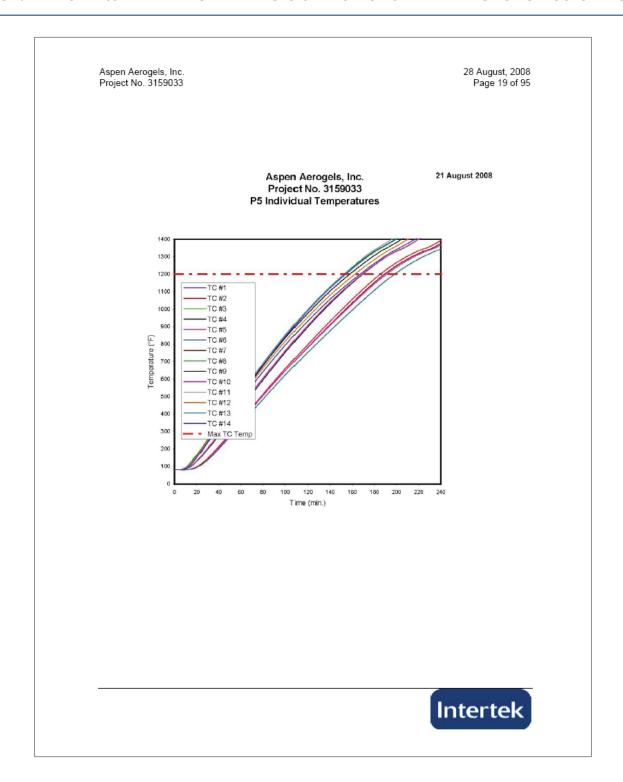
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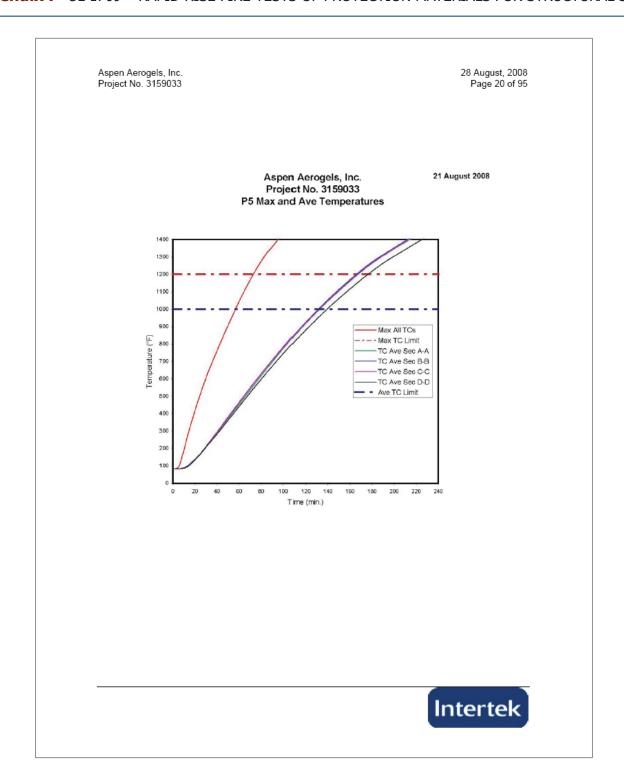
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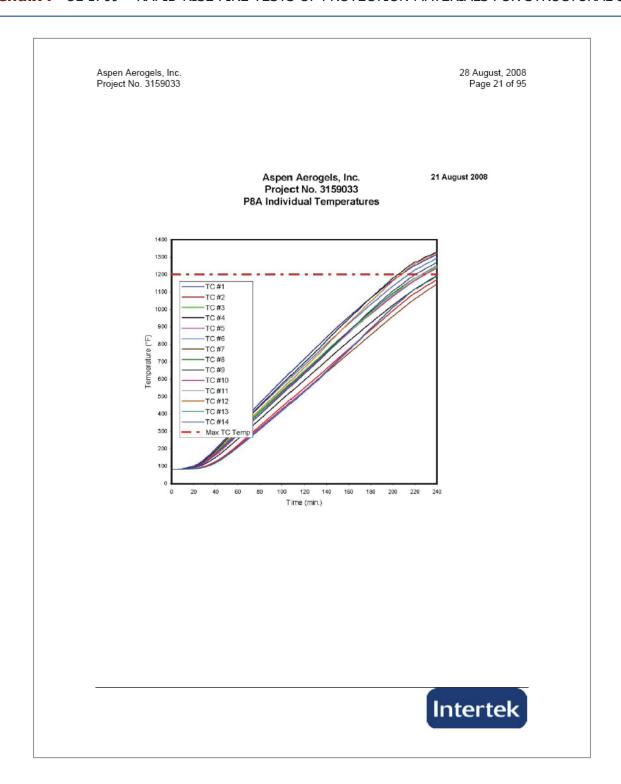
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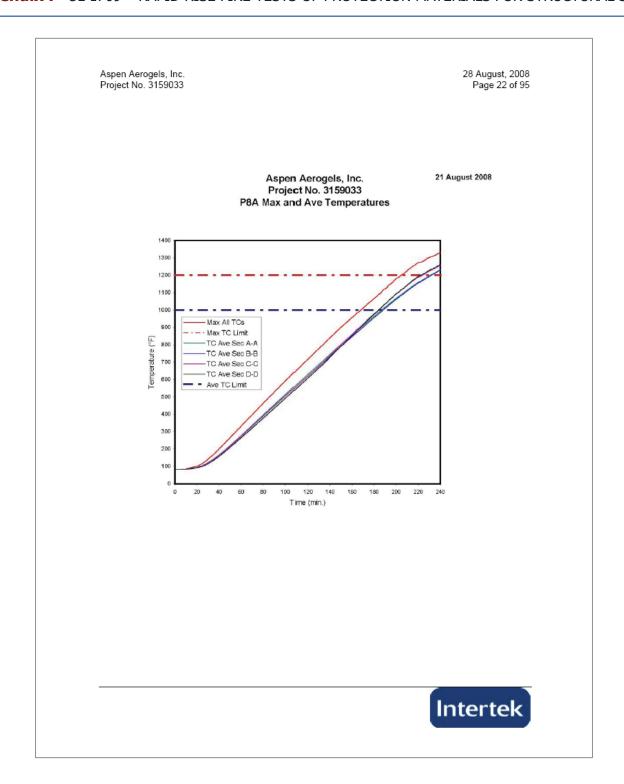
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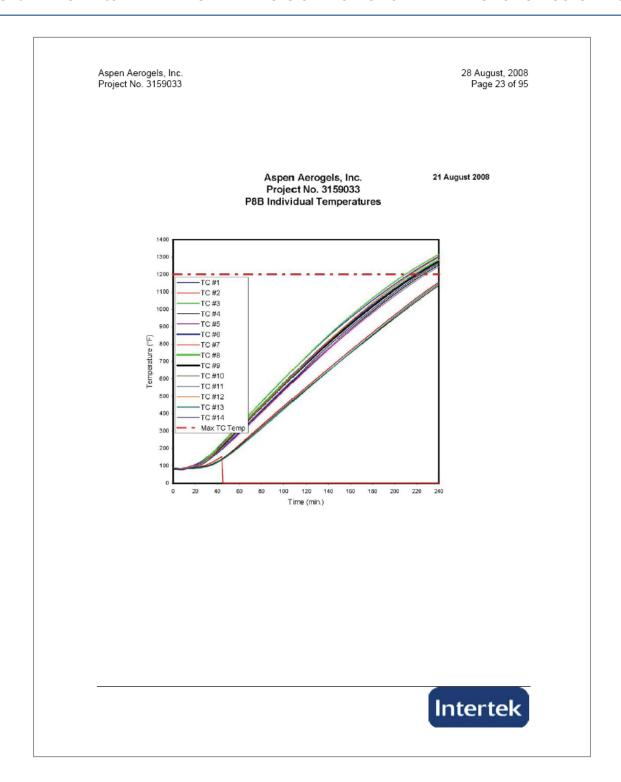
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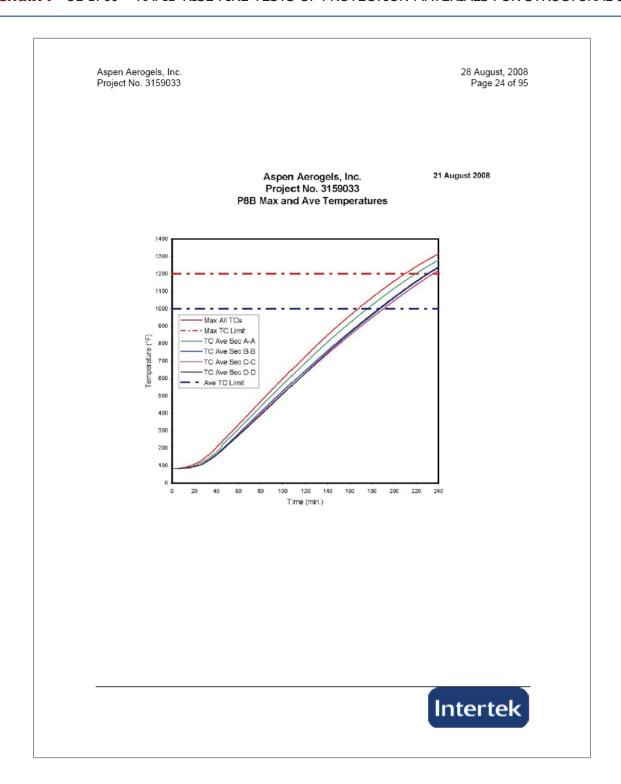
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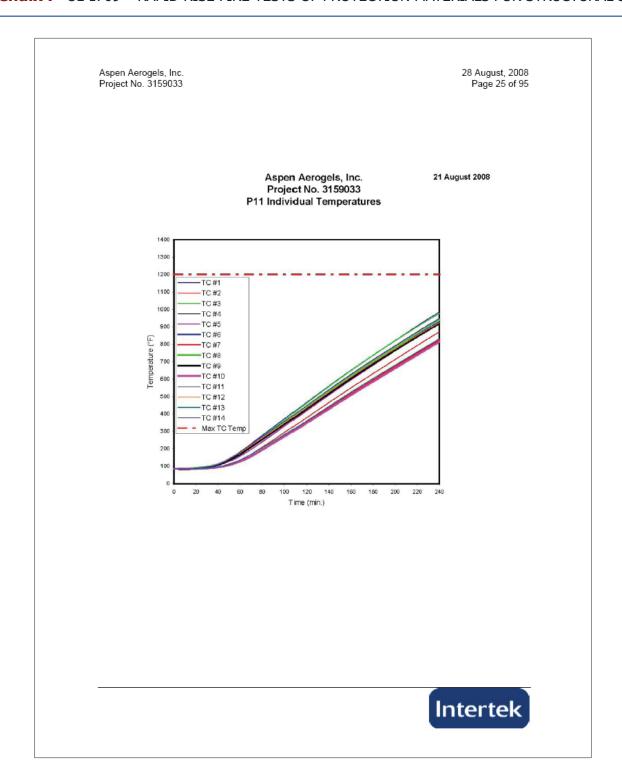
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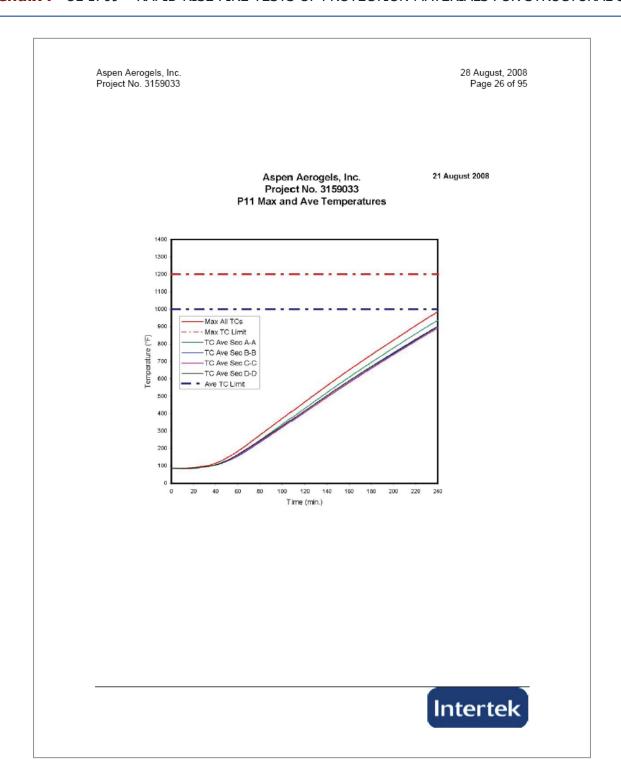
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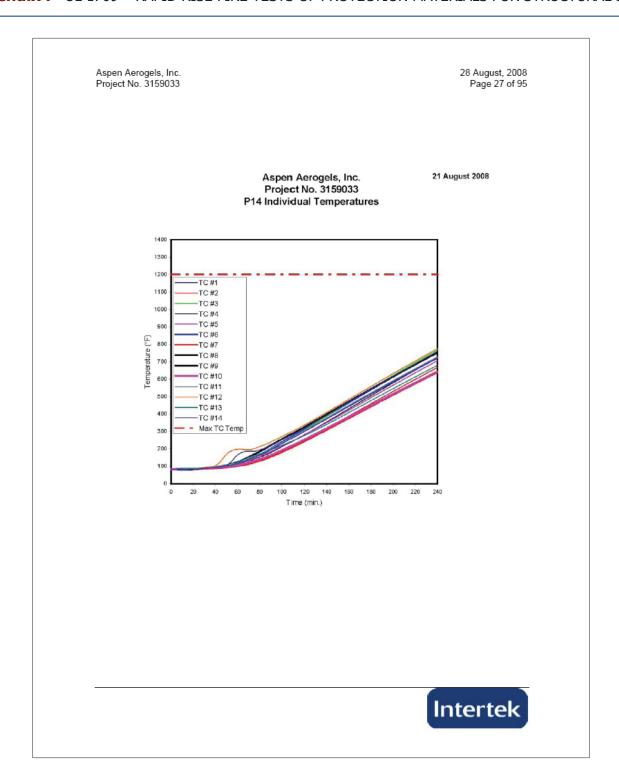
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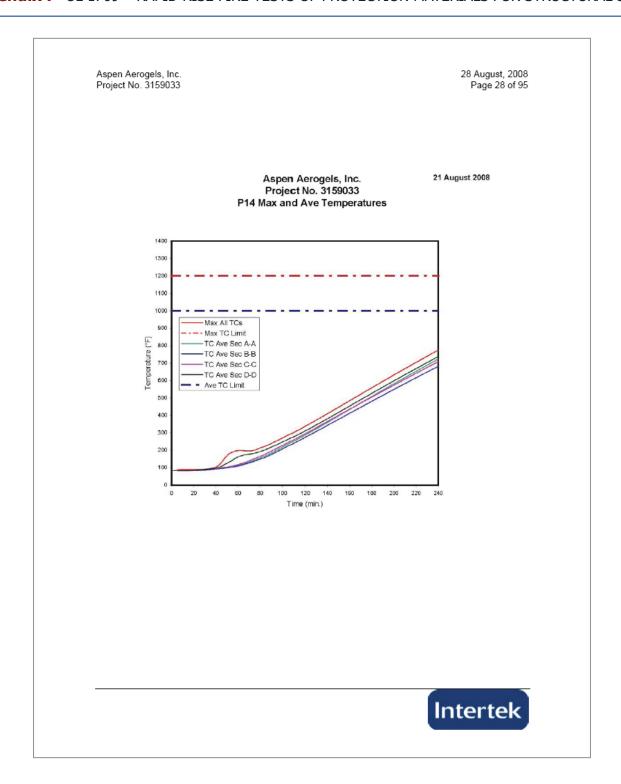
Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL







Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL





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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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21 August 2008

	UL 1709 Std	Furnace	Furnace Probe	Furnace	Furnace	Furnace Probe	Furnace Probe	Furnace Probe	Furnace	Furnace Probe	Furnace
Time	Average	Average	#1	W2	#3	#4	#5	#6	97	#8	1000
(min)	(°F)	(°F)	(°F)	(°F)	(°F)	("F)	(°F)	(°F)	(°F)	(°F)	(°F)
0	100	84	84	84	84	84	84		bad/probe	84	86
1	400	303	321	468	479	250	312		bad/probe	187	169
2	800	531	614	758	698	509	479		bad/probe	386	336
3	1400	990	957	1207	1138	998	937		bed/probe	881	791
4	1885	1457	1385	1590	1490	1484	1455		bad/probe	1429	1342
5	1917 1917	1735 1853	1621	1803 1863	1776 1899	1726	1794 1904		bad/probe bad/probe	1727	1654 1820
7	1917	1927	1851	1932	1975	1912	1974		bad/probe	1941	1903
8	1917	1946	1880	1949	1988	1927	1981		bad/probe	1956	1931
9	1917	1960	1897	1959	2007	1943	1994		bad/probe	1972	1943
10	1917	1960	1903	1987	2016	1939	1987	1956	bad/probe	1965	1944
11	1917	1954	1903	1957	1994	1933	1982	1958	bad/probe	1963	1939
12	1917	1957	1904	1962	2002	1935	1984		bed/probe	1967	1942
13	1917	1951	1897	1962	2004	1926	1980		bad/probe	1956	1938
14	1917	1923	1871	1936	1968	1898	1963		bad/probe	1927	1915
15	1917	1916	1861	1928	1969	1888	1950		bad/probe	1919	1904
16	1917	1912	1880	1922	1972	1886	1943 1942		bad/probe bad/probe	1915	1900
18	1917	1914	1884	1924	1969	1893	1942		bad/probe	1919	1905
19	1917	1922	1873	1933	1974	1899	1949		bad/probe	1929	1910
20	1917	1925	1874	1937	1977	1903	1950		bad/probe	1930	1913
21	1917	1925	1881	1936	1958	1905	1951		bad/probe	1935	1915
22	1917	1922	1879	1933	1953	1900	1951		bad/probe	1930	1912
23	1917	1920	1878	1936	1944	1902	1950	1915	bad/probe	1927	1910
24	1917	1923	1879	1940	1963	1900	1947		bad/probe	1930	1911
25	1917	1926	1886	1938	1954	1905	1952		bed/probe	1933	1914
26	1917	1930	1890	1941	1974	1908	1954		bed/probe	1935	1918
27	1917	1930	1894	1943	1950	1912	1959		bad/probe	1937	1920
28	1917	1923	1887	1940	1948	1904	1950 1947		bad/probe bad/probe	1928	1912
30	1917	1924	1888	1937	1949	1900	1955		bad/probe	1928	1910
31	1917	1923	1890	1937	1943	1903	1949		bad/probe	1928	1911
32	1917	1927	1890	1942	1963	1908	1950		bad/probe	1930	1913
33	1917	1916	1887	1927	1943	1896	1940		bad/probe	1920	1905
34	1917	1907	1878	1923	1927	1886	1932		bad/probe	1911	1895
35	1917	1908	1878	1926	1933	1888	1934	1903	bad/probe	1908	1893
36	1917	1908	1879	1924	1932	1889	1936		bad/probe	1908	1893
37	1917	1909	1883	1925	1931	1891	1935		bad/probe	1911	1894
38	1917	1916	1885	1933	1940	1899	1945		bad/probe	1915	1899
39	1917	1919	1892	1933	1952	1898	1944		bad/probe	1919	1901
40	1917	1921	1891	1941	1949	1904	1944		bad/probe bad/probe	1920	1904
42	1917	1924	1896	1942	1952	1902	1949		bad/probe	1922	1907
43	1917	1926	1898	1942	1942	1908	1954		bed/probe	1925	1910
44	1917	1928	1900	1947	1952	1910	1953		bad/probe	1926	1911
45	1917	1932	1906	1957	1955	1914	1956	1926	bad/probe	1930	1914
46	1917	1935	1910	1951	1968	1915	1960	1927	bad/probe	1931	1917
47	1917	1928	1904	1944	1950	1911	1954		bed/probe	1925	1913
48	1917	1923	1899	1941	1949	1902	1946		bad/probe	1920	1905
49	1917	1919	1897	1937	1944	1900	1943		bad/probe	1915	1902
50	1917	1918	1894	1940	1942	1899	1944		bad/probe	1915	1900
51 52	1917	1918	1896	1938	1936	1900	1942		bad/probe bad/probe	1916	1900
53	1917	1917	1894	1936	1949	1899	1941		bad/probe	1913	1899
54	1917	1918	1895	1941	1948	1894	1942		bad/probe	1911	1897
55	1917	1921	1897	1942	1953	1899	1943		bad/probe	1913	1898
56	1917	1920	1899	1942	1948	1900	1943		bad/probe	1915	1900
57	1917	1921	1900	1941	1945	1902	1944		bad/probe	1918	1901
58	1917	1921	1899	1938	1947	1903	1946		bad/probe	1915	1901
59	1917	1921	1899	1942	1952	1901	1942		bad/probe	1915	1900
60	1917	1920	1899	1945	1942	1900	1944		bad/probe	1915	1899
61	1917	1919	1897	1940	1947	1901	1942		bad/probe	1912	1899
62	1917	1918	1896	1941	1938	1900	1943		bad/probe	1911	1898
63	1917	1919	1898	1942	1941	1901	1942	1917	bad/probe	1915	1899

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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Р	Aspen Aerogel Project No. 31												28 August, 2008 Page 30 of 95
													21 August 2008
	Time (min)	L 1709 Std Average (°F)	Furnace Average (°F)	Furnace Probe #1 (°F)	Furnace Probe #2 (°F)	Furnace Probe #3 (°F)	Furnace Probe #4 ("F)	Furnace Probe #5 (°F)	Furnace Probe #6 (°F)	Furnace Probe #7 (°F)	Furnace Probe #8 (°F)	Furnace Probe #9 (°F)	
	64 65	1917 1917	1921	1900	1944	1950	1902	1943 1942	1912 8	ad/probe	1914	1899	
	66 67	1917 1917	1920 1922	1898	1939 1942	1943 1950	1902	1946 1945 1946	1917 b	ad/probe	1915 1915	1900 1901 1902	
	68 69 70	1917 1917 1917	1922 1923 1923	1902 1904 1902	1942 1943 1941	1942 1947 1950	1908 1907 1906	1947 1947	1917 b	ad/probe ad/probe	1918 1918 1916	1902 1905	
	71 72	1917 1917	1923 1921	1900	1947 1942	1942 1943	1906	1950 1945	1915 b	ad/probe	1917 1914	1906	
	73 74 75	1917 1917 1917	1918 1916 1918	1899 1896 1895	1941 1941 1940	1941 1932 1955	1898 1898 1899	1942 1943 1941	1910 t	ad/probe ad/probe ad/probe	1911 1910 1910	1899 1898 1898	
	76 77	1917 1917	1917 1916	1897 1897	1937 1936	1937 1944	1899 1898	1942	1917 E	ad/probe	1910 1908	1897 1895	
	78 79 80	1917 1917 1917	1914 1915 1916	1895 1893 1895	1931 1936 1939	1935 1942 1945	1897 1898 1898	1940 1939 1939	1909 6	ad/probe ad/probe ad/probe	1909 1908 1907	1893 1893 1893	
	81 82	1917	1915	1896	1935	1939	1899	1938	1907 b	ad/probe	1909	1894	
	83 84	1917 1917	1917 1916	1895 1896	1938 1939	1944 1941	1901 1899	1941 1941	1912 b	ad/probe	1908 1908	1894 1894	
	85 86 87	1917 1917 1917	1916 1918	1892 1894 1896	1940 1941 1941	1942 1935 1948	1898 1902 1901	1941 1940 1943	1912 b	ad/probe ad/probe ad/probe	1907 1909 1909	1894 1894 1896	
	88 89	1917 1917	1919 1918	1898 1898	1942 1942	1947 1938	1901 1902	1942 1943	1911 b	ad/probe	1912 1911	1896 1897	
	90 91 92	1917 1917 1917	1919 1918 1920	1898 1898 1898	1941 1939 1943	1946 1945 1938	1901 1902 1905	1944 1942 1945	1912 8	ad/probe ad/probe	1911 1911 1913	1897 1897 1899	
	93 94	1917	1922	1902	1945 1944	1941	1905	1948	1917 b	ad/probe	1916	1901	
	95 96	1917 1917	1922 1922	1902 1903	1943 1941	1947 1957	1904 1904	1948 1946	1918 b	ad/probe	1915 1914	1900 1899	
	97 98 99	1917 1917 1917	1922 1921 1923	1903 1901 1904	1940 1938 1947	1945 1945 1942	1906 1905 1907	1948 1947 1948	1917 b	ad/probe ad/probe ad/probe	1915 1914 1914	1900 1900 1902	
	100 101	1917 1917	1924 1921	1905	1944 1942	1954 1946	1905 1905	1947 1946	1919 b	ad/probe	1915 1913	1901 1901	
	102 103 104	1917 1917 1917	1922 1920 1921	1901 1899 1899	1942 1944 1941	1949 1947 1956	1905 1904 1904	1945 1944 1945	1912 b	ad/probe ad/probe	1914 1912 1913	1901 1900 1900	
	105 106	1917 1917	1920	1901	1941	1943 1945	1906	1943 1944	1917 b	ad/probe	1912 1913	1900	
	107 108	1917 1917	1922 1924	1903 1904	1941 1944	1951 1955	1907 1908	1945 1948	1920 B	ed/probe	1914 1916	1901 1902	
	109 110 111	1917 1917 1917	1923 1920 1921	1904 1902 1901	1943 1939 1939	1948 1940 1943	1907 1906 1905	1950 1943 1946	1915 b	ad/probe ad/probe ad/probe	1916 1913 1914	1903 1901 1901	
	112 113	1917 1917	1921	1901	1943 1940	1941 1946	1905	1944 1946	1918 b	ad/probe	1913 1913	1900 1899	
	114 115 116	1917 1917 1917	1919 1918 1918	1901 1900 1901	1941 1938 1936	1938 1938 1940	1904 1903 1904	1943 1942 1941	1911 8	ad/probe	1911 1911 1910	1899 1898 1899	
	117 118	1917	1920	1901	1939 1939	1946 1944	1906	1943	1917 b	ad/probe ad/probe ad/probe	1911	1900 1899	
	119 120	1917 1917	1922 1920	1900	1938	1957 1938	1904 1905	1947 1944	1915 b	ad/probe	1913 1915	1900 1901	
	121 122 123	1917 1917 1917	1921 1922 1922	1904 1903 1905	1938 1940 1940	1947 1951 1943	1908 1908 1908	1945 1945 1947	1915 b	ad/probe ad/probe ad/probe	1913 1913 1916	1901 1901 1902	
	124 125	1917 1917	1924 1925	1904 1906	1942 1943	1949 1949	1909 1910	1947 1949	1919 b	ad/probe	1918 1918	1903 1906	
	126 127	1917 1917	1923 1921	1905 1903	1942 1939	1949 1943	1906 1907	1946 1946	1916 b	ad/probe	1915 1916	1903 1902	
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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	UL 1709 Std		Furnace Probe	Furnace Probe	Furnace Probe						
Time	Average	Average	#1	W2	#3	#4	#5	#6	97	#8	#9
(min)	(°F)	(°F)	(°F)	(°F)	(°F)	("F)	(°F)	(°F)	(°F)	(°F)	(ok)
128	1917	1924	1905	1940	1956	1906	1947		bad/probe	1915	1903
129	1917	1922	1903	1941	1943	1908	1947		bed/probe	1917	1903
130	1917	1923	1903	1939	1947	1908	1945		bad/probe	1918	1903
131	1917	1923	1904	1939	1947	1907	1946		bed/probe	1916	1903
132	1917	1924	1905	1940	1945	1910	1947		bad/probe	1920	1905
133	1917	1924	1907	1939	1944	1910	1947 1947		bad/probe	1919	1905
134 135	1917 1917	1924 1926	1907	1937	1945 1952	1909	1947		bad/probe bad/probe	1919	1905
136	1917	1924	1912	1956	1948	1905	1942		bad/probe	1911	1900
137	1917	1924	1914	1953	1947	1902	1942		bad/probe	1912	1898
138	1917	1925	1915	1957	1954	1906	1942		bad/probe	1911	1900
139	1917	1921	1912	1949	1946	1901	1938		bad/probe	1910	1897
140	1917	1918	1910	1954	1938	1897	1935	1909	bad/probe	1906	1893
141	1917	1916	1903	1953	1943	1893	1932	1909	bad/probe	1902	1890
142	1917	1914	1904	1947	1933	1894	1933	1905	bad/probe	1903	1890
143	1917	1914	1901	1958	1931	1893	1932		bad/probe	1900	1889
144	1917	1912	1901	1948	1932	1893	1931		bad/probe	1901	1888
145	1917	1913	1902	1950	1928	1895	1932		bad/probe	1902	1889
146	1917	1915 1915	1903	1953	1935 1935	1893 1895	1934		bad/probe	1903	1891
147	1917	1914	1905	1955	1935	1894	1931		bad/probe bad/probe	1902	1889
149	1917	1913	1901	1957	1933	1893	1930		bad/probe	1902	1889
150	1917	1915	1904	1952	1945	1893	1932		bad/probe	1902	1889
151	1917	1917	1905	1953	1943	1895	1934		bad/probe	1904	1891
152	1917	1918	1906	1959	1945	1895	1934		bad/probe	1903	1891
153	1917	1916	1905	1953	1938	1896	1932		bed/probe	1903	1891
154	1917	1917	1906	1955	1942	1895	1933	1909	bed/probe	1904	1892
155	1917	1917	1907	1959	1935	1896	1935	1910	bad/probe	1903	1891
156	1917	1917	1904	1956	1935	1898	1934		bad/probe	1905	1892
157	1917	1919	1906	1956	1943	1897	1935		bad/probe	1904	1893
158	1917	1917	1906	1967	1941	1898	1934		bed/probe	1904	1892
159	1917	1918	1909	1968	1936	1897	1935		bad/probe	1905	1893
160	1917	1920	1909	1955 1965	1951 1948	1897	1935 1936		bad/probe	1905	1894 1894
161	1917 1917	1920 1920	1907 1910	1965	1943	1900	1930		bad/probe bad/probe	1906	1895
163	1917	1920	1909	1955	1948	1898	1937		bad/probe	1908	1895
164	1917	1919	1912	1945	1946	1899	1937		bed/probe	1907	1896
165	1917	1920	1911	1949	1947	1899	1937		bad/probe	1907	1895
186	1917	1922	1910	1985	1944	1902	1939		bad/probe	1909	1896
167	1917	1920	1908	1957	1942	1899	1938	1911	bad/probe	1907	1896
168	1917	1922	1908	1959	1949	1902	1939	1915	bad/probe	1909	1897
169	1917	1923	1912	1986	1950	1900	1938		bad/probe	1910	1897
170	1917	1923	1912	1965	1945	1902	1939		bad/probe	1910	1899
171	1917	1919	1910	1955	1944	1898	1935		bed/probe	1907	1895
172	1917	1917	1906 1904	1957 1954	1941	1895	1933		bad/probe	1904	1892 1889
173 174	1917	1914	1904	1954	1943	1894	1929		bad/probe bad/probe	1901	1889
175	1917	1913	1905	1944	1943	1894	1929		bed/probe	1900	1889
176	1917	1915	1905	1958	1938	1891	1931		bad/probe	1903	1889
177	1917	1915	1903	1951	1942	1894	1933		bed/probe	1903	1890
178	1917	1914	1904	1958	1924	1896	1933		bad/probe	1904	1891
179	1917	1917	1905	1955	1942	1896	1932	1907	bad/probe	1904	1891
180	1917	1915	1906	1953	1933	1895	1931	1906	bad/probe	1904	1891
181	1917	1917	1906	1958	1944	1895	1933		bad/probe	1905	1892
182	1917	1917	1907	1950	1944	1898	1933		baid/probe	1905	1894
183	1917	1919	1906	1956	1944	1899	1934		bad/probe	1906	1894
184	1917	1917	1909	1951	1938	1897	1934		bad/probe	1905	1894
185	1917	1919	1906	1959	1940	1899	1937		bad/probe	1907	1895
196 187	1917 1917	1920 1917	1908	1957	1948 1951	1899	1936		bad/probe bad/probe	1906	1895 1894
188	1917	1917	1909	1939	1951	1899	1934		bad/probe	1906	1894
189	1917	1921	1907	1969	1948	1896	1934		bad/probe	1907	1894
190	1917	1918	1907	1952	1937	1900	1934		bad/probe	1908	1895
191	1917	1919	1910	1947	1945	1901	1935		bad/probe	1908	1896





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Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerogels, Inc. 28 August, 2008 Project No. 3159033 Page 32 of 95 21 August 2008 Probe #3 (°F) Furnace Probe #9 (°F) Probe #5 (°F) Probe #4 ("F) 1908 bad/grobe 1907 bad/grobe 1907 bad/grobe 1907 bad/grobe 1908 bad/grobe 1903 bad/grobe 1903 bad/grobe 1903 bad/grobe 1904 bad/grobe 1904 bad/grobe 1907 bad/grobe 1907 bad/grobe 1907 bad/grobe 1908 bad/grobe 1908 bad/grobe 1909 bad/grobe 1908 bad/grobe 1909 bad/grobe 1909 bad/grobe 1909 bad/grobe 1909 bad/grobe 1909 bad/grobe 1937 bad/probe 1938 bad/probe 1938 bad/probe 1939 bad/probe 1938 bad/probe 1939 bad/probe 1940 bad/probe 1940 bad/probe 1934 bad/probe 1932 bad/probe 1930 bad/probe 1933 bad/probe 1933 bad/probe 1830 beddyrobe 1930 beddyrobe 1931 beddyrobe 1931 beddyrobe 1932 beddyrobe 1933 beddyrobe 1933 beddyrobe 1934 beddyrobe 1934 beddyrobe 1934 beddyrobe 1934 beddyrobe 1935 beddyrobe 1936 beddyrobe 1936 beddyrobe 1936 beddyrobe

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Part
1 83 83 83 83 83 83 83 83 83 83 83 83 82 83 83 83 82 83 83 84 82 83 83 84 82 83 83 84 82 83 84 83 84 83 83 83 83 83 83 83 84 82 83 83 84 82 83 84 84 82 83 84 84 84 82 84 84 84 84 84 84 84 84 84 84 84 84 84
51 920 767 863 580 930 7754 720 789 862 590 916 750 bedde 52 893 767 733 803 876 803 8976 803 897 763 bedde 53 948 703 800 604 948 780 767 733 803 876 803 897 777 bedde 54 802 605 8976 819 910 628 972 806 771 843 817 049 971 603 bedde 56 876 819 910 628 972 806 771 843 817 049 971 603 bedde 57 1004 843 941 651 997 831 796 869 944 869 988 829 bedde 59 1001 867 997 674 1021 855 620 894 818 978 1021 842 bedde 59 1031 867 822 808 831 957 678 1011 842 bedde 59 1031 867 822 808 831 957 678 1011 842 bedde 59 1031 867 822 808 887 997 898 999 809 808 828 848 848 848 848 848 848 848 848 84



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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aeroge Project No. 3													28 August, 2 Page 34 c	
												21	August 2008	
Time (min)	P2 P2Max (*F)	P2 AAAve (*F)	P2 Sec A-A TC #1 (*F)	P2 Sec A-A TC #2 (*F)	P2 Sec A-A TC #3 (°F)	P2 Sec A-A TC #4 (*F)	P2 Sec A-A TC #5 (*F)	P2 BBAve (°F)	P2 Sec B-B TC #6 (°F)	P2 Sec B-B TC #7 (°F)	P2 Sec B-B TC #8 (°F)	P2 CCAve (°F)	P2 Sec C-C TC #9 (°F)	
64 65 66 67 68	1095 1107 1119 1132 1143	926 938 949 960 971	1029 1040 1052 1064 1078	730 741 761 762 773	1080 1091 1102 1113 1124	914 925 936 948 969	879 801 903 914 925	954 966 978 989	1033 1045 1057 1089 1081	745 756 767 778 789	1085 1097 1110 1121 1133	916 927 939 951 962	badAc badAc badAc badAc badAc	
69 70 71 72	1156 1167 1179 1190	982 993 1004 1015	1088 1100 1111 1123	783 793 804 814	1134 1145 1155 1168	969 980 991 1001	937 948 959 970	1012 1023 1035 1045	1092 1104 1116 1127	810 821 831	1144 1156 1167 1178	974 985 997 1007	badAc badAc badAc badAc	
73 74 75 76	1202 1213 1223 1234 1245	1025 1036 1046 1056 1066	1134 1145 1156 1167 1177	824 834 844 854 864	1176 1188 1195 1205 1214	1012 1022 1032 1042 1062	981 992 1003 1013 1024	1056 1067 1077 1087 1098	1138 1149 1159 1170 1180	842 852 862 872 883	1189 1199 1209 1220 1230	1018 1029 1039 1050 1061	badific badific badific badific	
78 79 80 81	1255 1265 1275 1284	1076 1086 1095 1105	1188 1198 1208 1218	873 883 892 902	1223 1232 1241 1250	1061 1071 1080 1090	1034 1044 1054 1064	1107 1117 1127 1136	1190 1200 1209 1219	902 912 921	1240 1249 1259 1268	1071 1081 1091 1100	bedito bedito bedito	
82 83 84 85	1294 1303 1312 1321 1329	1114 1124 1132 1141 1150	1228 1238 1247 1250 1268	911 920 929 938 947	1259 1268 1275 1285 1293	1108 1117 1125 1134	1074 1084 1093 1103 1112	1145 1166 1164 1173 1182	1228 1238 1247 1256 1265	931 940 950 959 958	1277 1286 1295 1304 1312	1110 1119 1128 1138 1146	badAc badAc badAc badAc badAc	
87 88 89 90 91	1336 1343 1350 1357 1365	1159 1168 1177 1185 1193	1274 1283 1292 1301 1309	966 965 974 962 991	1302 1310 1318 1326 1333	1143 1151 1160 1168 1178	1121 1130 1139 1148 1157	1190 1198 1206 1213 1221	1274 1282 1291 1299 1308	977 988 995 1004 1013	1320 1326 1332 1337 1342	1154 1163 1171 1179 1187	badāc badāc badāc badāc badāc	
92 93 94 95	1373 1381 1389 1397	1202 1209 1217 1224	1318 1326 1333 1340	1008 1008 1016 1025	1340 1348 1352 1358	1184 1192 1199 1207	1166 1174 1183 1191	1228 1236 1244 1252	1316 1324 1331 1338	1021 1030 1038 1047	1348 1355 1382 1370	1196 1204 1212 1221	badito badito badito badito	
96 97 38 99 100	1405 1413 1421 1430 1438	1232 1239 1248 1254 1260	1347 1353 1359 1366 1372	1033 1042 1060 1068 1066	1365 1371 1377 1384 1390	1215 1222 1230 1237 1244	1199 1207 1215 1223 1230	1259 1266 1273 1280 1287	1344 1349 1355 1361 1367	1055 1064 1072 1080 1088	1377 1384 1391 1399 1406	1229 1238 1246 1255 1263	badito badito badito badito badito	
101 102 103 104 105	1447 1465 1463 1471 1480	1268 1274 1261 1288 1296	1379 1385 1391 1398 1406	1074 1082 1090 1098 1106	1398 1403 1409 1416 1423	1251 1257 1264 1270 1277	1238 1245 1253 1259 1267	1295 1302 1309 1316 1324	1373 1379 1385 1391 1398	1097 1105 1113 1121 1129	1414 1422 1430 1437 1445	1272 1280 1289 1297 1306	badAc badAc badAc badAc badAc	
106 107 108 109	1488 1496 1504 1512	1302 1309 1316 1322	1412 1419 1426 1433	1114 1122 1130 1137	1429 1436 1443 1450	1283 1289 1295 1300	1273 1280 1287 1292	1332 1339 1346 1354	1405 1411 1418 1425	1137 1145 1153 1161	1453 1460 1468 1476	1314 1322 1330 1339	badito badito badito badito	
110 111 112 113 114	1520 1527 1535 1542 1550	1329 1336 1342 1348 1354	1440 1447 1454 1461 1467	1145 1153 1160 1168 1175	1457 1464 1470 1476 1483	1306 1311 1316 1321 1328	1299 1304 1310 1316 1321	1361 1368 1376 1383 1390	1432 1430 1447 1453 1460	1169 1176 1184 1191 1199	1483 1490 1498 1505 1512	1347 1354 1362 1370 1378	badAc badAc badAc badAc badAc	
115 116 117 118 119	1567 1564 1571 1578 1586	1361 1367 1372 1379 1384	1474 1480 1487 1494 1500	1183 1190 1197 1204 1211	1489 1496 1502 1508 1514	1331 1336 1340 1346 1351	1326 1331 1336 1341 1346	1397 1405 1411 1418 1425	1467 1474 1481 1487 1494	1207 1214 1221 1228 1235	1518 1526 1532 1539 1546	1385 1393 1400 1407 1415	badde badde badde badde badde	
120 121 122 123	1593 1601 1608 1615	1390 1397 1403 1409	1508 1513 1519 1525	1218 1225 1232 1239	1521 1527 1533 1539	1357 1364 1370 1370	1350 1356 1362 1368	1431 1438 1445 1452	1500 1507 1513 1520	1242 1249 1258 1202	1552 1559 1566 1573	1422 1429 1436 1443	bedito bedito bedito	
124 125 126 127	1623 1631 1640 1647	1418 1422 1429 1435	1531 1538 1544 1550	1246 1262 1268 1264	1545 1551 1557 1563	1383 1390 1398 1405	1375 1381 1387 1395	1459 1466 1472 1479	1526 1533 1539 1545	1299 1276 1282 1289	1581 1588 1595 1603	1451 1458 1466 1473	bedAc bedAc bedAc bedAc	
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Ae Project N															ugust, 2 ge 35 d	
													21	August 20	108	
	Time (min)	P2 P2Max (*F)	P2 AAAve (°F)	P2 Sec A-A TC #1 (*F)	P2 Sec A-A TC #2 (*F)	P2 Sec A-A TC #3 (°F)	P2 Sec A-A TC #4 (*F)	P2 Sec A-A TC #5 (*F)	P2 BBAve (°F)	P2 Sec B-B TC #6 (°F)	P2 Sec B-B TC #7 (°F)	P2 Sec B-B TC #8 (°F)	P2 CCAve (°F)	P2 Sec C-C TC #9 (°F)		
	128 129 130 131	1663 1661 1669 1676	1442 1449 1455 1482	1558 1562 1568 1574	1271 1277 1283 1289	1589 1575 1581 1587	1412 1420 1427 1434	1401 1409 1416 1424	1485 1492 1498 1505	1551 1557 1563 1570	1295 1301 1307 1312	1610 1617 1624 1632	1479 1486 1493 1499	badito badito badito badito		
	132 133 134 135	1683 1689 1697 1705	1468 1475 1481 1488	1580 1587 1593 1800	1294 1300 1305 1311	1594 1601 1607 1614	1441 1448 1455 1462	1431 1438 1445 1452	1511 1517 1523 1529	1576 1583 1590 1596	1317 1322 1327 1332	1639 1646 1653 1680	1505 1510 1517 1523	badito badito badito badito		
	136 137 138	1712 1718 1725	1494 1500 1508	1607 1513 1620	1316 1321 1325	1620 1625 1632	1469 1476 1482	1459 1466 1473	1535 1541 1547	1603 1610 1617	1338 1340 1344	1686 1673 1679	1534 1540	bad/to bad/to bad/to		
	139 140 141 142	1731 1737 1743 1748	1513 1519 1624 1530	1626 1633 1639 1644	1330 1334 1338 1342	1639 1644 1650 1655	1489 1496 1602 1509	1479 1486 1492 1499	1552 1558 1565 1571	1630 1636 1642	1348 1354 1361 1369	1685 1691 1697 1702	1546 1553 1560 1567	bedAc bedAc bedAc bedAc		
	143 144 145	1763 1759 1765	1535 1541 1546	1650 1655 1661	1345 1349 1353	1661 1663 1671	1615 1522 1528	1505 1511 1518	1577 1584 1590	1648 1654 1660	1377 1385 1393	1707 1712 1718	1573 1581 1589	bad/to bad/to bad/to		
	146 147 148 149	1768 1774 1780 1762	1552 1568 1564 1570	1687 1672 1677 1683	1369 1365 1372 1378	1677 1682 1687 1692	1534 1641 1547 1554	1524 1530 1537 1543	1597 1604 1610 1617	1686 1671 1677 1682	1402 1412 1421 1431	1723 1728 1733 1738	1595 1604 1612 1617	badAc badAc badAc badAc		
	150 151 152 153	1789 1792 1798 1801	1576 1582 1589 1595	1688 1894 1699 1704	1386 1392 1400 1408	1697 1702 1707 1712	1561 1568 1575 1582	1550 1556 1563 1571	1624 1631 1637 1643	1688 1694 1699 1704	1440 1450 1459	1743 1748 1753	1626 1632 1640 1646	bed/to bed/to bad/to		
	154 155 156	1806 1810 1814	1602 1608 1615	1709 1714 1719	1416 1424 1432	1717 1722 1727	1589 1598 1604	1578 1585 1593	1650 1656 1662	1710 1715 1720	1468 1477 1486 1495	1757 1762 1767 1771	1653 1660 1666	bed/fc bed/fc bed/fc		
	157 158 159 160	1818 1821 1826 1829	1621 1628 1634 1640	1724 1729 1734 1738	1440 1449 1467	1732 1738 1741 1745	1611 1617 1624 1631	1600 1607 1615 1622	1688 1674 1680 1686	1726 1730 1736 1741	1503 1512 1521 1529	1778 1780 1784 1788	1673 1679 1685 1691	bedåc bedåc bedåc badåc		
	161 162 163	1833 1836 1838	1646 1652 1658	1743 1748 1752	1473 1480 1488	1750 1754 1759	1637 1644 1650	1629 1636 1643	1692 1697 1703	1746 1750 1755	1537 1546 1555	1792 1796 1800	1697 1703 1709	bedAc bedAc bedAc		
	164 165 166 167	1840 1844 1848 1849	1664 1670 1676 1681	1757 1761 1765 1769	1496 1504 1511 1519	1763 1767 1771 1775	1656 1662 1668 1673	1650 1656 1663 1669	1709 1715 1721 1727	1760 1764 1769 1773	1564 1574 1584 1594	1804 1808 1811 1814	1715 1722 1729 1735	bed/to bed/to bed/to		
	168 169 170	1862 1868 1868	1688 1692 1697	1773 1778 1782	1526 1534 1541	1779 1783 1787	1679 1685 1690 1695	1675 1681 1687	1733 1739 1745	1777 1782 1786 1790	1605 1615 1624	1818 1821 1824	1741 1748 1753 1758	bed/to bed/to bed/to		
	171 172 173 174	1859 1860 1860 1861	1703 1707 1712 1717	1785 1788 1791 1794	1548 1566 1564 1572	1791 1794 1797 1800	1700 1704 1709	1694 1699 1705 1710	1750 1756 1760 1764	1794 1797 1800	1634 1643 1651 1659	1827 1830 1831 1834	1762 1766 1770	bed/to bed/to bed/to		
	175 176 177 178	1863 1865 1866 1868	1722 1728 1732 1737	1796 1799 1802 1805	1581 1590 1600 1609	1802 1805 1808 1811	1714 1718 1723 1728	1715 1720 1726 1731	1769 1774 1778 1782	1804 1807 1810 1813	1688 1676 1684 1692	1835 1838 1840 1842	1774 1779 1783 1787	bed/to bed/to bed/to bad/to		
	179 180 181	1869 1883 1899	1742 1761 1769	1807 1883 1890	1619 1628 1637	1814 1817 1819	1733 1737 1742	1735 1740 1746	1787 1791 1795	1816 1819 1822	1700 1707 1714	1844 1846 1848	1791 1795 1799	badite badite badite		
	182 183 184 185	1901 1902 1904 1905	1773 1777 1782 1786	1901 1902 1904 1905	1645 1654 1661 1669	1825 1825 1828 1830	1748 1751 1755 1759	1750 1755 1780 1785	1799 1803 1807 1811	1825 1828 1831 1834	1722 1729 1735 1742	1851 1852 1855 1857	1803 1807 1810 1814	badAc badAc badAc badAc		
	196 187 188	1908 1908 1909	1790 1794 1798	1906 1908 1909	1677 1685 1692	1833 1835 1838	1764 1769 1772	1769 1774 1778	1814 1818 1822	1837 1839 1842	1748 1754 1761	1858 1860 1862	1817 1820 1824	badAc badAc badAc		
	189 190 191	1910 1911 1912	1801 1805 1809	1910 1911 1912	1699 1706 1713	1840 1842 1844	1776 1780 1784	1782 1786 1790	1825 1828 1831	1844 1846 1849	1766 1772 1777	1864 1865 1867	1827 1830 1833	bad/to bad/to bad/to		
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aeroge Project No. 31														ugust, 2008 age 36 of 95
												21	August 2	008
Time (min)	P2 P2Max (*F)	P2 AAAve (°F)	P2 Sec A-A TC #1 (*F)	P2 Sec A-A TC #2 (*F)	P2 Sec A-A TC #3 (°F)	P2 Sec A-A TC #4 (*F)	P2 Sec A-A TC #5 (*F)	P2 BBAve (°F)	P2 Sec B-B TC #6 (°F)	P2 Sec B-B TC #7 (°F)	P2 Sec B-B TC #8 (°F)	P2 CCAve (°F)	P2 Sec C-C TC #9 (°F)	
192 193 194	1913 1915 1915	1812 1816 1819	1913 1915 1915	1720 1726 1732	1847 1849 1850	1788 1792 1795	1794 1798 1802	1834 1836 1839	1851 1853 1856	1781 1786 1790	1869 1870 1871	1836 1839 1842	badAc badAc badAc	
195 196 197 198	1917 1918 1919 1920	1823 1826 1829 1832	1917 1918 1919 1920	1739 1744 1750 1756	1853 1855 1857 1859	1799 1803 1807 1810	1805 1809 1813 1816	1844 1846 1848	1857 1859 1861 1863	1794 1797 1800 1803	1873 1875 1876 1877	1845 1848 1851 1855	bedAc bedAc bedAc badAc	
199 200 201	1921 1922 1923	1835 1839 1842	1921 1922 1923	1762 1767 1773	1861 1863 1865	1813 1817 1820	1820 1824 1827	1850 1852 1854	1865 1866 1868	1808 1809 1812	1878 1890 1881	1857 1860 1863	badite badite	
202 203 204 205	1924 1925 1927 1928	1844 1847 1850 1853	1924 1925 1927 1928	1778 1783 1788 1793	1868 1868 1870 1872	1823 1826 1829 1833	1830 1833 1837 1840	1856 1857 1859 1861	1870 1871 1873 1875	1815 1817 1820 1823	1883 1884 1885 1886	1866 1868 1870 1873	badAc badAc badAc	
206 207 208	1928 1929 1930	1858 1858 1881	1928 1929 1930	1798 1803 1808	1874 1875 1877	1836 1839 1841	1843 1846 1849	1863 1865 1867	1876 1878 1879	1825 1828 1831	1887 1889 1890	1875 1877 1879	bed/to bed/to	
209 210 211 212	1931 1931 1932 1933	1864 1866 1869 1871	1931 1931 1932 1933	1812 1817 1822 1827	1879 1880 1882 1884	1844 1847 1860 1853	1852 1854 1857 1860	1868 1870 1871 1873	1880 1882 1883 1884	1833 1835 1838 1840	1891 1892 1893 1894	1883 1885 1887	badite badite badite	
213 214 215 216	1933 1934 1934 1935	1874 1876 1878 1881	1933 1934 1934 1935	1832 1836 1841 1846	1885 1887 1888 1889	1855 1858 1860 1863	1863 1865 1868 1870	1874 1876 1877 1878	1885 1887 1888 1889	1842 1845 1847 1849	1895 1895 1896 1896	1888 1890 1892 1893	badAc badAc badAc	
217 218 219	1936 1936 1938	1883 1885 1889	1936 1936 1938	1851 1856 1861	1891 1892 1894	1868 1868 1872	1873 1875 1878	1879 1881 1882	1890 1891 1892	1851 1853 1855	1897 1898 1899	1895 1896 1898	bedAc bedAc bedAc	
220 221 272 273	1939 1940 1940 1940	1891 1893 1895 1897	1939 1940 1940 1940	1866 1871 1876 1881	1895 1897 1898 1899	1874 1877 1879 1882	1880 1881 1883 1885	1883 1884 1885 1886	1893 1893 1894 1894	1857 1859 1861 1864	1900 1900 1900 1900	1889 1900 1901 1902	badito badito badito badito	
224 225 226 227	1941 1941 1942 1942	1900 1902 1904 1908	1941 1941 1942 1942	1895 1899	1900 1902 1903 1904	1885 1887 1890 1892	1887 1889 1891 1892	1887 1888 1889 1890	1895 1895 1896 1896	1866 1868 1870 1872	1900 1900 1900 1901	1903 1904 1905 1906	badito badito badito	
228 229 230 231	1943 1943 1943 1944	1908 1909 1910 1912	1943 1943 1944	1903 1908 1908 1910	1905 1908 1907 1907	1894 1896 1897 1899	1894 1895 1897 1898	1891 1892 1893 1894	1897 1898 1899 1899	1874 1877 1879 1881	1901 1902 1902 1903	1907 1908 1908 1909	bedito bedito bedito bedito	
232 233 234	1944 1945 1945	1913 1914 1915	1944 1945 1945	1912 1913 1915	1908 1909 1910	1900 1901 1902	1900 1901 1902	1895 1896 1897	1900 1900 1901	1883 1884 1896	1903 1903 1904	1910 1911 1912	bad/to bad/to bad/to	
235 236 237 238	1945 1946 1945 1946	1915 1916 1917 1918	1945 1945 1945 1946	1916 1917 1918 1918	1910 1911 1911 1912	1903 1904 1905 1906	1903 1904 1905 1908	1898 1898 1899 1900	1902 1902 1903 1903	1887 1888 1890 1891	1904 1904 1905 1905	1912 1913 1913	bedito bedito bedito	
239 240 Max To	1946 1946	1918 1919 1919	1948 1948	1919 1920 1920	1912 1913 1913	1907 1907 1907	1907 1908 1908	1901 1901	1904 1904	1892 1893 1893	1906 1906 1908	1914 1914 1914	badite badite	
Max A	1200	1000	1200	1200	1200	1200	1200	1000	1200	1200	1200	1000	1200	



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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

	21 August 2008
P2 P3 P2 P3	P5 P5 P5 P5 P5 P5 Sec A-A Sec A-A Sec A-A Sec A-A P5Max AAAva TC #1 TC #2 TC #3 TC #4 (*F) (*F) (*F) (*F) (*F) (*F)
0 82 83 83 baditc 83 83 1 82 82 83 baditc 83 83 2 83 83 83 baditc 83 83 3 83 83 83 baditc 83 83	82 81 81 81 81 81 81 82 81 81 81 81 81 81 82 81 81 81 82 81 82 81 81 81 82 81
4 85 85 84 baditc 82 85 5 83 88 85 baditc 81 89 6 84 97 88 baditc 81 95 7 84 113 98 baditc 82 110 8 85 135 108 baditc 82 120	82 81 81 81 81 82 83 81 81 81 81 81 81 83 82 82 81 81 82 85 82 83 81 82 82 87 84 85 81 85 84
9 87 159 117 badht 84 150 10 89 180 128 badht 87 169 11 93 205 139 badht 91 187 12 98 233 152 badht 93 207	90 86 88 82 87 86 93 87 90 81 90 86 97 89 93 82 93 88 103 91 97 83 97 80
14 111 283 180 bas/ltc 110 249 16 119 305 194 bas/ltc 118 269 16 128 327 208 bas/ltc 128 289 17 137 247 221 bas/ltc 125 307	118 99 108 84 110 96 126 104 116 86 118 100 134 110 124 87 127 105 143 116 133 89 136 110
18 147 397 235 badlic 144 325 19 167 388 249 badlic 165 343 20 168 408 233 badlic 165 381 21 100 429 278 badlic 175 379 22 192 448 293 badlic 188 398	151 123 142 92 145 117 168 129 151 94 164 122 165 136 159 88 162 130 172 142 166 101 170 136 181 149 174 105 179 142
23 204 487 308 baditc 240 417 24 218 483 323 baditc 211 435 25 229 500 338 baditc 224 453 26 242 518 354 baditc 234 471 27 256 535 370 baditc 249 490	190 157 184 110 188 149 199 163 190 114 197 155 208 171 203 119 207 161 217 170 212 134 217 168
28 269 553 385 bas/lfc 262 508 29 262 570 401 bas/lfc 275 526 30 296 567 416 bas/lfc 288 544 31 310 605 432 bas/lfc 301 562	236 194 230 135 236 183 245 202 239 141 245 191 254 210 248 147 254 198 264 218 257 153 284 206
33 337 659 462 best/lic 327 597 34 361 665 478 bast/lic 341 614 35 365 671 492 bast/lic 354 630 36 379 687 507 bast/lic 367 646	282 234 274 166 282 221 291 242 283 172 291 229 300 250 292 179 300 237 309 258 300 186 309 244
38 407 718 537 bad/fit 394 679 39 421 734 551 bad/fit 407 695 40 434 750 598 bad/fit 420 711 41 448 798 581 bad/fit 434 727	318 286 309 183 318 285 327 274 317 200 327 280 335 282 325 207 335 288 344 290 334 214 344 276 352 298 343 221 352 283
42 462 782 598 badite 447 744 43 475 797 810 badite 447 760 44 489 813 625 badite 473 776 45 502 829 639 badite 473 776 46 515 044 653 badite 488 807 47 528 889 687 badite 518 823	361 306 351 228 361 281 370 314 360 236 370 256 379 322 388 243 379 306 388 330 377 250 388 314 396 338 385 258 396 322
47 528 880 857 badite 511 823 48 541 878 882 badite 524 839 49 564 891 898 badite 538 854 50 567 905 708 badite 549 808 51 580 500 722 badete 561 883	405 947 304 285 405 330 415 355 403 273 414 338 424 383 412 280 423 345 433 371 420 287 422 354 441 379 428 295 440 362
52 592 934 736 bad/lc 574 897 53 805 948 740 bad/lc 598 911 54 817 882 782 bad/lc 588 925	450 388 438 302 449 370 450 306 448 310 458 377 468 404 454 317 460 380 477 412 463 325 475 394
95 929 976 779 bad/tc 610 939 56 841 990 787 bad/tc 621 952 57 854 1004 800 bad/tc 623 956 58 868 1017 812 bad/tc 645 979 59 978 1051 825 bad/tc 657 992 60 990 1044 637 bad/tc 665 1005	485 420 471 332 494 401 484 428 480 340 492 410 503 437 489 347 501 418 511 445 487 355 510 420 520 453 505 382 516 434
81 701 1057 840 badite 679 1018 82 713 1070 881 badite 691 1031 63 724 1082 873 badite 702 1043	529 461 514 370 527 442 538 480 523 377 536 450 546 477 531 385 545 458
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

P2	of 95
Sec C-C Sec C-C Sec C-C Sec C-C Sec D-D Sec	
66 747 1107 807 badle 725 1088 563 404 548 400 562 474 67 770 1132 920 badle 738 1080 572 502 557 408 671 402 68 761 1143 920 badle 747 1092 581 510 569 415 579 491 68 761 1143 931 badle 757 1104 589 519 574 423 588 499 69 792 1156 942 badle 768 1115 598 527 583 430 597 507 70 803 1187 953 badle 779 1138 618 543 600 516 71 814 1179 984 badle 779 1138 618 543 600 468 614 522 72 824 1190 975 badle 600 1150 624 551 600 453 602 531 73 834 1202 980 badle 811 1161 633 660 617 461 631 632 74 845 1213 997 badle 821 1172 642 688 628 648 640 647 75 855 1223 1007 badle 821 1172 642 688 628 648 640 647 76 809 1254 1017 badle 841 1393 688 862 681 641 643 657 583 77 876 1245 1037 badle 861 1203 688 862 681 491 686 677 79 806 1205 1048 badle 861 1203 688 680 680 680 680 677 580 80 905 1275 1553 badle 861 1224 684 608 608 608 608 608 608 80 905 1275 1553 badle 861 1224 684 608 608 608 608 608 608 80 805 1255 1553 badle 861 1223 709 633 641 77 548 641	
88 781 1143 931 baddic 757 1104 589 519 574 423 588 499 699 770 1805 1107 953 baddic 768 1115 588 527 583 540 597 507 70 803 1107 953 baddic 768 1115 588 527 583 540 597 507 70 803 1107 953 baddic 779 1127 607 635 591 438 605 515 71 81 81 1179 964 baddic 780 1138 818 643 600 446 614 523 72 824 1100 975 baddic 810 1101 624 6551 600 446 614 523 72 824 1100 975 baddic 810 1101 624 6551 600 617 401 631 631 639 71 81 81 81 81 81 81 81 81 81 81 81 81 81	
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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ime nin)	P2 Sec C-C TC #10 (*F)	P2 Sec C-C TC #11 (°F)	P2 DDAve (*F)	P2 Sec D-D TC #12 (*F)	P2 Sec D-D TC #13 (°F)	P2 Sec ID-D TC #14 (*F)	P5Max (°F)	P5 AAAve (°F)	P5 Sec A-A TC #1 (°F)	P5 Sec A-A TC #2 (°F)	P5 Sec A-A TC #3 (°F)	P5 Sec A-A TC #4 (°F)	
128 129 130	1304 1310 1316	1653 1661 1689	1439 1446 1453	bad/to bad/to	1287 1294 1301	1590 1598 1605	1055 1061 1068	974 981 987	1047 1053 1030	853 859 886	1055 1061 1068	955 982 968	
131 132 133	1321 1327 1331	1678 1683 1689	1461 1468 1473	bad/to bad/to bad/to	1308 1315 1320	1613 1620 1626	1074 1080 1087	994 1000 1007	1067 1073 1080	872 879 886	1074 1080 1087	975 981 988	
134 135	1336 1341	1697 1705	1480 1488	bad/tc bad/tc	1326 1333	1634 1643	1093 1099	1013	1088	892 898	1093	1001	
136 137 138	1345 1350 1354	1712 1718 1725	1495 1502 1508	bad/to bad/to bad/to	1339 1345 1360	1651 1659 1666	1106 1112 1118	1026 1032 1039	1099 1105 1111	905 911 918	1106 1112 1118	1007 1014 1020	
139 140	1361 1368	1731	1515 1521	bad/tc bad/tc	1355 1361	1674 1681	1124	1045	1117	924 931	1124	1026 1032	
141 142 143	1376 1385 1393	1743 1748 1753	1528 1535 1542	bad/to bad/to bad/to	1367 1375 1383	1688 1694 1700	1136 1142 1147	1057 1084 1089	1130 1136 1141	937 944 950	1136 1142 1147	1039 1045 1051	
144	1402 1412	1759 1765	1550 1557	bad/tc bad/tc	1392 1400	1707 1714	1153 1159	1075 1081	1147 1153	957 963	1153	1057	
146 147 148	1422 1433 1443	1768 1774 1780	1564 1572 1581	bad/to bad/to bad/to	1409 1419 1429	1718 1724 1732	1164 1170 1176	1087 1093 1099	1158 1164 1170	989 976 982	1164 1169 1175	1089 1076 1081	
149 150 151	1452 1463 1472	1782 1789 1792	1587 1596 1603	bad/to bad/to	1439 1449 1459	1735 1742 1747	1182 1187 1193	1105 1111 1116	1176 1181 1187	988 995 1001	1186 1191	1087 1093 1099	
152	1482 1491	1798	1812 1618	bad/to	1469 1478	1754 1758	1198	1122	1192 1198	1007	1197	1105 1110	
154 155 156	1500 1509 1518	1809 1810 1814	1626 1633 1640	bad/to bad/to	1488 1497 1506	1764 1769 1773	1209 1215 1220	1134 1139 1145	1203 1209 1214	1020 1026 1032	1208 1213 1218	1116 1122 1128	
157 158 159	1527 1538 1544	1818 1821 1826	1847 1853 1860	bad/to bad/to	1515 1524 1533	1778 1782 1787	1226 1231 1237	1150 1156 1162	1219 1225 1230	1038 1045 1051	1223	1133 1139 1146	
160 161	1553 1561	1829 1833	1666 1673	bad/tc bad/tc	1541 1550	1791 1796	1242	1167 1172	1235 1240	1057 1083	1234 1239 1243	1150 1155	
162 163 164	1570 1579 1589	1836 1838 1840	1680 1684 1690	bad/to bad/to bad/to	1559 1568 1575	1800 1801 1804	1253 1258 1264	1178 1183 1189	1246 1251 1256	1089 1075 1081	1249 1254 1259	1161 1166 1172	
165 166	1600 1610	1844 1848	1696 1703	bad/to bad/to	1584 1593	1808 1813	1269 1274	1194 1199	1261 1266	1087 1093	1264 1268	1177	
168 169	1620 1630 1639	1849 1852 1856	1709 1715 1722	bad/to bad/to bad/to	1603 1612 1622	1814 1817 1821	1279 1284 1289	1204 1210 1215	1271 1276 1280	1099 1105 1111	1273 1278 1283	1187 1193 1198	
170 171 172	1648 1656 1664	1858 1859 1860	1727 1732 1738	bad/to bad/to bad/to	1631 1640 1648	1823 1824 1824	1294 1299 1304	1220 1225 1230	1285 1290 1295	1116 1122 1128	1288 1292 1297	1203 1208 1214	
173 174	1671 1678	1860	1740 1745	bad/tc bad/tc	1655 1663	1825 1827	1309 1314	1235 1240	1300 1304	1134 1139	1301	1218 1223	
175 176 177	1685 1692 1699	1863 1865 1866	1740 1754 1758	bad/to bad/to bad/to	1670 1677 1684	1828 1830 1832	1318 1323 1327	1244 1249 1254	1308 1313 1318	1145 1151 1156	1310 1315 1319	1228 1233 1238	
178 179 180	1708 1712 1719	1868 1869 1871	1763 1767 1771	bad/tc bad/tc bad/tc	1691 1698 1704	1834 1836 1838	1332 1336 1340	1259 1263 1268	1322 1326 1331	1162 1167 1173	1323 1327 1331	1243 1248 1253	
181 182	1725 1731	1873 1874	1778 1780	bad/tc bad/tc	1711 1717	1840 1842	1344 1347	1273 1277	1335	1178 1183	1335 1338	1257	
183 184 185	1737 1742 1748	1876 1878 1879	1784 1787 1791	bad/to bad/to	1723 1728 1734	1844 1848 1848	1351 1354 1358	1281 1285 1289	1343 1348 1350	1188 1193 1198	1341 1344 1348	1266 1271 1275	
196 187	1753 1758	1880	1795 1798	bad/tc bad/tc	1739 1744	1850 1851	1362 1366	1294 1298	1353 1356	1204 1208	1351 1355	1280 1284	
188 189 190	1764 1769 1774	1884 1885	1802 1805 1809	bad/to bad/to bad/to	1750 1755 1760	1853 1855 1857	1370 1374 1377	1301 1306 1310	1359 1363 1367	1213 1218 1223	1358 1362 1366	1288 1292 1297	
191	1779	1887	1812	bad/tc	1765	1859	1381	1314	1370	1228	1369	1301	



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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

P2
Sec C-C Sec C-C Sec C-C Sec D-D Sec
192 1764 1888 1815 badfe 1769 1880 1335 1318 1374 1232 1373 1306
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1986 1804 1892 1827 bandre 1787 1888 1401 1333 1388 1250 1387 1319 1897 1809 1808 1830 1830 bandre 1791 1809 1807 1300 1300 1300 1300 1300 1300 1300 13
198 1914 1985 1933 baddle 1795 1871 1410 1940 1996 1258 1995 1329 1997 1918 1918 1988 1839 baddle 1799 1872 1414 191 1213 1999 1329 1329 1907 1918 1918 1918 1918 1918 1939 baddle 1902 1874 1418 1948 1409 1213 1999 1932 1932 1932 1934 1937 1934 1934 1934 1934 1934 1934 1934 1934
190
201 1828 1888 1844 badric 1903 1876 1423 1356 1419 1271 1407 1336
203 1835 1900 1846 baddle 1817 1831 1436 1356 1418 1279 1415 1344 1366 1848 1859 1801 1848 1850 1848 1850 1848 1440 1366 1428 1222 1418 1348
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207 1800 1004 1805 badric 1831 1836 1449 1373 1435 1233 1431 1332 288 1853 1055 1861 badric 1837 1838 1454 1330 1444 1330 1439 1359 1355 1355 1355 1861 1865 1867 1863 badric 1837 1838 1458 1330 1444 1330 1439 1359 1359 1359 1359 1359 1359 1359 13
2009 1866 1505 1863 badric 1807 1838 1458 1390 1444 1300 1439 1359
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213 1909 1910 1971 badric 1649 1893 1479 1395 1402 1313 1455 1374 214 1889 1911 1912 1918 badric 1928 1893 1438 1433 1403 1470 1330 1485 1338 215 1871 1912 1918 badric 1928 1893 1438 1433 1403 1470 1330 1485 1381 216 1873 1913 1913 1913 1913 1918 1894 1897 1438 1403 1470 1330 1485 1381 217 1875 1914 1914 badric 1928 1898 1492 1411 1479 1326 1471 1399 218 1877 1915 1916 1916 badric 1928 1898 1492 1411 1479 1326 1471 1399 220 1881 1917 1919 badric 1931 1900 1500 1419 1488 1332 1479 1397 222 1884 1917 1919 badric 1934 1901 1500 1419 1488 1332 1479 1347 222 1886 1917 1919 badric 1934 1901 1500 1471 1578 1493 1493 1414 1471 223 1886 1917 1919 badric 1938 1901 1500 1419 1489 1494 1494 224 1888 1918 1920 badric 1938 1903 1903 1474 1471 1502 1474 1471 1479 225 1890 1919 1920 badric 1938 1903 1500 1418 1500 1342 1485 1416 226 1890 1919 1921 badric 1938 1903 1500 1435 1500 1342 1485 227 1883 1919 1921 badric 1938 1903 1500 1438 1500 1342 1485 228 1890 1919 1921 badric 1938 1903 1500 1500 1448 1500 1342 1485 228 1890 1919 1921 badric 1938 1903 1503 1436 1503 1340 1444 1499 229 1898 1600 1922 badric 1938 1606 1531 1450 1523 1436 1607 1428 229 1898 1620 1922 badric 1938 1606 1531 1450 1523 1436 1607 1436 229 1898 1622 1928 badric 1938 1606 1535 1447 1538 1532 1350 1311 1432 229 1898 1622 1922 badric 1938 1606 1535 1447 1538 1532 1350 1351 1432 229 1898 1622 1928 badric 1938 1606 1535 1447 1538 1538 1538 1538 1444 220 1897 121 122 badric 1938 1606 1535 1447 1538 1538 1538 1439 1444 221 1897 121 122 badric 1938 1606 1535 1447 1538 1538 1538 1448 223 1890 1622 1924 badric 1938 1900 1598 1447 1538 1536 1358 1457 224 1490 1622 1924 badric 1938 1900 1598 1447 1538 1548 1538 1549 1447 223 1890 1622 1924 badric 1938 1900 1598 1447 1552 1372 1375 1449 223 1890 1624 1625 1526 1608 1909 1908 1589 1477 1552 1372 1376 1449 224 1890 1624 1625 1626 1638 1900 1598 1447 1558 1549 1349 1358 1448 225 1890 1624 1625 1626 1639 1900 1598 1449 1599 1390 1390 1390 1447 224 1890 1624 1625 16
215 1871 1912 1911 baddle 1928 1898 1483 1403 1470 1320 1485 1388 216 1873 1913 1913 baddle 1928 1898 1498 1498 1498 1498 1498 1498 149
217 1875 1014 1914 bedite 1029 14898 1492 1411 1479 1328 1471 1339 1218 1471 1478 1328 1471 1339 1218 1471 1478 1328 1471 1339 1475 1318 1471 1478 1328 1471 1339 1475 1339 1475 1471 1478 1328 1471 1471 1478 1471 1471 1471 1471 147
219 1879 1616 1816 1816 1817 1816 badite 1831 1890 1500 1418 1488 1332 1479 1387 220 1881 1816 1817 1818 badite 1833 18901 1504 1504 1427 1487 1337 1488 1482 221 1884 1817 1818 badite 1834 18901 1508 1427 1487 1337 1487 1406 1222 1886 1817 1819 badite 1805 18002 1512 1413 1502 1340 1481 1481 1485 1416 1222 18186 1817 1819 badite 1805 18002 1516 1415 1436 1508 1342 1489 1416 1416 1427 1428 1428 1428 1428 1428 1428 1428 1428
224 1863 1917 1918 badde 1934 1901 1508 1427 1437 1437 1467 1406 222 1866 1917 1918 badde 1902 1502 1512 141 1502 1347 1467 1440 223 1866 1917 1918 badde 1902 1505 1902 1512 141 1502 1342 1465 1416 224 1868 1918 1920 badde 1903 1903 1903 1500 1500 1416 1510 1342 1465 1416 225 1890 1918 1920 badde 1907 1903 1524 1442 1515 1346 1500 1442 226 1891 1919 1921 badde 1503 1904 1528 1442 1515 1346 1509 1428 227 1863 1919 1921 badde 1503 1904 1528 1442 1515 1346 1509 1428 228 1804 1919 1922 badde 1503 1904 1528 1445 1519 1348 1507 1428 229 1806 1807 1902 badde 1503 1904 1538 1405 1523 1450 1522 1446 1498 1509 1428 220 1806 1820 1922 badde 1503 1904 1538 1450 1523 1350 1511 1432 230 1808 1820 1922 badde 1503 1904 1503 1446 153 1447 1531 1536 1518 1446 1448 1448 1448 1448 1448 1448 14
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227 1803 1919 1921 baddle 1838 18004 1531 1450 1523 1350 1511 1432 228 1804 1919 1922 baddle 1938 1806 1535 1457 1527 1525 1516 1436 1436 1436 1436 1436 1436 1436 14
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231 1897 1821 1812 bedfile 1839 1907 1547 1465 1540 1361 1527 1449 232 bedfile 1839 1907 1547 1465 1540 1361 1527 1449 232 bedfile 1839 1907 1561 1449 1544 1334 1531 1453 233 1800 1022 1924 bedfile 1939 1908 1554 1473 1548 1388 1535 1457 234 1900 1023 1924 bedfile 1839 1908 1558 1477 1552 1372 1559 1462 235 1924 1560 1523 1924 1560 1560 1560 1451 1555 1375 1542 1466 236 1901 1223 1924 bedfile 1839 1909 1560 1461 1575 1565 1375 1542 1466 237 1924 1560 1477 1555 1375 1542 1466 1560 1477 1577 1577 1577 1577 1477 1477 1577 15
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236 1900 1823 1924 badne 1839 1909 1562 1481 1556 1375 1542 1466 236 1901 1823 1924 badne 1938 1909 1562 1485 1589 1379 1546 1470 237 1901 1824 1924 badne 1938 1910 1570 1480 1564 1333 1560 1474 238 1902 1824 1925 badne 1938 1911 1574 1493 1599 1396 1554 1478 239 1902 1824 1925 badne 1938 1911 1574 1493 1599 1396 1554 1478 1478 1478 1478 1478 1478 1478 147
237 1901 1924 1925 badic 1938 1910 1570 1489 1594 1383 1550 1474 238 1902 1925 badic 1938 1911 1578 1493 1509 1386 1554 1478 239 1902 1025 1926 1926 1938 1911 1578 1497 1573 1300 1554 1482
239 1902 1925 1925 baddte 1938 1911 1578 1497 1573 1390 1558 1482
Max.T: 1903 1925 backtc 1939 1912 1582 1601 1577 1394 1562 1486
Max A 1200 1200 1000 1200 1200 1200 1200 12

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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aeroge Project No. 3	els, Inc. 159033											ıst, 2008 41 of 95	
	P5	P5 P5	P5 P5		P5	P5	P 5	a r	P5		August 2008		
Time (min)	Sec A-A	P5 P5 Sec B-B BBAve TC #6 (*F) (*F)	Sec B-B Sec B-B TC#7 TC#8 (°F) (°F)	CCAve	Sec C-C TC #9 (*F)	Sec C-C TC #10 (°F)	Sec C-C TC #11 (°F)	DDAve (°F)	Sec D-D TC #12 (°F)	P5 Sec D-D TC #13 (°F)	P5 Sec D-D TC #14 (°F)		
0 1 1 2 2 3 3 4 4 5 6 6 6 7 7 8 8 9 9 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	82 81 81 81 81 82 82 83 84 86 87 89 99 91 91 91 91 91 91 91 91 91 91 91 91	82 82 82 82 82 82 82 82 82 82 82 82 82 8	82	82 82 82 82 82 82 82 82 83 83 84 84 88 88 88 88 99 92 96 101 106 118 123 130 130 130 146 149 149 120 121 121 130 130 130 130 130 130 130 130 130 13	822 82 82 82 82 82 82 82 82 82 82 82 82	82 82 82 82 82 82 82 82 82 82 82 82 82 8	82 2 82 82 82 82 82 82 82 82 82 82 82 82	82 82 82 82 82 82 82 83 86 86 86 86 86 86 86 86 86 86 86 86 86	82 2 82 82 82 82 82 82 82 82 82 82 82 82 82 8	82 82 82 82 82 82 82 82 82 82 82 82 82 8	82 82 82 82 82 82 82 82 82 82 82 82 82 8		
										ln	tert	ek	



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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

## P5	Aspen Ae Project N															ugust, 2 ige 42 (
Figure Temp Temp														21	August 2	008	
68		Time	Sec A-A TC #5	BBAve	Sec B-B TC #6	Sec B-B TC #7	Sec B-B TC #8	CCAve	Sec C-C TC #9	Sec C-C TC #10	Sec C-C TC #11	DDAve	Sec D-D TC #12	Sec D-D TC #13	Sec D-D TC #14		
		656 667 678 659 659 677 777 78 777 78 777 78 78 78 78 78 78 7	485 493 501 151 151 151 151 151 151 151 151 151	908 608 608 608 608 608 608 608 608 608 6	5500 577 588 588 588 687 770 770 770 770 770 770 770 770 770 7	994 402 410 410 410 410 410 410 410 410 410 410	693 693	5014 5015 5029 5030 5030 5030 5030 5030 5030 5030 503	551 551 551 551 551 551 551 551 551 551	996 403 403 411 419 426 434 441 449 446 457 458 458 458 458 458 458 458 458 458 458	953 3 646 623 625 629 629 629 629 629 629 629 629 629 629	480 488 496 504 512 520 529 529 535 543 543 557 557 557 657 657 657 657 657 657 657	541 542 542 542 542 542 542 542 542 542 542	378 385 386 3812 398 398 399 407 44 421 421 421 431 431 431 431 431 431 431 431 431 43	622 559 650 650 650 650 650 650 650 650 650 650		



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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerog Project No. 3														ugust, age 43	
												21	August 2	008	
Tim (mir		P5 BBAve (*F)	P5 Sec B-B TC #6 (*F)	P5 Sec B-B TC #7 (*F)	P5 Sec B-B TC #8 (°F)	P5 CCAve (*F)	P5 Sec C-C TC #9 (*F)	P5 Sec C-C TC #10 (°F)	P5 Sec C-C TC #11 (°F)	P5 DDAve (°F)	P5 Sec D-D TC #12 (°F)	P5 Sec D-D TC #13 (°F)	P5 Sec D-D TC #14 (°F)		
12 12 12 12 12 12 12 12 12 12 12 12 12 1	128 962 962 128 962 128 962 128 962 128 962 128 962 128 128 128 128 128 128 128 128 128 12	978 8 6644 664 664 664 664 664 664 664 664	1045 (1988) (198	836 844 846 846 846 846 846 846 846 846 84	1025 1029 1027 1077 1077 1077 1077 1077 1085 1091 1091 1098 1104 1114 1114 1115 1114 1115 1116 1116 111	972 964 972 973 974 975 974 975 975 975 975 975 975 975 975 975 975	1000 1003 1003 1003 1003 1003 1003 1003	832 839 846 851 851 851 851 851 851 851 851 851 851	1054 1084 1087 1067 1067 1066 1092 1106 1090 1106 1090 1106 1111 1112 1130 1142 1130 1147 1153 1154 1154 1154 1154 1154 1154 1155 1154 1154 1154 1155 1154 1155 1	932 938 944 957 968 969 969 969 969 960 1005 1001 1002 1022 1023 1034 1054 1054 1056	1004 1014 1014 1014 1017 1017 1018 1019 1019 1019 1019 1019 1019 1019	803 810 82 82 82 82 82 82 82 82 82 82 82 82 82	984 901 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		



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Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerogels, Inc. Project No. 3159033

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	ro	1.0	FU		1.0	Fu	ro	10	10	F-0	FO	Fo		
	Sec A-A		Sec B-B	Sec B-B	Sec B-B		Sec C-C		Sec C-C			Sec D-D	Sec D-D	
Time	TC #5	BBAve	TC #6	TC #7	TC #8	CCAve	TC#9	TC #10	TC #11	DDAve	TC #12	TC #13	TC #14	
(min)	(*F)	(°F)	(*F)	(°F)	(°F)	(*F)	(°F)	(°F)	(°F)	(°F)	(°F)	(°F)	(°F)	
192	1305	1320	1371	1214	1374	1314	1353	1205	1385	1273	1335	1171	1313	
193	1308	1324	1375	1219	1378	1318	1356	1210	1389	1277	1338	1176	1317	
194	1312	1328	1379	1223	1381	1323	1380	1215	1393	1281	1342	1181	1321	
195	1315	1332	1383	1228	1385	1327	1364	1219	1397	1285	1345	1185	1325	
196	1319	1336	1388	1232	1389	1331	1368	1224	1401	1289	1348	1190	1329	
197	1322	1340	1390	1237	1393	1335	1371	1228	1405	1293	1351	1195	1332	
198	1325	1344	1393	1241	1397	1339	1375	1232	1410	1296	1354	1199	1335	
199	1328	1348	1397	1245	1401	1343	1379	1237	1414	1300	1358	1204	1339	
200	1331	1352	1401	1250	1405	1347	1382	1241	1418	1304	1382	1208	1342	
201	1334	1356	1405	1254	1409	1351	1386	1245	1423	1308	1365	1213	1345	
202	1336	1380	1409	1258	1413	1356	1390	1250	1427	1311	1369	1217	1348	
203	1339	1364	1413	1262	1417	1360	1394	1254	1432	1316	1373	1222	1352	
204	1342	1388	1417	1266	1421	1364	1398	1257	1436	1319	1377	1226	1355	
205	1345	1372	1421	1270	1426	1368	1402	1261	1440	1323	1380	1230	1358	
206	1348	1376	1425	1273	1429	1372	1405	1265	1445	1327	1384	1234	1362	
207	1362	1380	1429	1277	1434	1376	1410	1269	1449	1331	1388	1238	1366	
208	1355	1384	1433	1280	1438	1380	1413	1273	1454	1335	1392	1243	1369	
209	1358	1388	1437	1284	1442	1384	1418	1276	1458	1338	1395	1247	1373	
210	1362	1391	1441	1287	1443	1388	1422	1280	1462	1342	1400	1251	1376	
211	1365	1395	1445	1291	1460	1392	1426	1284	1466	1346	1404	1255	1380	
212	1369	1399	1449	1294	1455	1396	1430	1287	1471	1350	1408	1259	1383	
213	1373	1403	1453	1298	1459	1400	1434	1290	1475	1354	1412	1262	1387	
214	1377	1407	1457	1301	1463	1403	1437	1293	1479	1357	1416	1266	1390	
215	1381	1411	1461	1304	1467	1407	1442	1297	1483	1381	1420	1270	1394	
216	1385	1414	1465	1307	1471	1411	1445	1300	1488	1335	1424	1273	1398	
217	1389	1418	1469	1310	1476	1415	1449	1304	1492	1339	1428	1277	1402	
218	1393	1422	1473	1313	1479	1419	1453	1307	1496	1373	1433	1280	1406	
219	1397	1426	1477	1316	1484	1422	1457	1310	1500	1377	1437	1284	1410	
220	1402	1430	1481	1320	1488	1426	1461	1313	1504	1381	1441	1287	1414	
221	1406	1433	1485	1322	1492	1430	1465	1316	1508	1385	1445	1291	1418	
222	1411	1437	1489	1325	1499	1433	1469	1319	1512	1388	1449	1294	1421	
223	1415	1440	1492	1328	1500	1437	1473	1322	1516	1392	1453	1297	1425	
224	1420	1444	1495	1331	1504	1440	1476	1325	1520	1395	1457	1300	1429	
225	1424	1447	1500	1333	1508	1444	1480	1327	1524	1399	1461	1303	1432	
226	1428	1450	1504	1335	1512	1447	1484	1330	1528	1402	1485	1306	1436	
227	1432	1453	1507	1337	1516	1450	1487	1332	1531	1408	1489	1309	1440	
228	1436	1457	1511	1339	1620	1454	1491	1335	1635	1409	1472	1312	1444	
229	1441	1480	1515	1341	1524	1457	1495	1337	1539	1413	1476	1315	1447	
230	1445	1483	1518	1343	1527	1460	1499	1339	1543	1416	1480	1318	1451	
231	1449	1466	1522	1346	1531	1463	1502	1341	1547	1420	1484	1321	1455	
232	1463	1470	1526	1349	1635	1467	1506	1343	1651	1424	1488	1324	1459	
233	1457	1474	1530	1352	1539	1470	1510	1346	1554	1427	1492	1326	1463	
234	1461	1477	1533	1355	1543	1474	1514	1349	1558	1431	1496	1329	1467	
235	1465	1481	1537	1358	1547	1477	1517	1351	1562	1434	1499	1332	1470	
236	1469	1484	1541	1362	1550	1481	1521	1355	1566	1437	1503	1335	1474	
237	1473	1488	1544	1366	1554	1484	1524	1358	1570	1441	1507	1337	1478	
238	1477	1492	1548	1369	1558	1488	1528	1361	1574	1443	1510	1339	1481	
239	1481	1495	1551	1373	1562	1492	1532	1365	1578	1447	1514	1341	1485	
240	1485	1499	1555	1377	1563	1495	1535	1368	1582	1450	1518	1343	1489	
Max Te	1485	1499	1555	1377	1563	1495	1535	1368	1582	1450	1518	1343	1489	
Max A	1200	1000	1200	1200	1200	1000	1200	1200	1200	1000	1200	1200	1200	





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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerogels, Project No. 3159													ust, 2008 e 45 of 95
											21	August 2008	
Time (min)	P8A P8AMax (°F)	P8A AAAve (°F)	P8A Sec A-A TC #1 (*F)	P8A Sec A-A TC #2 (°F)	P8A Sec A-A TC #3 (*F)	P8A Sec A-A TC #4 (°F)	P8A Sec A-A TC #5 (°F)	P8A BBAve (°F)	P8A Sec B-B TC #6 (°F)	P8A Sec B-B TC #7 (°F)	P8A Sec B-B TC #8 (°F)	P8A CCAve (°F)	
0 1 2	83 83 83	82 82 82	83 83 83	82 82 82	82 82 82	82 82 82	82 82 82	82 82 83	82 82 83	82 82 83	83 83 82	83 83 83	
3 4 5 6	83 83 83 84 84	82 83 83 83	83 83 83	83 83 83 83	82 83 83 83	82 82 82 82	82 82 82 83 83	83 83 83 83	83 83 83 83	83 82 83 83	83 83 83 83	83 83 83	
7 8 9 10	84 84 84 85	83 83 84 85	83 83 84 85 87	82 82 82	83 84 86 86	82 83 83 84 85	83 84 85 85	83 83 84 85	84 84 85	83 83 83 83	83 83 84 85	83 83 84	
12 13 14 15	90 92 93	88 87 88 89	88 90 92 93	82 83 83 84 84	87 89 90 91	85 86 87 87	88 87 88 89	85 86 87 89	86 87 89 90	83 83 83 84	86 87 89	85 85 86 87 88	
16 17 18 19	95 96 98 100	90 91 92 93	95 96 98 100	84 85 86	92 94 95 97	88 89 90 91	90 91 92 93	90 90 91 93	92 93 94 96 98	84 84 85	92 93 94 96	89 90 91 92	
20 21 22 23	102 104 107 110	95 96 98 100	102 104 107 110	87 89 89	98 100 102 104 106	93 94 95 97 98	95 96 98 99	95 96 98 100	100 102 104 107 110	86 87 88	98 99 102 104 107	94 95 97 99 101	
24 25 26 27 28 29	113 117 122 126 131	102 104 107 110 113	113 117 122 126 131	91 92 93 94 96 98	109 112 116	100 102 104 107	101 104 106 109 113	102 105 107 111 114	114 118 123	89 90 91 92 94	110 113 117	103 106 108 112	
30 31 32	136 142 147 153	117 121 124 129	138 142 147 153	102 104	120 124 128 133 138	110 113 116 120	116 121 124 129	117 121 125 129	128 132 137 142 148	94 95 97 99 101	121 125 130 134 139	115 119 123 127	
33 34 35 36 37	158 163 169 175 181	132 137 141 146 150	158 163 169 175 181	109 112 115 118	142 147 152 157 162	123 127 131 135 139	133 138 142 147 151	133 138 142 146 150	153 158 163 168 174	103 106 108 111 114	144 149 154 159 163	131 135 139 144 148	
38 39 40 41	188 194 201 207	155 159 164 169	188 194 201 207	121 124 128 131	166 171 175 180	144 147 152 158	158 160 165 170	155 160 165 170	180 185 192 199	118 121 124 128	168 173 179 184	152 157 162 167	
42 43 44 45 46	213 220 226 233 239	174 179 185 190 195	213 220 226 233 239	135 139 143 147 151	186 193 199 205 211	165 170 175 180	174 179 185 191 196	175 180 186 191 197	205 211 218 224 230	131 135 139 143 147	190 195 201 207 213	172 177 182 188 193	
47 48 49	246 252 259 266	201 207 213	246 262 269 266	155 160 165 169	218 224 230 236	185 191 196 201	202 208 214	202 208 213 219	237 243 250 258	151 156 160 165	219 224 230 236	199 204 210 216	
50 51 52 53 54	272 279 285 292	218 224 230 238 242	272 279 285 292	174 179 184 189	242 248 254 200	207 212 218 223	220 226 232 238 244	225 230 236 242	263 269 275 282	169 174 179 184	242 248 254 260	221 227 232 238	
54 55 56 57 58 59	299 305 312 318 325	247 253 259 265 271	299 305 312 318 325	194 199 204 210 215	266 272 278 284 290	229 234 240 245 251	249 258 262 268 274	248 253 259 265 270	288 294 301 307 313	189 194 199 204 209	266 271 277 283 289	244 250 256 261 267	
60 61 62 63	332 338 345 352	277 283 288 295	332 338 345 352	220 226 231 237	295 301 307 313	256 262 267 273	286 286 292 298	276 282 288 293	319 325 332 338	214 219 225 230	295 301 306 312	273 279 285 290	
											In	ter	tek



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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

PRA	PBA	Aspen Aerogels, Ir Project No. 315903	ic. 33												gust, 200 e 46 of 9	
Time	Times												21	August 200	8	
Section Sect	Mathematics		P8AMax	AAAve	Sec A-A TC #1	Sec A-A TC #2	Sec A-A	Sec A-A TC #4	Sec A-A TC #5	BBAve	Sec B-B TC #6	Sec B-B TC #7	Sec B-B TC #8	CCAve		
67	FF	64 65	358 365	300 306	358 365	242 248	319 325	279 284	304 310	299 305	344 350	235 240	318 324	296 302		
70 390 303 390 980 275 356 312 341 333 381 287 352 331 71 72 411 344 411 288 381 347 353 381 287 352 331 77 72 411 344 411 288 397 332 385 337 386 337 386 337 386 337 386 337 386 337 386 387 386 337 386 387 386 387 387 387 387 387 387 387 387 387 387	70 596 330 596 275 356 312 341 333 381 297 352 331 337 337 338 338 337 338 3	67 68	378 385	318 324 330	378 385	259 264	337 343	295 301	322 329	316 322	363 369	251 258	335 341	313 319		
73	73	70 71	398 404	338 342	398 404	275 281	355 381	312 318	341 347	333 339	381 387	267 273	352 358	331 337		
766 437 372 437 509 396 396 397 396 397 498 397 498 398 397 498 398 397 498 398 397 398 398 397 398 398 398 398 398 398 398 398 398 398	76	73 74	418 424	364 360	418 424	292 298	373 379	329 335	369 365	351 357	400 408	283 289	370 376	348 354		
70	70	76 77	437 444	372 378	437 444	309	392 398	346 352 358	377	388 374	418 424	300 306	387 393	366 372		
82 478 408 478 342 428 381 414 403 455 332 422 401 83 483 484 314 483 348 348 433 348 420 400 481 337 428 407 84 499 420 469 329 445 389 392 426 415 467 343 434 441 85 602 432 409 329 445 389 432 420 407 86 602 432 502 354 451 403 438 428 427 3334 444 410 88 615 402 438 208 370 477 408 420 488 339 451 430 88 615 446 515 375 463 415 408 420 488 339 451 430 88 615 446 523 351 408 420 408 420 489 339 451 430 88 615 446 523 351 408 420 488 428 339 451 430 89 623 450 523 474 488 428 489 359 451 430 90 623 451 524 489 523 489 489 489 489 523 578 448 489 529 578 489 589 589 589 589 589 589 589 589 589 5	82 478 408 478 342 428 381 414 493 485 332 422 407 84 499 420 469 339 430 439 392 428 415 467 343 484 410 85 499 420 489 339 445 388 483 488 426 473 343 444 418 86 602 432 502 354 451 403 453 888 87 508 438 388 515 446 515 375 463 415 403 438 488 426 479 355 445 430 88 515 446 515 375 463 415 408 420 489 399 441 430 481 430 481 430 481 481 481 481 481 481 481 481 481 481	79 80	457 463	390 398	467 463	325	410 416	364 369	396 402	386 392	437	316	405 411	383 389		
85	85	82 83	476 483	408 414	476 483	342 348	428 433	381 386	414 420	403 409	455 461	332 337	422 428	401 407		
88	88	85 86	496 502	426 432	502	359 364	445 451	398 403	432 438	420 426	473 479	348 353	440 445	418 424		
92 641 407 641 388 486 437 474 400 515 386 480 449 481 941 486	92 641 407 541 388 486 437 473 480 515 385 480 459 454 454 480 481 481 482 481 480 481 482 481 481 481 481 481 481 481 481 481 481	88 89	521	449	521	381	463 468 474	420	450 456 462	443	497 503	389 375	463 469	441		
86 680 484 560 414 560 409 400 609 400 503 454 411 477 533 401 488 470 897 572 489 572 489 572 489 572 489 572 489 572 489 503 489 544 551 417 515 480 896 615 508 615 508 615 508 615 508 615 617 477 615 610 618 618 618 618 618 618 618 618 618 618	86	92 93	541 547	467 473	541 547	398 403	486 492	437	474 480	460 466	515 521	385	480 486	459 464		
88 579 502 579 431 521 471 509 494 551 417 515 403 99 605 508 656 438 527 477 515 505 557 423 521 409 100 691 514 691 441 632 483 521 606 563 428 527 506 101 608 520 608 447 638 488 527 617 609 433 533 511 102 604 528 604 433 544 494 533 518 575 439 539 518 103 610 531 610 438 550 500 539 523 581 444 544 522 104 617 537 617 494 666 505 545 529 587 449 650 628 106 623 543 623 499 662 511 561 561 509 563 485 509 483 509 483 518 107 609 543 623 499 662 511 561 651 509 567 509 587 549 589 589 589 589 589 589 589 589 589 58	88 579 502 579 431 521 471 509 494 551 417 515 420 99 605 508 508 568 438 527 477 515 500 557 423 521 4490 100 691 514 691 441 632 483 521 606 633 428 627 506 101 608 520 508 447 638 488 527 617 609 433 53 531 511 102 604 528 604 443 535 544 494 533 518 575 439 539 518 103 610 531 610 438 550 500 539 523 581 444 544 522 104 617 537 617 444 656 505 549 589 589 449 650 628 106 623 543 623 489 692 511 551 551 449 650 628 106 623 543 623 489 692 511 551 551 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 455 560 450 560 560 560 560 560 560 560 560 560 5	95 96	560 566	484 490	560 566	414 420	503	454 480	491 497	477	533 539	401	498 504	476 482		
101 698 520 508 447 638 488 527 612 690 433 633 511 102 600 433 633 611 1033 610 538 604 438 550 500 539 523 581 444 544 544 524 104 617 537 617 439 650 628 104 617 537 617 449 650 628 105 623 518 623 518 623 518 520 500 539 523 581 444 544 544 524 105 623 516 623 549 620 549 620 511 557 6439 650 628 540 650 623 549 620 475 620 549 620 620 620 620 620 620 620 620 620 620	101 698 520 698 447 638 488 527 612 569 433 633 511 102 603 613 516 1033 610 531 610 483 550 500 539 523 581 444 544 544 544 544 544 544 544 544 54	98 99	579 585	502 508	579 585	431 438	521 527	471 477	509 515	494 500	551 557	417	515 521	493 499		
104 617 537 617 494 656 505 629 887 449 650 528 106 623 614 600 623 648 659 659 659 659 455 659 659 659 659 659 659 659 659 659 6	104 617 537 617 444 656 505 545 620 587 449 650 628 106 623 106 623 459 643 623 459 668 517 551 551 555 594 455 656 634 106 630 546 536 638 480 573 522 563 566 606 480 662 540 108 642 590 642 540 108 642 590 642 540 555 638 480 573 522 563 566 606 480 658 545 108 642 590 642 481 579 528 563 564 611 470 574 551 557 110 655 572 655 648 481 591 539 530 563 674 577 577 557 557 110 655 572 655 548 610 591 539 530 652 481 502 553 561 561 561 561 561 561 561 561 561 561	101 102	598 604	520 528	598 604	447 453	538 544	488 494	527 533	512 518	569 575	433 439	533 539	511 516		
107 639 555 638 480 573 522 583 549 605 486 588 546 109 673 573 522 683 549 605 486 588 546 109 648 586 582 448 597 578 528 584 587 578 578 577 677 476 579 557 677 476 579 557 677 476 579 557 677 476 579 557 677 476 579 557 677 476 579 557 677 476 579 557 677 476 579 579 579 579 579 579 579 579 579 579	107 639 555 638 480 573 522 563 646 805 486 688 545 109 571 528 563 546 805 548 545 1109 648 595 648 491 595 534 574 577 617 476 579 557 563 549 571 571 572 572 572 572 572 572 572 572 572 572	104 105	617 623	537 543	617 623	464 469	666 682	505 511	545 551	629 636	587 593	449	550 556	528 534		
110 655 572 655 480 591 509 500 503 022 481 565 563 653 614 114 661 578 661 572 506 545 586 560 503 486 601 568 114 661 578 661 578 661 572 602 486 560 568 560 568 560 588 560 580 580 580 580 580 580 580 580 580 58	110 655 572 655 480 591 509 500 630 023 481 585 563 111 661 578 661 562 566 545 568 560 563 620 486 561 568 561 568 1112 667 594 697 602 581 592 575 633 690 691 691 692 691 692 691 692 691 692 691 692 691 692 691 692 692 692 692 692 692 692 692 692 692	107 108	636 642	555 560	636 642	480 485	573 579	522 528	563 568	546 552	605 611	466 470	568 574	545 551		
113 674 500 674 513 608 566 508 560 941 497 603 580 567 114 609 508 608 518 614 502 604 508 607 608 518 614 502 604 508 617 609 509 609 609 609 609 609 609 609 609 609 6	113 674 500 674 513 608 565 508 500 641 497 603 560 114 609 505 600 518 614 502 604 505 647 503 609 567 115 606 601 666 524 620 567 610 502 653 508 615 562 116 6093 607 693 529 625 573 616 597 695 513 620 568 117 600 813 600 535 631 570 821 603 685 518 626 604 118 705 619 705 640 637 504 627 609 671 524 632 601 119 711 025 711 548 643 500 633 615 677 529 638 615 121 724 533 724 533 684 601 644 626 688 540 644 621 122 730 642 730 662 600 600 600 631 644 626 688 540 649 627 123 735 647 736 567 600 012 658 637 700 550 601 634 625 632 124 742 633 742 573 671 077 602 642 700 550 601 634 645 655 632 126 748 659 748 659 748 677 623 667 600 612 658 677 626 668 668 678 665 678 678 665 678 665 678 678 678 678 678 678 678 678 678 678	110 111	655 661	572 578	655 661	493 502	591 596	539 545	580 586	563 560	623	481 486	585 591	563 568		
116 693 607 693 829 625 573 618 597 659 613 620 568 117 690 613 809 535 631 570 621 603 665 618 626 604 118 705 619 705 640 4037 564 627 609 071 524 632 610 119 711 625 711 549 643 590 633 615 777 529 638 615 120 717 830 717 551 648 505 839 620 882 534 644 621 121 724 635 724 535 654 601 644 626 888 540 649 627 122 730 642 730 562 600 600 600 600 600 631 684 555 652 123 739 647 730 567 600 601 600 600 630 631 684 555 652 124 742 635 742 573 677 607 608 677 700 556 600 643 126 748 650 748 578 677 602 667 648 712 661 672 649 643 678 678 678 678 678 678 678 678 678 678	116 693 607 693 539 625 573 616 597 659 513 620 568 117 600 535 631 570 621 603 665 518 626 604 118 705 619 705 540 637 564 627 621 603 665 518 626 604 118 705 619 705 540 637 564 627 606 671 524 632 610 119 711 625 711 548 648 595 639 620 682 534 644 621 120 717 724 638 724 638 654 631 644 621 626 688 540 649 627 121 724 638 724 638 654 631 644 621 626 688 540 649 627 122 730 642 730 562 600 608 600 631 604 626 688 540 649 627 122 730 642 730 562 600 608 600 631 604 626 688 640 649 627 122 730 642 730 562 600 608 600 631 604 649 655 632 123 736 644 742 638 742 573 671 677 602 642 706 555 606 643 126 748 669 748 678 678 677 603 667 648 712 661 672 648 655 685 685 685 685 685 685 685 685 68	113 114	674 680	590 596	674 680	513 518	608	556 562	598 604	580 586	641 647	497 503	603	580 587		
119 711 025 711 5-45 643 590 033 615 077 529 038 015 120 717 529 717 551 648 505 71 529 718 621 718 719 719 719 719 719 719 719 719 719 719	119 711 025 711 549 643 590 033 615 077 528 038 615 120 717 528 718 621 121 724 536 717 551 648 555 639 620 622 534 644 621 121 724 536 724 536 654 690 600 600 631 644 626 688 540 649 627 122 730 642 730 662 600 600 600 631 604 545 655 632 123 739 647 730 567 600 012 058 637 700 550 601 638 655 632 123 736 654 655 677 600 612 058 637 700 550 601 638 126 748 659 748 659 748 677 623 667 648 712 661 672 648 126 754 648 754 683 629 673 654 718 566 678 655	116 117	693 699	607 613	693 609	529 535	625	573 579	616	597 603	659 665	513 518	620 626	598 604		
122 730 842 730 542 800 606 850 631 884 545 655 632 129 736 847 790 547 800 612 058 637 700 550 601 630 124 742 833 742 573 671 817 862 642 708 555 888 643 748 669 748 678 677 623 867 648 742 661 678 678 677 623 667 648 742 661 672 649 126 754 864 754 683 629 673 654 718 568 678 678 685	122 730 642 730 562 660 606 650 631 694 545 655 632 125 736 647 739 567 690 112 058 637 700 550 681 638 124 742 633 742 573 671 017 662 642 706 555 660 643 126 748 669 748 678 677 603 667 648 712 661 672 648 126 754 684 754 683 629 673 654 718 568 678 665	119 120	711 717 724	625 630	711 717	545 551	643 648	590 595	633 639	615	677 682	529 534	638 644	615 621		
125 748 650 748 678 677 623 667 648 712 561 672 649 126 754 684 754 583 683 629 673 654 718 566 678 655	126 748 869 748 578 677 623 667 648 712 561 672 649 126 754 884 754 583 683 629 673 654 718 586 678 656	122 123	730 736	842 847	730 736	562 567	680 686	606 612	650 658	631 637 642	694 700	545 550	655 661	632 638		
		125 126	748 754	659 664	748 754	578 583	677 683	623 629	667 673	648 654	712 718	561 566	672 678	649 656		
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerogels, Project No. 3159													ıgust, 2 ge 47 o	
											21	August 20	08	
Time (min)	P8A P8AMax	AAAve	P8A Sec A-A TC #1	P8A Sec A-A TC #2	P8A Sec A-A TC #3 (*F)	P8A Sec A-A TC #4 (*F)	P8A Sec A-A TC #5 (°F)	P8A BBAwe (°F)	TC #6	P8A Sec B-B TC #7 (°F)	P8A Sec B-B TC #B (°F)	P8A CCAve		
128 129	(°F) 787 773	(*F) 676 682	(*F) 767 773	(°F) 594 600	694 700	640 645	685 691	665 671	(%F) 730 735	576 582	689	(°F) 687 672		
130 131 132	779 785 791	688 693 699	779 785 791	605 610 618	706 712 717	651 656 662	697 702 708	676 682 688	741 747 753	587 592 597	701 707 713	679 685 690		
133 134 135	797 803 810	704 710 716	797 803 810	621 626 632	723 729 735	667 673 679	713 719 725	693 699 705	759 765 771	602 608 613	718 724 730	695 701 707		
136 137 138	816 822 829	722 728 734	816 822 829	638 643 649	740 746 752	684 690 695	731 737 743	710 716 722	777 783 789	618 624 629	736 742 748	714 720 726		
139 140 141	835 841 847	740 745 751	835 841 847	655 660 666	758 764 769	701 707 712	749 755 761	728 734 740	796 802 808	634 640 645	754 760 766	733 739 746		
142 143 144	853 859 885	757 763 769	853 859 865	672 678 683	775 781 787	718 724 730	767 772 778	746 751 757	814 820 828	951 956 981	772 778 784	752 758 784		
145 146 147	871 877 883	774 780 788	871 877 883	689 695 700	793 798 804	735 741 746	784 790 795	763 769 775	832 838 844	667 672 678	790 796 802	770 776 782		
148 149 150	889 895 901	791 797 803	889 895 901	703 711 717	809 815 821	752 757 763	801 807 812	780 786 791	849 855 861	683 689 694	807 814 819	788 795 800		
151 152 153	908 912 918	808 814 819	908 912 918	723 728 734	826 831 837	768 774 779	818 824 829	797 803 809	867 873 879	699 704 710	825 831 837	807 812 818		
154 155 156	923 929 935	825 830 836	923 929 935	739 745 750	843 848 853	785 790	835 840 846	814 820 825	884 890 896	715 721 726	842 848	824 830 836		
157 158 159	940 948 861	841 847 852	940 946 951	758 761 767	859 864 870	796 801 806 812	851 857 862	830 836 842	901 907 912	731 737	854 859 865 871	842 848 854		
160 161	967 962	858 863	957 962	772 778	875 880	817	867 873	847 853	918 923	742 747 753	876	860 866		
162 163 164	968 974 960	869 874 880	968 974 980	783 789 795	886 891 897	828 833 839	878 884 889	858 864 870	929 935 941	758 763 769	888 894 899	872 878 884		
165 166 167	965 990 995	885 890 896	985 990 995	805 811	902 907 913	844 849 855	894 899 905	875 880 886	948 951 957	774 779 784	905 910 916	890 895 901		
168 169 170	1001 1008 1011	901 906 911	1001 1006 1011	816 821 826	918 923 928	865 870	910 915 920	891 896 901	962 967 972	790 795 800	921 926 932	906 912 917		
171 172 173	1017 1023 1029	917 922 929	1017 1023 1029	832 838 845	934 939 945	876 881 887	926 931 937	907 913 919	978 984 991	806 811 817	938 944 950	924 931 938		
174 175 176	1035 1040 1045	934 939 945	1035 1040 1045	850 856 862	950 955 961	892 898 903	943 948 953	925 930 936	996 1002 1007	823 828 833	956 961 967	944 950 956		
177 178 179	1051 1058 1062	950 955 960	1051 1056 1061	867 872 878	966 971 976	908 913 918	959 964 969	941 946 952	1013 1018 1023	839 844 849	972 977 983	962 987 973		
190 181 182	1068 1071 1077	966 970 975	1066 1071 1076	883 888 893	981 986 991	923 928 933	974 979 984	957 962 968	1029 1034 1039	854 860 865	988 993 999	978 984 989		
183 184 185	1082 1090 1093	981 988 991	1081 1088 1091	905 909	996 1001 1006	939 944 949	989 994 999	972 978 983	1044 1050 1054	870 878 880	1003 1009 1014	995 1001 1006		
196 187 188	1099 1106 1113	996 1001 1007	1098 1102 1107	915 921 927	1011 1016 1021	954 959 934	1004 1009 1015	988 994 1000	1059 1065 1071	886 892 897	1020 1025 1031	1011 1018 1025		
189 190 191	1119 1122 1126	1012 1017 1022	1113 1117 1122	933 938 942	1026 1031 1036	970 974 979	1020 1025 1030	1005 1010 1015	1077 1081 1086	903 908 913	1036 1041 1045	1031 1035 1040		
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL



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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerog Project No. 3					28 August, 2008 Page 49 of 95
	P8A P8A Sec C-C Sec C-C S	P8A P8A P8A ec C-C Sec D-D	P8A P8A Sec D-D Sec D-D	P8B P8B P8B Sec A-A Sec	21 August 2008 P8B P8B A-A Soc A-A
Time (min) 0 1	TC #9 TC #10 (*F) (*F) 83 83 83 83	fC #11 DDAve TC #12 (*F) (*F) (*F) 82 82 82 82 82 82 82	TC #13 TC #14 (*F) (*F) 82 82 82 82	PSBMax AAAve TC#1 TC (°F) 83 82 83 83 82 83	C #2 TC #3 (°F) (°F) 83 82 83 82
2 3 4 5 6	83 83 83 83 83 83	83 83 83 82 82 82 82 82 82 83 83 83 83 82 82	82 83 82 82	83 82 83 84 82 83 84 82 83 84 82 82 84 83 83 85 83 83	83 82 83 82 83 82 82 82 82 82 82 82
, 9 10 11 12	83 83 84 83 85 83 86 83	83 82 82 83 83 83 84 83 83 85 83 84 86 84 85	82 83 82 83 82 84	86 84 84 87 84 85 88 85 86 89 86 88 90 87 90	63 85 85 85 84 86 86 88 88 88 88 88
13 14 15 16	88 84 89 84 91 84 92 84 93 85	87 85 88 88 86 87 89 87 88 91 88 90	82 87 82 88 83 89 83 90 84 92	92 88 92 93 89 93 96 91 96 98 92 98 100 94 100	84 89 85 91 86 92 86 94
18 19 20 21 22	94 85 98 88 98 99 100 87 102 88	92 89 91 94 90 92 95 91 94 97 98 93 97 100 95 99	84 94 85 98 85 97 86 99	102 95 102 105 97 105 108 99 108 110 101 110 113 104 113	87 96 88 98 89 100 90 103 92 106
23 24 25 26 27	108 89 111 90 115 91 119 92	102 97 102 105 98 104 107 100 107 111 103 111 114 108 115 118 109 119	87 103 88 106 89 109 90 112	116 108 118 119 109 119 123 112 123 127 115 127 132 119 132 137 122 137	93 109 94 113 96 117 97 122 99 128 101 133
28 29 30 31 32 33	134 97 139 98 144 100	122 112 123 126 115 128 131 119 133 136 123 138	93 120 94 124 96 128 98 133	142 128 142 147 130 147 152 134 152 156 138 156	103 139 105 144 108 149 110 155 113 160
33 34 35 36 37 38	166 110 171 113 177 116	145 131 149 150 135 154 155 140 159 159 144 165 164 149 171	103 142 105 147 108 152 111 157 113 162	166 147 165 172 151 170 178 156 175 182 161 180 190 185 182	116 169 119 172 122 178 125 182 130 190
39 40 41 42 43	202 129 209 133	168 153 176 174 168 182 179 163 188 184 168 194 190 173 201	120 171 123 177 127 162 131 188	204 177 197 210 182 205 217 188 212 224 194 219	135 197 136 204 141 210 145 217 149 224
44 45 46 47 48 49	228 145 235 149 242 153	195 178 207 201 183 213 207 188 219 213 194 225 218 199 232 224 205 238	142 204 147 210 151 215	237 217 233 ba 243 224 240 ba 250 229 246 be 256 238 253 ba	183 230 iddhe 237 iddhe 243 iddhe 250 iddhe 256 iddhe 263
50 51 52 53 54	255 163 261 167 268 172	224 205 238 230 210 244 236 216 250 241 221 256 247 227 262 253 232 268	160 227 165 232 169 238 174 244	269 248 267 ba 276 254 274 ba 283 261 280 ba 280 267 287 ba	ddhc 289 ddhc 276 ddhc 283 ddhc 280 ddhc 280
55 56 57 58	287 185 294 191 301 195 307 201 313 206	259 237 274 284 243 280 270 248 288 278 254 292 282 280 298	183 255 188 280 193 286 198 272 203 278	302 279 300 be 309 288 307 be 315 292 314 be 322 298 320 be 329 304 327 be	dific 302 dific 309 dific 315 dific 322 dific 329
60 51 62 63	333 222	287 285 304 293 271 310 299 276 316 305 282 322	213 289 218 294	341 317 341 ba 348 323 347 ba	d/te 335 d/te 341 d/te 348 d/te 355
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aeroge	ls. Inc.											28 A	ugust,	2008	
Project No. 31													age 50		
, , , , , , , , , , , , , , , , , , , ,													3		
											21	August 2	2008		
	P8A	P8A	P8A	P8A	P8A	P8A	PBA	P8B	P8B	P8B	P8B	P8B			
Time		TC #10	Sec C-C TC #11	DDAve	Sec D-D TC#12	Sec D-D TC #13	Sec D-D TC #14	P8BMax	AAAve	Sec A-A	Sec A-A TC #2	Sec A-A TC #3			
(min)	(°F)	(°F)	(°F)	(°F)	(°F)	(*F)	(°F)			(°F)	(°F)	(°F)			
64 65	345 352	232 237	310 316	287 293	328 334	228 233	305 311	361 368	335 342	360 367	bad/to bad/to	361 368			
66	358	243	3.22	298	340	238	317	374	348	374	bad/to	374			
67 68	364 371	248 253	327 333	304 309	348 351	243 248	322 328	381 388	355 382	381 388	bad/to	381 388			
69 70	377 384	258 264	339 345	314	357 364	253 259	333 339	395 401	368 374	394 401	bad/to bad/to	395 401			
74 72	390 397	289 274	351 358	326 331	370 375	264 269	345 350	408 415	381 387	408	bad/to bad/to	408 415			
73 74	403 409	280 285	362 368	337 343	382 388	274 280	356 362	421 428	393 400	421 428	bad/to bad/to	421 428			
75	416	291	374	349	394	285	368	435	406	435	bad/to	435			
76 77	422 429	298 301	380 385	354 360	400 408	290 296	373 379	441	412	441	bad/to	441			
78 79	435 441	307 312	391 397	366 372	412 418	301 306	385 391	455 462	426 432	455 462	bad/to bad/to	454 461			
80 81	448 454	317	403 408	377 383	424 430	311	397 402	468 475	438 445	468	bad/to	458 474			
82 83	460 467	328	414	389 394	438 442	322 327	408 414	482 488	452 458	482 488	bad/to bad/to	481 487			
84 85	473 479	339	426 431	400 406	448 454	332 338	420 426	495 501	464	495 501	bad/to	494 501			
86 87	486 492	350 355	437 443	411 417	460 463	343 348	431	508 515	477 483	508 515	bed/to bad/to	507 514			
88 89	498 504	380 386	449 454	423 429	472 478	354 359	443 449	521 527	490 496	521 527	bad/to bad/to	520 527			
90 91	510	371 376	460	434 440	484 490	364	454 460	534	502	534	badito	533			
92	516 523	382	466 471	446	495	370 375	486	541 547	509 515	541 547	bad/to bad/to	540 546			
93 94	529 535	387 393	477 483	451 457	502 508	380 386	472 478	554 560	521 527	554 560	bad/to bad/to	553 559			
95 96	541 548	398 403	489	463 468	514 520	391 396	483 489	567 573	534 541	567 573	bad/to bad/to	566 573			
97 98 99	554 560	409 414	500 508	474 480	528 532	402 407	495 501	580 586	547 553	580 586	bad/to bad/to	579 586			
99 100	566 572	420 425	508 511 517	486 492	538 544	412 418	507 513	586 593 599	560 566	593 599	bad/to bad/to	592 599			
101	579 585	430 436	523 528	497 504	550 557	423 429	519 525	605 612	572 579	605 612	bad/to bad/to	606 612			
103 104	591 597	441 447	534 540	509 515	563 669	434 439	531 536	618 625	585 591	618 625	bad/to bad/to	618 625			
105	604 610	452 458	548 552	521 527	675 582	446 451	543 549	632	598 604	631 638	badito	632 638			
106 107	616	463	557	533	588	457	555	638 645	610	844	bad/to bad/to	645			
108 109	628	458 474	563 569	538 544	594 599	461 467	560 566	651 658	617 623	651 657	bad/to bad/to	651 658			
110 111	634 640	479 484	575 580	550 556	603 612	473 478	572 578	664 670	629 635	684 670	bad/tc bad/te	684 670			
112 113	647 653	490 495	598 592	562 568	618 625	483 489	584 590	677 683	641 647	676 682	bad/to bad/to	677 683			
114 115	660 666	502 507	598 603	574 580	631 637	495 501	596 602	690 696	654 660	689	bad/to bad/to	690 696			
116 117	672 678	513 518	609 615	586 591	643	506 511	608	702 709	666 673	701 708	bad/to bad/te	702 709			
118 119	684 690	524 529	621 625	597 603	655 661	517 523	620 625	715 721	679 685	714 720	bad/to bad/to	715 721			
120 121	898 702	534 540	632 638	609 614	687 673	528 533	631 637	728 734	691 697	728 732	bad/to bad/to	728 734			
122 123	708 714	545 550	843 849	620 626	679 685	539 544	643 648	740 746	703 709	739 745	bad/to bad/to	740 746			
124	720	555	654 660	631	691	549	654 660	753	718	751	badito	753			
125 126	726 733	560 567	686	637 643	696 703	564 561	666	759 765	722 728	757 763	bad/to bad/to	759 766			
127	739	573	672	650	710	567	672	771	734	769	bad/te	771			
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aer Project No	ogel . 31	s, inc 59033	}												igust, 2 ge 51 o	
													21	August 20	08	
	Time	TC #9	TC #10	P8A Sec C-C TC #11	P8A DDAve	TC#12	TC #13	P8A Sec D-D TC #14	,	P8B P8BMax	P8B AAAve	TC #1	TC #2	P8B Sec A-A TC #3		
•	min) 128 129	(*F) 745 751	(°F) 578 583	(°F) 677 683	(°F) 655 661	(°F) 716 722	(°F) 572 577	(*F) 678 684		778 784	740 748	(°F) 775 781	(°F) badito badite	(°F) 778 784		
	130 131 132	768 764 769	595 600	689 695 700	667 673 678	728 734 740	683 588 593	690 696 701		790 796 802	752 758 764	787 783 799	bad/to bad/to	790 796 802		
	133 134 135	775 782 788 795	604 610 618	706 712 718	684 690 696	746 752 759 768	598 604 610	707 713 719		808 814 820	769 775 781 787	805 811 817	bad/to bad/to bad/to	808 814 820		
	136 137 138 139	802 808 815	622 629 635 641	724 730 738 742	703 709 716 722	773 780 786	617 623 629 635	726 732 738 745		826 832 838 844	793 799 804	823 828 834 840	badito badito badito badito	826 832 838 844		
	140 141 142	822 829 835	647 654 660	748 764 760	729 736 742	793 801 807	642 649 655	751 758 764		850 856 861	810 816 822	845 851 857	bad/to bad/to bad/to	850 856 861		
	143 144 145 146	841 848 854 860	666 672 678 684	766 772 778 784	748 755 761 767	814 821 827 833	661 687 673 679	770 777 783 789		867 873 879 884	827 833 839 844	862 868 873 878	bad/to bad/to bad/to	867 873 879 884		
	147 148 149	867 873 880	690 693 703	789 795 801	774 780 786	840 846 853	686 692 698	796 802 808		890 896 901	850 855 861	884 890 895	bad/to bad/to bad/to	890 896 901		
	150 151 152	885 892 898	709 715 721	807 813 818	792 798 805	859 865 872	704 710 716	814 820 826		907 912 918	868 871 877	900 905 910	bad/to bad/to bad/to	907 912 918		
	153 154 155 156	904 910 916 922	727 733 739 745	824 830 838 841	811 817 823 829	878 884 891 897	722 728 734 740	833 838 844 851		923 929 934 939	882 888 893 898	916 921 926 931	bedfic bedfic bedfic bedfic	923 929 934 938		
	157 158 159	928 934 940	751 757 763	847 853 858	835 842 848	903 910 916	746 753 758	857 863 869		945 950 956	904 909 914	938 942 947	bad/to bad/to bad/to	945 950 956		
	160 161 162 163	946 952 958 965	709 775 781 787	884 870 878 882	854 860 865 872	922 928 933 941	764 771 776 783	875 881 886 893		961 966 972 977	919 925 930 935	952 957 962 987	badfic badfic badfic badfic	961 966 972 977		
	164 165 166	971 977 982	794 800 805	888 893 898	879 885 889	947 953 958	790 796 800	900 905 910		982 988 993	940 946 951	972 978 982	bad/to bad/to bad/to	982 988 993		
	167 168 169 170	988 993 998 1004	817 822 827	904 909 915 920	896 902 907 912	965 970 976 981	807 813 818 823	917 922 928 933		998 1003 1000	956 961 966 972	988 992 997	bad/to bad/to bad/to	998 1003 1009 1014		
	171 172 173	1012 1018 1026	834 841 849	927 933 939	919 927 934	988 995 1003	830 838 845	940 947 954		1014 1019 1024 1029	976 982 987	1003 1007 1013 1017	bad/to bad/to bad/to	1014 1019 1024 1029		
	174 175 176	1032 1038 1045	855 862 868	945 950 958	941 947 963	1010 1017 1023	852 859 865	960 986 972		1034 1030 1044	992 997 1002	1022 1027 1032	bad/to bad/to bad/to	1034 1039 1044		
	177 178 179 180	1050 1055 1062 1066	875 880 886 892	962 967 972 977	965 971 976	1029 1035 1040 1048	872 878 883 889	978 983 989 994		1049 1054 1059 1064	1007 1011 1016 1021	1037 1041 1046 1051	badito badito badito	1049 1054 1059 1064		
	181 182 183	1071 1077 1082	898 903 909	983 988 993	982 987 993	1051 1058 1083	895 900 906	1000 1005 1011		1089 1074 1079	1026 1031 1036	1056 1061 1065	bad/to bad/to bad/to	1089 1074 1079		
	184 185 186 187	1090 1093 1099 1108	915 920 928	999 1004 1009	999 1005 1010	1089 1074 1079 1088	912 918 923 931	1017 1022 1027		1084 1088 1093	1041 1048 1051	1070 1075 1079	bad/to bad/to bad/to	1084 1088 1093 1098		
	188 189 190	11 13 11 19 11 22	933 941 947 952	1015 1021 1027 1031	1017 1024 1030 1035	1093 1100 1104	938 946 950	1034 1040 1046 1051		1098 1103 1108 1112	1055 1060 1065 1070	1084 1089 1093 1098	badito badito badito	1103 1108 1112		
	191	1126	967	1036	1040	1109	955	1055		1117	1075	1103	bad/te	1117		
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerog Project No. 3			28 August, 2008 Page 52 of 95
Time (min) 192 193 194 196 197 197 197 202 203 204 205 207 201 201 201 201 202 203 204 205 207 208 209 201 201 201 201 201 201 201 201 201 201	(*F) (*F) (*F) (*F) 1133 984 1042 1143 977 1053 1145 977 1053 1150 983 1058 1156 989 1094 1161 904 1055 1161 904 1055 1161 904 1055 1161 904 1055 1161 1007 1074 1174 1008 1184 1023 1086 1188 1023 1086 1188 1023 1086 1198 1028 1098 1198 1028 1098 1199 1049 1118 1209 1049 1118 1201 1055 1105 1208 1066 1114 1209 1049 1118 1217 1056 1123 1220 1061 1123 1220 1061 1123 1221 1068 1133 1233 1072 1139 1242 1084 1143 1255 1089 1163 1255 1099 1162 1256 1199 1162 1267 1174 1180 1273 1120 1183 1277 1120 1183 1277 1120 1183 1277 1120 1183 1277 1120 1183 1277 1120 1183 1277 1120 1183 1277 1120 1183 1277 1120 1183 1277 1120 1183 1277 1120 1183 1277 1171 1180 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1287 1136 1201 1288 1159 1224 13018 1189 1224 13018 1189 1224 1315 1167 1223 1315 1167 1223 1315 1177 1253 1315 1177 1253 1315 1177 1253 1315 1177 1253 1315 1177 1253 1315 1177 1253	P8A P8A Sep D-D Sec D-	PBB
Mex A	1 1331 1191 1253 1200 1200 1200	1262 1325 1190 1270 1000 1200 1200 1200	1315 1280 1304 badde 1315 1200 1200 1200 1200 1200 1200



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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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	P8B P8E	. P8B P8B	P8B P8B	PSB PSB	P8B P8B	21 Augu	
Time (min)	Sec A-A Sec A-A TC #4 TC #5 (*F) (*F)	Sec B-B BBAve TC#6	Sec B-B Sec B-B TC #7 TC #8 (°F) (°F)	Sec C-C CCAve TC #9 (°F)	Sec C-C Sec C-C TC #10 TC #11 (°F) (°F)	Sec D-D Sec D-DDAve TC#12 TC#1	D 3
0 1 1 2 3 4 5 6 7 7 8 8 9 9 11 11 12 13 14 14 15 16 16 17 18 19 10 10 10 10 10 10 10 10 10 10 10 10 10	82 82 82 82 82 82 82 82 82 82 82 82 82 8	82 82 82 82 82 82 82 82	82 82 82 82 82 82 82 82 82 82 82 82 82 8	83 82 83 83 83 83 83 83 83 81 83 82 84 84 85 85 86 88 88 87 87 87 87 88 86 98 98 96 90 92 91 93 92 91 93 92 91 93 92 91 93 92 91 93 92 91 93 96 94 98 95 100 98 102 100 105 102 108 104 111 106 114 109 118 113 122 119 131 127 144 135 151 151 172 191 172 194 173 194 174 175 178 178 204 178 204 178 204 178 204 178 204 179 217 179 217 17	83 83 83 83 83 83 83 83 83 83 83 83 83 8	82 83 8 8 82 83 83 84 83 84 83 84 82 84 82 84 82 84 82 85 83 86 83 86 83 86 83 86 87 90 87 90 87 90 90 90 90 90 90 90 90 90 90 90 90 90	12 12 12 12 12 13 14 14 16 16 16 16 16 16 16 16 16 16 16 16 16
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aero Project No.													28 Aug Pag	gust, 2008 e 54 of 95
												21	August 200	8
Tirr (mi		Sec A-A	P8B BBAve	P8B Sec B-B TC #6 (*F)	P8B Sec B-B TC #7 (°F)	P8B Sec B-B TC #8 (*F)	P8B CCAve	P8B Sec C-C TC #9 (°F)	P8B Sec C-C TC #10 (°F)	P8B Sec C-C TC #11 (°F)	P8B DDAve	P8B Sec D-D TC #12 (°F)	P8B Sec D-D TC #13 (°F)	
	4 312 5 316 6 326 7 331	314 320	308 315 321 327	338 345 361 368	242 248 254 259	344 351 357 363	299 308 311 318	339 346 351 358	236 242 247 253	323 330 335 342	296 302 308 314	342 348 354 360	229 234 240 245	
6	18 337 19 343 10 349 11 359	333 339 345	333 339 346 352	365 371 378 385	285 271 277 282	370 376 383 389	323 329 335 341	384 370 377 383	258 263 269 274	348 354 360 368	319 325 332 337	388 372 379 385	250 256 261 286	
	2 362 3 368 4 374	367 363 389	358 364 370 377	391 398 404	288 283 299 304	396 402 408	348 353 359 366	390 395 402	280 285 291 296	373 379 385 392	343 349 355	391 397 403	271 277 282 287	
1	75 386 76 386 77 393 78 396 79 405	381 388 394	383 389 395	411 417 424 431 437	310 315 321	415 421 427 433	371 377 383	409 415 421 427 433	301 307 312 318	396 404 410 416	361 387 373 379	410 416 423 429	293 298 303 309	
	00 411 01 418 02 424 03 430	408 412 419	401 407 414 419 426	444 451 457 464	327 332 338 343 349	439 446 452 458 464	389 395 401 407 413	440 446 452 458	323 329 335 340	423 429 435 441	385 391 397 403 409	435 441 447 454 460	314 320 325 331	
8	M 436 15 445 17 455	431 437 443	432 438 444 450	470 476 483 489	355 360 365 371	471 477 483 489	420 425 431 437	465 471 477 483	346 351 356 362	448 454 460 488	415 421 427 433	486 472 479 485	336 342 347 353	
1	17 45: 18 46: 19 46: 10 47:4 11 48:	456 462 468	456 462 468 474	498 502 509 515	377 382 388 393	495 501 507 513	443 449 455 461	490 495 502 508	367 373 378 384	472 478 484 491	438 444 451 457	485 491 497 504 510	358 363 369 375	
9	12 486 13 492 14 498	480 486 492	480 488 492	521 528 534	389 405 410	520 526 532	487 473 478	514 521 528	389 395 400 406	497 503 509	489 475 481	517 523 529	380 386 391	
	85 505 86 511 87 517 88 523 89 528	505 511 517	498 504 510 516 522	540 547 553 559 568	416 421 426 432 437	538 544 550 556 562	485 490 496 502 508	533 539 545 552 558	411 417 422 428	515 521 527 533 539	487 493 499 505	536 542 548 555 561	397 403 408 413 419	
10 10 10	00 535 01 542 02 545	630 536 542	528 534 539 546	572 578 584 591	443 449 454 459	568 575 580 587	514 520 526 532	564 570 577 583	433 439 444 450	545 551 557 563	511 517 523 529	567 574 580 586	426 430 436 441	
10 10 10	4 560 5 561 6 573	664 660 567	562 568 564 569	607 604 610 616	465 470 476 481	593 599 605	538 544 550 555	589 595 602 608	455 461 466 471	569 575 581 587	535 542 547 554	593 599 605 612	447 463 458 464	
10 10 11	8 585 9 591 10 591	579 585 591	575 581 588 593	622 629 635 641	487 492 498 503	617 623 630 635	567 573 579	614 620 626 632	477 482 488 493	593 599 605 611	560 566 572 578	618 625 631 637	470 475 481 486	
11 11 11	2 609 3 615 4 623	603 609 616	599 605 611 617	647 653 659 666	509 514 520 525	642 648 654 660	584 590 596 602	638 644 651 657	498 504 509 515	617 622 628 634	584 590 598 602	644 650 656 662	492 497 503 508	
1: 1: 1:	6 634 7 646 8 646	628 634 640	623 629 634 640	672 678 684 690	531 538 541 547	666 672 678 684	608 613 619 625	663 669 675 681	520 525 530 536	648 648 652 658	608 614 620 627	669 675 681 687	514 520 525 531	
12 12 13 13	0 850 1 864 12 670	652 658 684	646 652 658 663	698 702 708 714	552 557 563 568	690 696 702 708	630 636 642 648	687 693 699 705	541 546 552 557	683 689 675 681	633 639 645 651	694 700 706 712	536 542 547 553	
12 12 12 13	M 662 5 688 6 694	682 688	675 680 686	720 726 732 738	573 579 584 589	714 719 726 731	659 665 670	711 717 723 729	563 568 573 578	688 692 698 704	657 663 669 674	719 725 731 737	558 564 569 574	
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Ae Project No															gust, 2008 ge 55 of 95
													21	August 20	08
	Time (min)	P8B Sec A-A TC #4 (*F)	P8B Sec A-A TC #5 (°F)	P8B BBAve	P8B Sec B-B TC #6 (*F)	P8B Sec B-B TC #7 (°F)	P8B Sec B-B TC #8 (*F)	P8B CCAve	P8B Sec C-C TC #9 (°F)	P8B Sec C-C TC #10 (°F)	P8B Sec C-C TC #11 (°F)	P8B DDAve	P8B Sec D-D TC #12 (°F)	P8B Sec D-D TC #13 (°F)	
	128 129 130 131	708 712 718 724	700 705 711 717	692 698 703 709	744 750 766 762	595 600 605 610	737 743 749 755	676 682 687 693	735 741 747 753	583 589 594 599	709 715 721 727	680 686 692 698	743 749 756 762	580 585 591 596	
	132 133 134 135	730 735 741 747	723 729 735 741	715 721 726 732	768 774 779 785	616 621 626 632	761 767 773 778	704 709 715	759 765 770 778	604 609 615 620	732 738 743 749	704 710 715 721	768 774 780 786	602 607 612 618	
	136 137 138 139	763 769 764 770	746 752 758 763	737 743 749 754	791 797 803 808	637 642 647 653	784 790 796 802	721 726 731 737	782 788 793 799	625 630 635 640	755 760 766 771	727 732 738 744	792 798 804 810	623 628 633 639	
	140 141 142 143 144	778 782 788 793 799	769 775 780 786 792	760 765 771 776 782	814 820 825 831 837	658 663 669 674 679	807 813 819 824 830	742 748 753 759 784	805 811 816 822 828	645 651 656 661 666	777 782 788 793 799	750 756 761 767 773	816 822 828 834 840	644 650 656 660 666	
	145 146 147 148	805 810 816 821	797 803 808 814	787 793 798 804	842 848 863 859	684 690 695 700	835 841 846 852	769 775 780 788	833 839 844 850	671 677 682 687	809 815 821	778 783 789 785	845 851 867 863	671 676 682 687	
	149 150 151 152 153	827 833 838 843 849	819 825 830 836 841	809 814 820 825 830	869 875 880 885	705 711 718 721 727	857 863 868 873 878	791 798 801 807 812	855 861 866 871 877	692 697 702 708 713	825 831 838 841 847	806 811 816 822	868 874 880 885 891	692 698 703 708 714	
	154 155 156 157	859 865 871	847 852 857 862	836 841 845 852	896 901 907	732 737 742 748	884 889 895 900	817 822 828 833	882 887 893 898	718 723 728 734	852 857 862 868	827 833 838 844	897 902 907 913	719 724 729 735	
	158 159 160 161 162	876 881 886 892 897	868 873 878 883 889	857 862 867 872 878	912 917 922 928 933	753 758 763 768 774	906 911 916 921 926	839 844 849 854 859	904 909 914 919 925	739 744 749 754 759 764	873 878 883 888 894	849 854 860 865 870	919 924 930 935 941	740 745 751 756 761	
	163 164 165 166	902 908 913 918	894 899 904 910	883 888 893 898	938 943 948 963	779 784 789 794	932 937 942 947	864 869 875 880	930 935 941 946	769 774 779	904 909 914	875 881 886 891	946 952 957 982	786 772 777 782	
	167 168 169 170 171	924 929 934 939 944	915 920 925 930 935	904 909 914 919 924	969 964 969 974 979	799 805 810 815 820	953 958 963 968 973	885 890 895 900 905	951 956 961 967 972	785 790 794 800 804	919 924 929 934 939	902 908 913 918	968 973 979 984 989	787 792 798 803 808	
	172 173 174 175	950 955 960 965	941 945 960 965	929 934 939 945	984 989 994 900	825 830 835 841	979 984 989 994	910 915 920 925	977 982 987 992	810 814 819 824	944 949 954 950	923 928 933 938	995 1000 1005 1010	813 818 824 829	
	176 177 178 179 180	970 975 980 985 990	960 965 970 975 980	950 955 960 965 970	1004 1009 1014 1019 1024	843 851 853 861 866	1004 1009 1014 1019	930 935 940 945 950	997 1002 1007 1012 1017	829 835 839 845 850	984 989 973 978 983	943 949 954 959 964	1015 1021 1026 1031 1036	834 839 844 849 854	
	181 182 183 184	995 1000 1005 1010	985 990 995 1000	974 980 985 990	1028 1033 1038 1043	871 877 882 887	1024 1029 1034 1039	955 960 965 970	1022 1027 1031 1037	854 860 865 870	988 993 998 1002	989 974 979 984	1041 1046 1051 1056	860 865 870 875	
	185 186 187 188 189	1015 1020 1025 1030 1035	1005 1010 1014 1019 1024	995 999 1004 1009 1014	1048 1053 1057 1062 1067	892 897 902 907 912	1044 1048 1053 1056 1063	974 979 984 989 989	1041 1048 1051 1058 1061	875 880 885 890 895	1007 1012 1017 1021 1026	989 994 999 1004 1009	1081 1086 1071 1076 1081	886 891 896 901	
	190 191	1040 1045	1029 1034	1019 1024	1072 1076	917 922	1068	999 1004	1066 1070	900 905	1031 1036	1014 1019	1086 1090	906 911	
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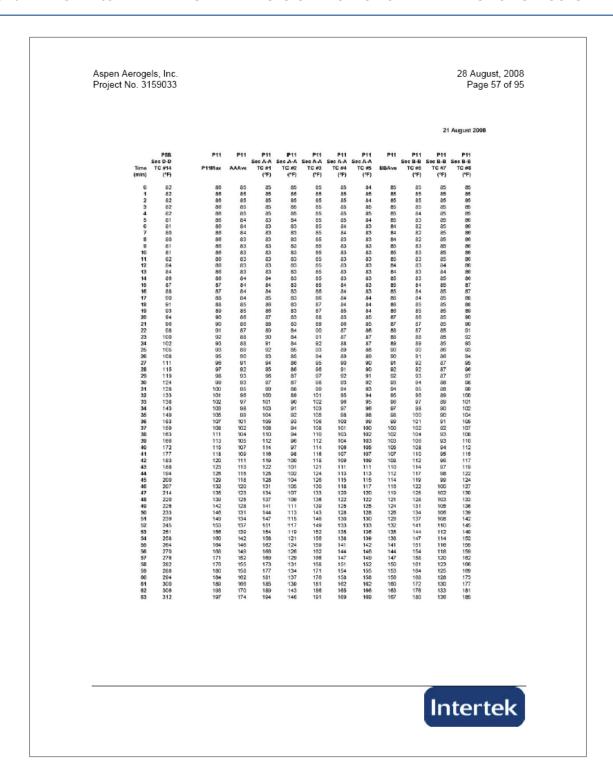
Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen As Project N															ugust, age 56	
													21	August 2	008	
	Time (min)	P8B Sec A-A TC #4 (*F)	P8B Sec A-A TC #5 (*F)	P8B BBAve	P8B Sec B-B TC #6 (*F)	P8B Sec B-B TC #7 (°F)	P8B Sec B-B TC #8 (*F)	P8B CCAve	P8B Sec C-C TC #9 (°F)	P8B Sec C-C TC #10 (°F)	P8B Sec C-C TC #11 (°F)	P8B DDAve	P8B Sec D-D TC #12 (°F)	P8B Sec D-D TC #13 (°F)		
	192 193 194 195	1049 1054 1059 1064	1039 1043 1048 1052	1029 1034 1038 1043	1081 1086 1090 1095	927 933 938 943	1078 1082 1087 1092	1008 1013 1018 1023	1075 1080 1085 1089	910 915 920 925	1040 1045 1050 1054	1024 1029 1033 1038	1095 1100 1105 1110	916 921 926 931		
	196 197 198 199	1069 1073 1078 1083	1058 1062 1067 1072	1048 1052 1057 1062	1100 1104 1109	948 952 957 962	1097 1101 1108 1111	1028 1032 1037 1042	1094 1099 1103 1108	930 934 939 944	1059 1064 1068 1073	1044 1048 1053 1058	1115 1119 1124 1129	937 942 947 952		
	200 201 202 203	1097 1092 1097 1101	1076 1081 1085 1090	1087 1072 1076 1081	1118 1123 1127 1132	988 973 977 982	1115 1120 1125 1129	1047 1051 1056 1061	1113 1117 1122 1126	949 954 959 964	1078 1082 1087 1092	1083 1068 1072 1077	1133 1138 1143 1147	957 962 967 972		
	204 205 206 207	1108 1111 1115 1120	1095 1099 1104 1108	1098 1090 1095 1100	1138 1141 1145 1160	987 992 997 1002	1134 1138 1143 1148	1065 1070 1075 1079	1131 1135 1140 1144	989 974 979 984	1098 1101 1105 1110	1082 1087 1091 1096	1152 1157 1161 1166	977 982 987 992		
	208 209 210 211	1124 1129 1133 1137	1113 1118 1122 1126	1104 1109 1114 1118	1154 1159 1163 1167	1007 1012 1017 1022	1152 1157 1161 1165	1084 1088 1093 1097	1149 1153 1157 1161	989 993 998 1003	1114 1118 1123 1127	1100 1105 1109 1114	1170 1174 1179 1183	997 1002 1006 1011		
	212 213 214 215	1142 1146 1151 1155	1131 1135 1140 1144	1123 1127 1132 1138	1172 1176 1181 1185	1027 1032 1037 1041	1170 1174 1178 1183	1102 1106 1111 1115	1166 1170 1174 1178	1018 1018 1022	1132 1136 1141 1145	1119 1124 1128 1132	1188 1192 1197 1201	1016 1022 1026 1031		
	216 217 218 219	1159 1164 1168 1172	1148 1153 1157 1161	1141 1145 1150 1154	1189 1193 1197 1201	1048 1051 1056 1061	1187 1191 1196 1200	1120 1124 1129 1133	1183 1187 1191 1195	1027 1032 1037 1041	1149 1153 1158 1162	1137 1141 1146 1150	1205 1209 1214 1218	1036 1041 1046 1051		
	220 221 222 223 224	1176 1180 1184 1189 1193	1168 1170 1174 1178 1182	1159 1163 1167 1172 1176	1206 1210 1214 1218 1222	1088 1070 1075 1080 1084	1204 1208 1212 1217 1221	1137 1141 1145 1150 1154	1199 1203 1207 1211 1215	1046 1051 1055 1060 1065	1166 1170 1174 1179 1183	1155 1159 1163 1168 1172	1222 1226 1230 1234 1238	1055 1080 1095 1070 1074		
	225 226 227 228	1197 1201 1205 1209	1187 1191 1195 1199	1180 1184 1188 1192	1226 1230 1234 1237	1089 1094 1098 1103	1225 1229 1233 1236	1159 1163 1167 1171	1219 1223 1227 1231	1070 1074 1079 1083	1187 1191 1195 1190	1176 1180 1185 1189	1242 1246 1250 1254	1079 1084 1089 1093		
	229 230 231	1213 1217 1221 1226	1203 1207 1211 1215	1198 1200 1204 1209	1241 1245 1249 1263	1107 1112 1116 1121	1240 1244 1248 1252	1175 1179 1183 1188	1235 1238 1242 1246	1088 1092 1097 1102	1203 1207 1211 1215	1193 1197 1201 1205	1258 1261 1265 1269	1098 1102 1107		
	232 233 234 235 236	1228 1232 1236 1240	1219 1222 1226 1230	1213 1216 1220 1224	1257 1260 1264 1268	1125 1129 1134 1138	1256 1260 1263 1267	1191 1195 1199 1203	1250 1254 1257 1261	1106 1110 1115 1119	1218 1222 1226 1230	1209 1213 1217 1221	1273 1277 1280 1284	1116 1120 1124 1129		
	237 238 239 240	1243 1247 1251 1255	1234 1238 1241 1245	1228 1232 1238 1240	1272 1275 1279 1283	1142 1147 1151 1155	1271 1275 1278 1283	1207 1211 1215 1219	1264 1268 1272 1276	1124 1128 1132 1136	1234 1238 1242 1246	1225 1228 1233 1237	1288 1291 1295 1299	1133 1137 1142 1146		
	Max To Max A	1255 1200	1245 1200	1240 1000	1283 1200	1155 1200	1283 1200	1219 1000	1276 1200	1136 1200	1248 1200	1237 1000	1299 1200	1146 1200		





Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL





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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerogels, Inc. Project No. 3159033										28 Aug Pag	gust, 2008 e 58 of 95
									21	August 200	8
P8B Sec D-D Time TC #14 (min) (*F)	P11 P11Max A	P11 P1 Sec A- MAVE TC #	Sec A-A	P11 Sec A-A TC #3 (*F)	P11 Sec A-A TC #4 (°F)	P11 Sec A-A TC #5 (°F)	P11 BBAve	P11 Sec B-B TC #6 (°F)	P11 Sec B-B TC #7 (°F)	P11 Sec B-B TC #8 (°F)	
64 318 65 324 66 330 67 338	202 208 210 214	178 19 182 20 186 20 190 21	4 152 9 156 4 159	198 200 205 210	173 177 180 184	173 177 180 185	171 175 179 182	185 189 194 198	138 141 144 147	190 194 198 202	
68 342 69 348 70 355 74 361	219 224 229 234	195 21 199 22 203 22 208 23	9 162 4 166 9 169 4 173	215 220 224 229	188 192 197 201	189 193 197 202	187 191 195 199	203 208 212 217	150 154 157 160	207 211 216 220	
72 367 73 373 74 379 75 366 76 392	239 244 248 253 258	212 23 216 24 221 24 225 25 230 25	4 181 8 185 3 189	234 238 243 248 252	205 209 214 218 222	206 210 215 219 223	203 207 211 216 220	221 226 230 235 239	164 168 171 175 179	224 228 233 237 241	
77 398 78 404 79 410 80 417	263 267 272 277	234 26 239 26 243 27 247 27	3 197 7 201 2 206 7 209	267 262 266 271	227 231 235 239	228 232 237 241	224 228 232 238	244 248 253 257	182 186 190 194	245 250 254 258	
81 423 82 429 83 436 84 442 85 448	282 288 291 296 301	252 28 256 28 261 29 265 29 270 30	3 217 1 221 3 225	276 281 286 290 295	244 248 263 257 262	246 250 254 259 263	241 245 249 253 257	262 266 271 275 279	197 201 205 209 213	263 267 271 276 280	
86 454 87 460 88 466 89 473	305 310 315 320	275 30 279 31 284 31 288 32	5 234 0 238 5 242 0 246	305 305 309 314	266 271 275 280	268 272 277 281	262 266 270 275	284 288 293 297	217 221 225 229	285 289 293 296	
90 479 91 485 92 491 93 498 94 504	324 329 334 338 343	293 32 297 32 302 33 308 33 311 34	9 255 4 259 3 264	319 323 328 333 338	284 288 293 297 302	286 290 294 299 303	279 283 287 292 296	301 306 310 315 319	233 237 241 245 249	307 311 315 320	
95 510 96 516 97 523 98 529	348 353 357 362	315 34 320 35 324 35 329 36	3 272 3 276 7 281 2 285	343 347 352 357	306 311 316 320	307 312 316 321	300 305 309 313	323 328 332 336	253 257 261 265	324 329 333 338	
99 535 100 541 101 548 102 554 103 560	367 372 376 381 385	334 36 338 37 343 37 347 38 352 38	2 294 3 298 1 302	362 367 371 376 381	325 329 334 338 343	325 330 334 339 343	317 322 328 330 334	341 345 349 354 358	269 273 277 281 285	342 347 351 356 360	
104 566 105 573 106 579 107 585	391 398 401 405	367 39 361 39 366 40 371 40	311 316 319 324	386 391 396 401	348 352 357 362	347 352 356 361	339 343 348 352	363 367 372 376	289 293 297 301	366 369 374 379	
108 591 109 598 110 604 111 610 112 617	410 415 420 424 429	375 41 380 41 384 42 389 42 393 42	332 337 4 341	405 410 415 420 425	366 371 375 380 385	365 370 374 379 383	358 361 365 369 373	385 389 394 398	305 309 313 317 321	383 388 392 396 401	
113 623 114 629 115 635 116 641	434 439 444 448	398 43 403 43 407 44 412 44	4 350 9 354 4 358 3 362	430 435 439 444	389 394 399 403	388 393 397 401	378 382 387 391	403 407 412 416	325 329 333 337	406 410 415 419	
117 647 118 654 119 662 120 868 121 675	453 458 463 467 472	417 45 421 45 426 46 430 46 435 47	371 3 376 7 380	449 454 458 463 488	408 412 417 422 426	406 410 415 419 424	395 399 404 408 413	420 425 429 434 438	341 345 349 353 358	424 428 433 437 442	
122 681 123 667 124 694 125 700	477 481 488 491	439 47 444 48 448 48 463 49	7 388 1 393 3 397 1 402	473 478 482 487	431 438 440 445	428 433 437 442	417 421 428 430	443 447 452 456	362 366 370 374	447 451 456 460	
126 708 127 712	498 500	458 49 462 50		492 497	450 454	446 451	434 439	460 465	378 382	465 469	
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Aspen Aerogels, Inc. Project No. 3159033												st, 2008 59 of 95
										21	August 2008	
P8B Sec D-D Time TC #14 (min) (*F)	P11 P11Max	P11	P11 Sec A-A TC #1 (°F)	P11 Sec A-A TC #2 (*F)	P11 Sec A-A TC #3 (*F)	P11 Sec A-A TC #4 (°F)	P11 Sec A-A TC #5 (°F)	P11 BBAve	P11 Sec B-B TC #6 (°F)	P11 Sec B-B TC #7 (°F)	P11 Sec B-B TC #8 (°F)	
128 718 129 724 130 730	505 510 514	467 472 476	505 510 614	415 419 423	501 508 511	459 463 468	455 460 464	443 447 452	489 474 478	386 390 394	474 478 483	
131 738 132 742 133 748 134 754	519 524 528 533	481 485 489 494	519 524 528 533	427 432 436 440	516 520 525 530	472 477 481 486	469 473 477 482	458 461 464 469	483 487 491 496	398 403 406 411	487 492 496 501	
135 760 136 765 137 771	538 542 547	499 503 508	538 542 547	445 449 453	535 539 544	491 495 500	486 491 495	473 478 482	500 505 509	415 419 423	505 510 515	
138 777 139 783 140 789 141 795	562 556 561 565	512 517 521 526	556 561 565	467 462 466 470	553 558 563	504 509 513 518	504 509 513	487 491 495 499	518 522 527	427 431 435 439	519 523 528 632	
142 800 143 806 144 812 145 817	570 575 579 584	531 535 539 544	570 575 579 584	475 479 483 487	568 572 577 581	522 527 531 536	518 622 526 531	504 508 512 516	531 536 540 544	443 447 451 455	537 642 548 550	
146 823 147 828 148 834	588 593 598	548 663 557	588 693 598	491 496 500	586 590 595	540 545 549	535 640 544	521 626 529	549 553 557	459 463 467	555 659 564	
149 839 150 845 151 850 152 855	602 607 611 616	568 571 575	602 607 611 616	504 509 513 517	600 604 609 613	558 563 567	548 553 557 561 566	534 538 542 547	562 566 570 575	472 475 480 484	568 572 577 581	
153 861 154 866 155 872 156 877	620 624 629 633	579 583 588 592	620 624 629 633	521 525 529 534	618 622 627 631	571 576 580 584	586 570 574 579	551 555 558	579 583 588 592	488 492 496	586 590 594 599	
157 883 158 888 159 893	838 842 647	597 601 605	638 642 647	538 542 546	636 640 645	589 593 597	583 587 591	564 568 572 576	598 601 605	500 504 508 512 516	603 607 611	
160 899 161 904 162 909 183 914	651 655 660 664	614 618 622	651 655 660 664	550 555 559 563	649 653 658 662	602 606 610 615	596 600 604 608	580 584 589 593	609 613 618 622	520 524 528	616 620 624 629	
164 920 185 925 186 930 167 935	690 873 677 682	627 631 635 640	669 673 677 682	667 671 675 579	671 676 680	619 623 628 632	613 617 621 625	601 605 610	626 630 634 639	532 536 540 544	633 637 642 646	
168 940 169 946 170 951	686 690 695	644 648 662	686 690 695	683 687 691	684 689 693	636 641 645	629 634 638	613 618 622	643 647 651	544 647 552 655	650 654 659	
171 958 172 961 173 966 174 971	699 703 708 712	656 665 670	699 703 708 712	595 599 603	702 706 711	649 653 658 662	642 646 650 655	626 630 634 638	656 660 664 668	559 563 567 571	663 667 671 676	
175 976 176 981 177 986 178 991	716 721 725 729	673 678 682 686	716 721 725 729	611 616 620 624	715 719 724 728	668 670 675 679	650 663 667 671	643 647 650 655	673 677 681 685	575 579 582 586	680 684 688 693	
179 996 180 1001 181 1006	733 738 742	690 695 600	733 738 742	628 632 636	732 736 741	683 687 691	676 680 684	659 663 667	689 693 697	590 594 598	697 701 706	
182 1011 183 1016 184 1021 185 1026	748 751 755 759	703 707 711 715	748 751 755 759	640 644 648	745 749 753 758	700 704 708	688 692 696 700	671 675 679 683	701 706 710 714	602 609 613	709 713 717 722	
186 1031 187 1035 188 1041 189 1045	763 767 771 776	719 724 728 732	763 767 771 776	656 660 664 668	762 766 770 775	712 716 721 725	704 709 713 717	687 691 695 699	718 722 726 730	617 621 625 629	726 730 734 738	
190 1050 191 1055	780 784	736 740	780 784	672 676	779 783	729 733	721 725	703 707	734 738	633 637	742 746	
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aerogels, Inc. Project No. 3159033				28 August, 2008 Page 60 of 95
P88 Sec 0-0 Time TC #14 (min) ("F)	P11Max AAAve T0	P11 P11 P11 P1 c A-A Sec A-A Sec A-A Sec A- TC #1 TC #2 TC #3 TC # (*F) (*F) (*F) (*F)	1 P11 P11 P11 P11 A Sec A-A Sec B-B Sec B-B S 4 TC#5 BBAve TC#6 TC#7	August 2008 P11 Fice B-B TC #8 (*F)
192 1068 193 1865 194 1869 195 1879 1979 1979 1979 1979 1979 1980 1981 1982 1983 200 1999 201 1107 203 1112 204 1116 205 1121 206 1125 207 1130 208 1134 211 1148 211 1152 211 1161 216 1165 217 117 218 1167 218 1167 218 1167 218 1170 218 1170 218 1170 218 1187 219 1182 219 1182 220 1187 221 1191 222 1191 222 1191 223 1291 224 1291 225 1207 226 1221 227 1216 228 1221 229 1223 220 1223 220 1223 220 1227 221 1231 222 1235 223 1238 223 1238 223 1238 224 1242 225 1266 227 1266 228 1237 229 1223 220 1223 220 1227 221 1231 222 1235 223 1238 223 1238 224 1242 225 1266 227 1266 227 1266 228 1237 229 1223 220 1223 220 1223 220 1223 220 1223 221 1246 222 1246 223 1246 223 1246 224 1242 225 1246 227 1265 228 1246 227 1265 228 1246 227 1265 228 1246 227 1265 228 1246 228 1249 229 1223 220 1223 220 1223 221 1246 222 1246 223 1246 225 1246 227 1265 228 1246 227 1265 228 1257 228 1265 228 1265 228 1265 228 1265 228 1265 228 1265 228 1265 228 1265 228 1265 228 1265	7902 748 7907 765 801 767 805 761 808 765 813 769 817 777 825 781 820 778 820 781 821 788 821 788 822 788 824 788 824 788 825 810 825 810 826 810 827 818 828 822 827 828 828 828 828 828 828 838 828 828 839 842 848 828 828 859 842 859 848 828 859 842 859 859 842 859 859 842 859	788 680 787 737 702 684 701 731 702 684 705 744 707 682 790 744 601 682 790 744 605 692 790 744 605 693 701 818 75 613 704 812 76 817 709 814 78 820 717 824 77 830 721 828 77 830 721 828 73 843 733 841 79 843 733 841 74 855 745 853 80 864 753 853 80 864 753 85 83 80 867 749 857 80 86 867 739 85 83 81	1 733 715 747 644 746 779 751 654 8 757 779 751 654 9 742 723 755 652 9 777 742 727 759 656 8 758 737 753 763 660 9 782 743 775 667 9 784 745 727 759 671 9 784 795 743 775 671 9 784 795 797 799 675 9 785 797 799 695 9 785 797 799 695 9 785 797 799 695 9 785 797 799 695 9 785 797 799 695 9 785 797 799 695 9 785 797 799 695 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 785 775 808 702 9 8 791 771 804 9 8 791 771 804 9 8 791 771 804 9 8 791 771 804 9 8 8 791 771 804 9 8 8 791 771 804 9 8 8 791 771 804 9 8 8 8 791 775 9 8 8 8 791 775 9 8 8 8 8 8 8 791 775 9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 7 8	751 758 768 7787 7787 7787 787 787 787 787 787
Max T 1265 Max A 1200		985 872 976 92 1200 1200 1200 1201	0 1200 1000 1200 1200	tertek



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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

Aspen Aeroge Project No. 31	s, Inc. 59033	28 August, 2008 Page 61 of 95
		21 August 2008
Time (min)	P11	P14 P14 P14 P14 Sec A-A Sec A-A P14 Max AAAve T0 TC #2 ("F) ("F)
0 1 1 2 3 3 4 4 5 6 6 7 7 8 8 9 10 0 11 11 12 2 11 14 14 15 16 16 17 7 18 18 9 20 21 2 2 3 2 2 5 2 2 7 2 2 3 3 3 3 2 5 3 3 3 3 4 4 4 5 6 6 7 7 8 8 9 6 6 1 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	85 85 85 85 85 85 85 86 86 86 86 85 85 85 85 85 85 85 85 85 85 85 85 85	84 82 82 82 82 82 83 82 82 84 82 82 82 82 82 82 82 82 82 82 82 82 82
		Intertek



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P11	Aspen Aer Project No	rogels,). 3159(Inc. 033										28 / P	August, 2008 age 62 of 95
			B44 B44	D44	D44	B44	B14	D44	B44	B44	B1/			2008
66 170 180 140 206 185 100 151 202 177 122 131 100 166 167 167 167 167 167 167 167 167 167		Time CC	Sec C-C Ave TC#9	Sec C-C S TC #10	TC #11		Sec ID-D	Sec D-D TC #13	TC #14			Sec A-A TC #1	Sec A-A TC #2	
		65 65 65 65 65 65 65 65 65 65 65 65 65 6	170	142 148 149 149 149 149 149 149 149 149 149 149	208 227 228 248 268 269 271 289 289 289 289 299 299 299 299 299 299	185 189 189 189 189 189 189 189 189 189 189	1909 203 207 212 214 224 224 224 225 226 226 227 227 227 227 227 227 227 227	151 155 156 169 169 169 169 169 169 169 169 169 16	204 208 213 217 222 228 228 229 229 229 229 229 229 229	107 107 108 108 108 108 108 108 108 108 108 108	12241 12881 13021 13441 13121 13441 14131 14141 14161	131 134 138 138 138 138 138 138 138 138 138 138	100 101 113 115 115 115 115 115 115 115 115 11	
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Aspen Aerog Project No. 3	els, Inc. 159033					28 August, 2008 Page 63 of 95
						21 August 2008
Time (min)	P11 P1 Sec C-4 CCAve TC #	Sec C-C Sec C-C	P11 P11 P11 Sec ID-D Sec D-D S DDAve TC #12 TC #13 4*F) (*F)		Max AAAve TO	P14 P14 A-A Soc A-A : #1 TC #2 (*F) (*F)
128 129 130	443 48 447 48 461 47	385 489 389 493	451 473 394 455 478 399 460 482 403 464 486 407	490 494	360 320 373 323	343 278 346 281 350 285 354 288
131 132 133 134	458 47 460 48 464 48 469 49	397 502 401 507 405 511	468 491 411 473 495 415 477 500 419	503 508 512	380 330 384 334 388 338	367 291 361 295 365 298
135 136 137 138	473 49 477 49 482 50 486 50	413 520 417 525	481 504 423 488 609 427 480 513 432 495 518 436	522 526	395 345 399 349	969 301 372 305 376 308 380 311
139 140 141	490 51: 494 51: 498 62	425 533 429 538 433 642	499 522 440 503 526 444 508 631 448	535 540 544	406 356 409 359 413 363	384 315 387 318 391 322
142 143 144 145	503 52 507 62 512 53 516 53	441 551 448 558	512 535 452 516 540 456 521 544 460 525 549 465	553 558	421 371 424 375	395 325 399 329 403 332 406 336
146 147 148 149	520 54 625 64 529 55 533 55	454 564 458 569 482 573	530 553 469 634 657 473 538 561 477 542 506 481	567 671 578	432 382 438 386 439 390	410 339 414 342 418 346 422 349
150 151 152	537 58 541 56 545 56	470 582 473 586 478 590	548 570 485 551 574 489 555 579 493	584 589 593	447 397 450 401 454 404	425 353 429 356 433 360
153 154 155 156	549 57 554 57 558 58 562 58	485 599 489 603	559 583 497 563 587 501 568 591 506 572 596 510	602 606	462 412 465 415	437 364 441 367 444 370 448 374
157 158 159 160	568 58 570 59 574 59 578 60	497 612 501 616 506 620	578 600 514 580 604 518 585 608 522 589 612 526	615 619 624	473 423 476 427 480 430	462 377 466 381 469 385 463 388
161 162 163	583 60 587 61 591 61	513 629 517 633 521 637	593 617 530 597 621 534 601 625 538	632 636 640	488 438 491 442 495 445	467 392 471 395 474 369
164 185 186 167	595 61 599 62 603 62 607 63	529 645 533 650 536 654	605 620 542 609 633 545 613 637 550 618 642 554	649 653 658	502 453 508 457 510 460	478 402 482 406 486 409 489 413
168 169 170 171	611 63 615 64 619 64 624 64	544 662 548 666	622 646 557 628 650 561 630 654 565 634 658 569	666 670	517 467 521 472	493 417 497 420 501 424 504 427
172 173 174 175	628 63 632 65 636 68 640 68	5 558 675 560 679 564 683	638 662 573 642 666 577 643 671 581 650 675 585	679 683 687	529 479 532 482 538 486	508 431 512 434 516 438 519 441
176 177 178	644 66 648 67 652 67	571 691 575 695 579 700	654 679 559 658 683 593 662 687 596	695 699 704	543 493 547 497 551 501	523 446 527 448 530 452
179 180 181 182	656 68 660 68 664 69 668 69	590 712	666 691 600 670 695 604 674 699 608 678 703 612	712 716	558 508 562 512	534 455 538 459 542 463 545 466
183 184 185 186	672 69 876 70 680 70 684 71	597 720 801 724 805 728	682 707 616 688 711 619 690 715 623	724 728 732	569 519 573 523 577 527	549 470 553 473 556 477 560 480
187 188 189	688 71 692 71 696 72	613 798 617 740 621 744	698 723 631 702 727 635 706 731 639	740 744 748	584 534 588 538 592 541	564 484 567 487 571 491
190 191	699 72 703 73	624 748 628 752	710 736 642 714 739 646	752 756		575 494 579 498
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				21 August 2008
Time (min)	CCAve TC#9	P11 P11 P11 Sec C-C Sec C-C TC #10 TC #11 DDAve (*F) (*F)	P11 P11 P11 Sec D-D Sec D-D Sec D-D TC W12 TC W13 TC W14 (*F) (*F) (*F)	P14 P14 P14 P14 Sec A.A. Sec A.A. P14 Max. AAAva T.C. #1 T.C.#2 ("F) ("F)
1923 1941 1955 1996 1997 1997 1998 2000 2007 2006 2007 2010 2111 2113 213 214 215 217 217 218 219 219 220 220 220 220 221 221 221 221 221 221	711 738 742 719 746 757 750 757 750 757 750 757 750 750 750	632 756 718 636 760 722 640 764 738 640 764 738 640 768 729 647 772 733 655 760 741 655 780 741 656 780 788 660 788 788 660 788 788 660 788 788 660 788 788 660 788 788 660 788 788 660 788 788 678 680 788 678 680 788 678 680 788 681 788 682 688 888 683 682 689 816 779 683 682 689 816 779 704 831 779 704 831 782 708 831 701 852 788 687 704 831 701 853 883 701 853 883 701 855 788 701 857 708 851 811 707 708 655 788 708 708 851 709 858 709 868 709 868 709 878 709 889 709 887 709 889 709 889 709 887 709 889 709 887 709 889 709 887 709 889 709 887 709 889 709 887 709 889 709 887 70	743 650 760 747 654 764 751 654 764 751 654 768 759 601 772 759 855 778 759 855 778 750 699 780 770 877 788 7774 881 779 881 770 881 770 882 882 881 780 881 780 881 780 881 780 881 780 881 780 881 780 881 780 881 780 881 882 881 882 881 882 881 882 881 882 881 882 881 882 881 882 881 882 881 882 881 882 881 882 881 780 882 883 883 883 883 883 883 883 883 883 883 883 883 883 883 883	602 552 582 502 606 656 588 505 610 659 699 508 613 563 590 512 617 567 597 515 621 574 601 519 624 574 604 522 632 889 611 523 632 889 615 383 633 839 616 383 640 592 543 641 592 543 644 592 544 644 592 547 654 603 559 657 607 637 564 651 610 641 557 664 614 644 560 686 617 648 564 672 621 651 567 682 632 662 578 </td
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Aspen Aerog	gels, Inc.		28 August, 2008
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Time (min)	P14 P14 P14 Sec A-A sc A-A Sec A-A ne TC #3 TC #4 TC #5 n) (°F) (°F) (°F)	P14 P14 P14 P14 Sec B-B Sec B-B Sec B-B 3BAve TC#6 TC#7 TC#8 (*F) (*F) (*F)	
	0 82 82 82 1 82 82 82 2 82 82 82 3 82 82 82	82 82 82 badño 82 82 82 badño 82 82 82 badño 83 82 83 badño	
4 5	4 83 82 82 5 83 82 82 6 82 82 82 7 81 82 82	83 82 83 bedito 83 82 83 bedito 83 82 83 bedito 82 81 82 bedito 82 81 82 bedito	
\$ \$	8 81 82 82 9 81 82 82 10 81 82 82	82 81 82 badño 82 81 82 badño 82 81 82 badño	
11 12 12 14	14 80 82 82	82 81 82 badño 82 81 82 badño 82 81 82 badño 82 81 82 badño 82 81 82 badño	
14 16 16 17 18	18 80 82 82	82 81 82 badño 82 81 83 badño 82 81 83 badño 82 81 83 badño	
15 20 21 22	20 81 82 82 21 81 82 83 22 82 83 83	82 81 83 badño 83 82 83 badño 83 82 83 badño 83 82 83 badño	
22 24 25 26	23 82 83 83 24 82 83 83 25 83 84 84 26 84 84 84	83 83 83 badfe 84 83 84 badfe 84 badfe 85 85 84 badfe	
27 28 25	27 85 85 84 28 85 85 85 29 86 88 85	85 85 84 badhc 85 86 84 badhc 86 86 85 badhc 86 87 85 badhc	
36 35 35 34 36 36 36	31 87 87 86 32 88 87 87 33 89 88 87	87 88 85 badño 87 89 85 badño 88 89 86 badño 88 89 86 badño	
36 36 37 38	MS 93 91 90	89 91 96 badño 90 92 87 badño 90 92 87 badño 90 93 87 badño	
35 40	39 94 52 91 40 95 92 92 41 95 93 93	91 94 88 badho 92 95 88 badho 92 95 89 badho 93 96 89 badho	
43 43 44 45	15 99 96 95	94 97 90 badho 94 98 90 badho 95 99 91 badho 95 99 91 badho	
46 47 48 45	48 102 99 98 49 103 100 99	96 100 92 badño 97 101 92 badño 98 102 93 badño	
50 55 55 55	53 108 104 103	98 103 93 badño 99 104 94 badño 100 105 95 badño 101 107 95 badño	
54 55 55 57	57 113 108 107	102 108 96 badño 103 109 97 badño 105 111 98 badño 106 113 98 badño	
	59 116 111 110 50 118 112 112 51 119 113 113	107 114 99 badño 108 116 100 badño 110 118 101 badño 111 120 102 badño	
	82 121 115 115 53 123 117 117	113 122 103 badño 114 124 104 badño	
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Aspen Aeroge Project No. 3		28 August, 2008 Page 67 of 95
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Time	P14 P14 P14 P14 P14 P14 P14 P14 Sec A-A to A-A Sec A-A TC	
(min) 128 129	(°F) (°F) (°F) (°F) (°F) (°F) (°F) (°F)	
130 131 132 133	348 318 315 308 339 277 badho 352 321 319 312 343 280 badho 358 325 322 315 346 284 badho 360 329 325 319 350 287 badho	
133 134 135 136	304 332 329 322 353 290 badho 308 338 333 325 357 293 badho 372 339 338 328 360 296 badho	
137 138 139 140	376 343 340 332 364 300 baddte 380 347 349 336 368 303 baddte 384 351 346 339 371 306 baddte 388 354 350 343 375 310 baddte 302 368 364 346 379 313 baddte	
141 142 143 144	392 358 354 346 379 313 badño 396 362 357 350 362 317 badño 400 368 361 363 386 320 badño 404 370 384 357 380 323 badño	
145 146 147	408 373 368 360 393 326 badfic 412 377 372 364 397 330 badfic 416 381 375 367 400 333 badfic	
148 149 150 151	420 385 379 370 404 336 badfic 424 388 382 374 407 340 badfic 428 392 386 377 411 343 badfic 432 396 390 381 415 346 badfic	
152 153 154	436 400 393 384 418 350 bad/fic 440 404 397 388 422 353 bad/fic 444 407 400 391 425 356 bad/fic	
155 156 157 158	448 411 404 395 429 380 badfic 452 415 407 398 433 383 badfic 455 419 411 402 436 387 badfic 459 422 415 405 440 370 badfic	
159 160 161 162	463 428 418 408 443 373 badha 407 430 422 412 447 377 badha 471 434 428 415 450 380 badha 475 438 429 419 454 383 badha	
163 164 185	479 441 433 422 457 397 badha 483 445 436 426 461 390 badha 487 449 440 429 465 393 badha	
186 167 188 189	491 453 444 433 468 397 badño 495 457 447 436 472 400 badño 490 480 451 439 476 403 badño 500 464 454 443 479 407 badño	
170 171 172 173	507 468 458 446 482 410 badño 510 472 462 450 486 414 badño 514 475 465 484 490 417 badño 518 479 469 457 403 420 badño	
174 175 176	522 483 472 461 497 424 badfic 526 487 476 464 500 427 badfic 530 490 479 467 503 430 badfic	
177 178 179 180	534 494 483 471 507 434 bedfic 537 496 487 474 511 437 bedfic 541 501 490 477 514 440 bedfic 545 505 494 481 518 444 bedfic	
181 182 183	540 500 498 484 521 447 bedfic 553 513 501 488 525 451 bedfic 557 516 505 491 528 454 bedfic	
184 185 186 187	580 520 508 495 532 457 badfic 564 524 512 498 535 461 badfic 588 528 516 502 539 464 badfic 572 532 519 505 542 467 badfic	
188 189 190	576 535 523 509 546 471 bedfic 580 539 526 512 549 474 bedfic 583 542 530 515 563 477 bedfic	
191	587 546 534 519 556 481 bad/tc	
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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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	Photographs	
		Intertal
		Intertek





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Appendix F UL 1709 - RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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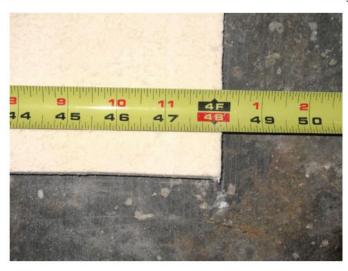
Intertek





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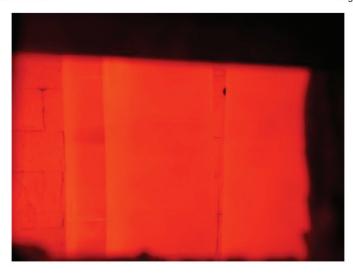




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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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Appendix F UL 1709 – RAPID RISE FIRE TESTS OF PROTECTION MATERIALS FOR STRUCTURAL STEEL

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REVISION SUMMARY

DATE	SUMMARY
<insert date="" of="" revision=""></insert>	<insert of="" revision="" summary=""></insert>

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Appendix G ASTM C 411/C 447 – HOT SURFACE PERFORMANCE

TUTCO SCIENTIFIC CORPORATION

714 East Aspen Ave. Fruita CO 81521

p&f 970 858 3584; e-mail: tutco@bresnan.net

REPORT ON

96 HOUR

HOT SURFACE PERFORMANCE

DETERMINED USING ASTM C411 AND C447

AT 1200 °F (650 °C)

FOR

ASPEN AEROGELS

PYROGEL XT

(SAMPLE ID - ENG921)

PREPARED FOR

ASPEN AEROGELS 30 FORBES RD BLDG B NORTHBOROUGH, MA 01532

TUTCO SCIENTIFIC REPORT NO. AERO\411&447(306138).308 March 10, 2008

Reported by_

Kenneth Whorlow

President



TECHNICAL GUIDE

Appendix G ASTM C 411/C 447 – HOT SURFACE PERFORMANCE

AERO\411&447(306138).308 PAGE 2

<u>Project:</u> Determine the hot surface performance and the interior temperature rise of one sample of Flexible Insulation Blanket received from Aspen Aerogels. The testing was conducted by request of Cindy MacLaurin by letter for purchase order 306138.

Samples: The sample was identified as Pyrogel XT, Sample ID ENG921

Test Method: ASTM C 411 (Hot Surface Performance of High-Temperature Thermal Insulation - Pipe Insulation Method) continuing the test for 4 days as required by C 411. The test was conducted at 1200 °F (650 °C) hot surface temperature. In addition, during the heat up, the interior temperature rise at layers 2, 4, 6, 8, and 10 were recorded in accord with C447 section 8.1.6. Shrinkage across the 36" length and around the first and part of the second wrap was determined as described in the procedure section.

Procedure: The temperature was targeted to be 1200 °F (650 °C) and the temperature of the hot pipe surface was within +/- 25 °F as required by ASTM C411. The material was installed on the pipe as a continuous 11 ply installation with 4 inches overlapping the outside seam. Sheathed thermocouples were placed between layers 2-3, 4-5, 6-7, 8-9, 10-11. The data was recorded by a data logger 4 times a minute during the heating of the pipe (approximately 400 minutes). An aluminum jacket was installed over the insulation. The hot surface temperature of the pipe was controlled to a maximum of 1200 °F (650 °C) and monitored with thermocouples on the surface of the hot pipe and guards. The test was continued for 96 hours at the 1200 °F (650 °C) hot surface temperature.

The leading edge of the insulation material was started on the pipe using wire. A 0.06 inch wire was wrapped around the pipe and twisted tight. One lead was clipped and the other formed into a small hook. The wires were used in the center and 2 inches from each end. The leading edge of the material was pushed onto the hook, and then the wire hook was tapped flat. The insulation material was then wrapped around the affixed leading edge. The 11 layers of material were wrapped tight and were held in place on the pipe using fiberglass reinforced tape wrapped around the outer layer of insulation. The tape was positioned approximately 2 inches from each end and at 10 inch intervals. The aluminum jacket was installed on the test pipe using wire at the center and 6 inches in from each end. The circumference of the insulation was 30.75 inches and the circumference with the aluminum jacket installed was 31 inches.

Shrinkage across the 36" length of the leading edge and 10 cm back from the leading edge was measured. Circumferential shrinkage around the first wrap and part of the second wrap were determined at 10 cm intervals. The shrinkage was determined by imbedding small staples along the edges and up the center of the blanket. The distance between the staples was measured to 0.1 cm accuracy using a tape measure before and after exposure. The percentage changes for the measurements are provided.

Observations and Results: After 4-days exposure at 1200 °F (650 °C)

Figure 1 is a graph of the thermocouple temperatures at the layers and cold surface during heatup and continuing for the first 400 minutes of the test. None of the layers indicated an exothermic heat rise.

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Appendix G ASTM C 411/C 447 – HOT SURFACE PERFORMANCE

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Observations and Results: (continued)

There were no observed changes of the installed material during the test or at the conclusion of the 96 hour heating period. After the test equipment had cooled, the material was removed from the pipe and remained intact.

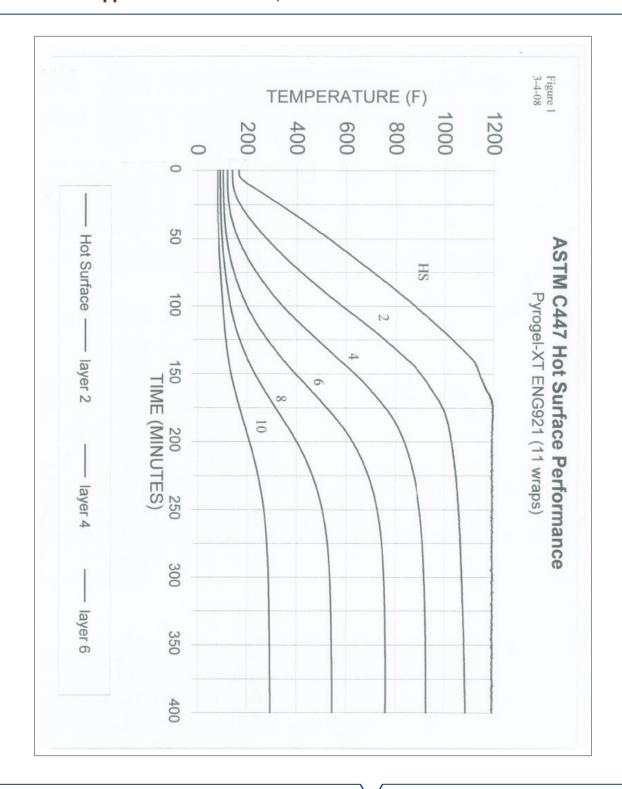
- 1. Visual examination during the test period was limited because of the exterior metal jacket.
- 2. There was no apparent flaming, glowing, smoldering, or smoking at any time during the test that could be seen at the exposed ends of the jacketed material.
- 3. There was some odor during the heating.
- 4. None of the layers indicated an exothermic heat rise.
- 5. Visual examination of the exterior of the installed material at the conclusion of the test, after the pipe had cooled and the jacket was removed, showed no apparent sagging, surface cracking, warpage, de-lamination or shrinkage.
- 6. After disassembly, all layers of the 11 ply pipe insulation showed no apparent sagging, surface cracking, warpage, de-lamination or shrinkage. The material remained flexible.
- 7. The was no evidence of flaming, glowing, smoldering, or smoking on the inner layers.

Results of the Shrinkage Measurements during C411 Hot Surface Performance test

- 1. Across the 36 inch length of the leading edge the percentage shrinkage was 0.9%.
- 2. Across the 36 inch length approximately $10\ \mathrm{cm}$ back from the leading edge the percentage shrinkage was 0.8%.
- 3. The circumferential shrinkage was measured along both sides and in the center of the blanket, along the leading edge and at approximately 10 cm positions back from the leading edge. The average percentage shrinkage at the leading edge was 1.77%. The average percentage shrinkage at the next four positions were: 1.65%, 2.66%, 2.02%, 2.65%
- 4. The measured circumferential shrinkage around the sample was greater than across the width. This is probably due to the added condition of permanent wrinkles caused by compression of the measured surface of the blanket as it is wrapped around the pipe. The wrinkles are not an indication of shrinkage of the blanket fibers.



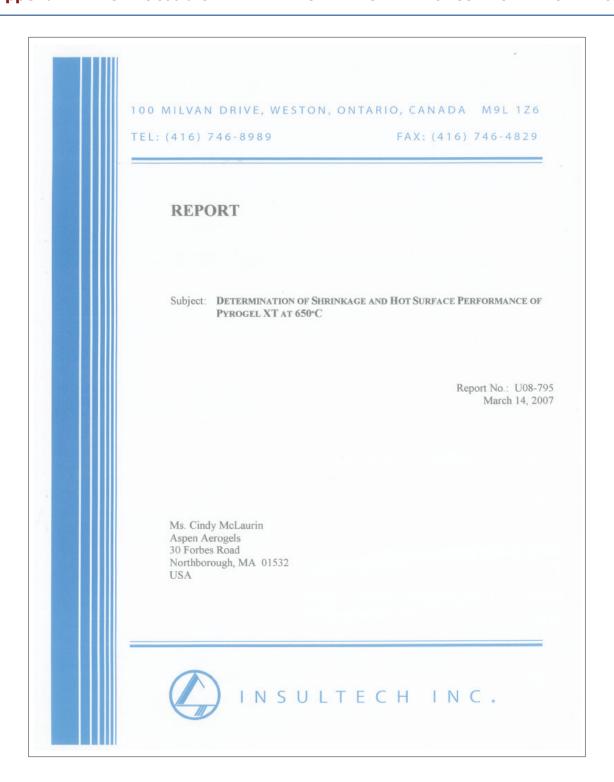
Appendix G ASTM C 411/C 447 – HOT SURFACE PERFORMANCE







Appendix H ASTM C 356 & C 411 – LINEAR SHRINKAGE AND HOT SURFACE PERFORMANCE





TECHNICAL GUIDE

Appendix H ASTM C 356 & C 411 – LINEAR SHRINKAGE AND HOT SURFACE PERFORMANCE

		*
		INSULTECH INC.
	TEST REPORT	
8		
	Firm: Aspen Aerogel 30 Forbes Road	Report No.: U08-795
	Northborough, MA 0153 USA	Date: March 14, 2007 Ref. No.: 27.48
		No. 100. 27.70
		Page: 1 of 4
	1 1/4	2////
	Tested: Approved:	Outle
	Robert Hall	Leslie K. Truksa, Ph.D.
	Material: One sample of Pyrogel XT	
*		
	Tests Requested: Shrinkage C356 and hot surface performance C411	on 12 layer stack at 650°C.

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Appendix H ASTM C 356 & C 411 – LINEAR SHRINKAGE AND HOT SURFACE PERFORMANCE





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Appendix H ASTM C 356 & C 411 – LINEAR SHRINKAGE AND HOT SURFACE PERFORMANCE







Appendix H ASTM C 356 & C 411 – LINEAR SHRINKAGE AND HOT SURFACE PERFORMANCE

aspen aerogels™

		Pyrogel	IXT: C356, C411 @ 650		INSULT
					Page 4 of
Aspen A	Aerogels.		TR: U08-795		March 14, 20
4.0	RESULT	rs			
410	TUDOUZ.				
	.1 Linear sh	rinkage			
	.1 Linear Si	ittikage	χ	(n=4	σ/υ
	Mass loss of	n drving. %	0.26	,	0.087/32.97
	Mass loss or		1.05		0.185/17.61
	Shrinkage, 9	%	1.28		0.307.24.00
	Visual obse	rvations: No s	significant change from	the original.	
	All speci integrity.	mens appea	ination or change of	d retained g	ood structural
	_		n temperature was		
			emperature recordent ation of glowing, sr		
	flaming.	is no mulca	mon or growing, si	noking, sm	outdering of
		a no oridor	nce of sustained ex	othorm	



TECHNICAL GUIDE

Appendix I MECHANICAL RESILIENCE AND WATER RESISTANCE



TESTING GROUP

www.bodycote.com www.bodycotetesting.com

EVALUATION OF THE PHYSICAL PROPERTIES OF PYROGEL XT BLANKET THERMAL INSULATION

Report to:

Aspen Aerogels Inc. 30 Forbes Road

Northborough, MA

01532

Attention:

Cindy MacLaurin

Telephone:

508-691-1132

Fax:

508-691-1114

E-mail:

cmaclaurin@aerogel.com

Report No.:

08-06-M0061

5 Pages

Proposal No.:

08-006-0200

Date:

April 28, 2008

Bodycote Testing Group 2395 Speakman Drive • Mississauga • Ontario • Canada • L5K 1B3 • Tel: +1 (905) 822-4111 • Fax: +1 (905) 823-1446



TECHNICAL GUIDE

Appendix I MECHANICAL RESILIENCE AND WATER RESISTANCE

Bodycote Testing Group

Evaluation of Physical Properties of Pyrogel XT for Aspen Aerogels Inc.

Page 2 of 5 Report No. 08-06-M0061

1.0 INTRODUCTION

At the request of Aspen Aerogels Inc., Bodycote Testing Group was retained to evaluate several physical properties of a sample of thermal insulation material.

Upon receipt, the sample was assigned the following Bodycote Sample No.

Client Sample Description	Bodycote Sample No.
PYROGEL XT	08-06-M0061

2.0 PROCEDURE

The sample was evaluated according to the following standard test methods:

Test Description	Test Method
Standard Test Method for Determining the Water Vapor Sorption of Unfaced Mineral Fibre Insulation	ASTM C 1104 - 00
Standard Test Method for Determining the Water Retention (Repellency) Characterisitics of Glass Fibre Insulation	ASTM C 1511 - 04
Standard Test Method for Measuring Compressive Properties of Thermal Insulation	ASTM C 165 - 07
Standard Test Method for Determining Wicking of Glass Fibre Blanket Insulation	ASTM C 1559
Standard Test Method for Breaking Strength and Elongation of Textile Fabrics (Grab Test)	ASTM D 5034 -95(2001)





Appendix I MECHANICAL RESILIENCE AND WATER RESISTANCE

3.0 RESULTS

A summary of all data is provided in table 1. Detailed results are provided in tables 2 through 6.

Table 1 – Summary of Results Bodycote Sample No. 08-06-M0061				
Description	Result			
Water Vapor Sorption (ASTM C 1104) Mass Gain, %	2.25			
Water Retention (Repellency) (ASTM C 1511) Water Repellency, g Mass Gain, % Volume of Water, %	16.3 16.4 4.2			
Compressive Properties (ASTM C 165) 5 layers, 30.2mm thickness Compressive Stress @ 10% Compression, kPa Compressive Stress @ 25% Compression, kPa	103.1 217.4			
Wicking (ASTM C 1559) As Received; 20 ^o C; 168 hours, mm As Received; 50 ^o C; 168 hours, mm 336 hr Aged; 20 ^o C; 168 hours, mm 336 hr Aged; 50 ^o C; 168 hours, mm Leached; 20 ^o C; 168 hours, mm Leached; 50 ^o C; 168 hours, mm	0 0 0 2 0 1			
Grab Test (ASTM D 5034) Maximum Load, Machine Direction, N Maximum Load, Cross Direction, N	490 370			

Table 2 – Water Vapor Sorption (ASTM C 1104) Bodycote Sample No. 08-06-M0061				
Specimen	Initial Mass, g	Final Mass, g		
1	24.73	25.28		
2	24.07	24.65		
3	25.07	25.60		
Average	24.62	25.18		
	Mass Gain:	2.25%		



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Appendix I MECHANICAL RESILIENCE AND WATER RESISTANCE

Table 3 – Water Retention (ASTM C 1511) Bodycote Sample No. 08-06-M0061				
Specimen	Initial Mass, g	Final Mass, g		
1	101.43	118.70		
2 100.08		114.34		
3	96.83	114.32		
Average 99.44		115.78		
	Water Repellency:	16.3 g		
	Mass Gain:	16.4 %		
	Volume of Water:	4.2 %		

	Table 4 – Compressive Strength Bodycote Sample No. 08-0	
Specimen	Stress at 10% Compression, kPa	Stress at 25% Compression, kPa
1	103.1	214.4
2	108.1	217.4
3	112.7	172.1
Average	108.0	201.3

			icking (ASTM mple No. 08-0			
	Max Hei	ight, mm	Max He	ight, mm	Max He	ight, mm
Duration, hrs	As Re	ceived 50°C	Heat 20°C	Aged 50°C	Lead 20°C	ched 50°C
24	0	0	0	1	0	0
48	0	0	0	1	0	0
72	0	0	0	1	0	1
96	0	0	0	1	0	1
168	0	0	0	2	0	1



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Appendix I MECHANICAL RESILIENCE AND WATER RESISTANCE

Bodycote Testing Group	
Evaluation of Physical Properties of Pyrogel XT for Aspen Aerogels Inc.	Page 5 of 5 Report No. 08-06-M0061

Table 6 – Grab Test (ASTM D 5034) Bodycote Sample No. 08-06-M0061				
Specimen	Maximum Load	Maximum Load		
	Machine Direction, N	Cross Direction, N		
1	420	340		
2	340	380		
3	550	400		
4	530	390		
5	610	330		
Average	490	370		

Reported by:

Reviewed by:

David Beauchamp, B.Sc., Ext. 228 Scientist, Building Performance Centre

Product Testing Group

Franz C. Bauer, Ext. 403

Manager, Building Performance Centre

Product Testing Group

REGISTRATION

ISO 9001:2000 registered by QMI, Registration #001109

This report refers only to the particular samples, units, material, instrument, or other subject used and referred to in it, and is limited by the tests and/or analyses performed. Similar articles may not be of like quality, and other testing and/or analysis programs might be desirable and might give different results.

Please note that unless otherwise notified by the Client, the sample(s) will be disposed of 30 days following issue of the final report. The Client is responsible for any costs associated with returning the sample.



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Appendix J ASTM C 795 – CORROSION TEST

10-29-2008 22:53 KENNETH WHORLOW

PAGE2

TUTCO SCIENTIFIC CORPORATION 714 East Aspen Ave Fruita, CO 81521

phone and Fax 970-858-3584 email: tutco@bresnan.net

28-DAY CORROSION TEST

AND CHEMICAL TESTS OF

PYROGEL XT BLKT 1205

(SAMPLE ID 08090168)

IN ACCORD WITH

ASTM C795

USING THE TEST METHODS OF

ASTM C 692 AND ASTM C 871

PREPARED FOR ASPEN AEROGELS 30 FORBES RD BLDG B NORTHBOROUGH, MA 01532

TUTCO SCIENTIFIC REPORT NO. AERO\692(307922).008 October 29, 2008

Reported by_

Kenneth Whorlow President



TECHNICAL GUIDE

Appendix J ASTM C 795 – CORROSION TEST

10-29-2008 22:53 KENNETH WHORLOW

PAGE3

AERO\692(307922).O08 Page 2

<u>Subject</u>: This report covers ASTM C871 Chemical Tests (Standard Test Method for Chemical Analysis of Thermal Insulation Materials for Leachable Chloride, Fluoride, Silicate, and Sodium Ions) and ASTM C 692 28-Day (Pre-Production) Corrosion Tests (Standard Test Method for Evaluating the Influence of Thermal Insulations on the External Stress Corrosion Cracking Tendency of Stainless Austeritic Steel). The material tested was Pyrogel XT Blkt 1205, Sample ID 08090168 received from Aspen Aerogels on PO # 307922, dated 23-Sep-08.

The results may be used to determine the qualification of the insulation to the requirements of ASTM C 795 (Standard Specification for Thermal Insulation for Use in Contact with Austenitic Stainless Steel).

Samples: The samples were identified as #1 Name: Pyrogel XT Blkt 1205, Sample ID, 8090168

CHEMICAL TESTS

Sample Preparation: Samples were cut from the submitted specimen such that the test samples were representative of the entire cross section of the material. Samples weighing 20.0 grams were prepared for the duplicate extractions.

Each weighed sample was put in a blender jar containing 500 ml of demineralized water, ground and crushed into small pieces and quantitatively transferred to a one-liter stainless steel beaker. The sample slurry was heated to boiling and maintained at temperature for 30 minutes. The liquid was cooled, the weight was brought to 500 grams, and then strained and then filtered to produce the extraction solution for chemical tests.

<u>Chemical Test Procedures</u>: All test procedures were conducted in accord with ASTM C871. The tests used were as follows: Chloride - Amperometric-coulometric titrator; Silicate - Molydisilicic acid; Sodium - Ion Selective Electrode; Fluoride - Ion Selective Electrode; pH - Standard pH probe and meter.

Test Results: Given in parts per million (mg/kg).

Sample	Sodium	Silicate	Chloride	Fluoride	pH
1A	41	7349	33	9	8.8
1B	40	7230	32	9	8.8

<u>Chemical Test Conclusions:</u> The sample identified as Pyrogel XT Blkt 1205, Sample ID 08090168 met the chemical requirements of ASTM C 795, falling within the "acceptable" range of the "acceptability curve".



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Appendix J ASTM C 795 – CORROSION TEST

10-29-2008 22:54 KENNETH WHORLOW

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AERO\692(307922).008 Page 3

28-DAY CORROSION TEST

Corrosion Test Procedures: The 28-Day Corrosion Test was run in accord with ASTM C692, using the Drip Test Procedure. The metal used to fabricate the test coupons had a 0.051 carbon content. The coupons were sensitized by heating at 1200°F in an air atmosphere for 3 hours. They were then prepared in accord with ASTM C692. The lot of sensitized steel was qualified by three-day exposure to a 1500 ppm chloride solution - all specimens cracked, and 28-day exposure to de-ionized water none cracked.

Sample Preparation: Test samples were fabricated from the blanket insulation to form approximately 1.5" thick, 4" wide, 3.5" tall sections using 4 layers of the material held together with rubber bands. Four specimens were prepared and each fitted with a u-bend coupon. The test coupons and specimens were set up on the C692 drip test apparatus, which was brought to operating temperature and the flow of de-ionized water from the peristaltic pump was started. The material is hydrophobic and does not readily wet, therefore 1/4 inch channels were cut in the center pieces of the insulation. Water dripped into the channel percolated down to the coupon surface. The flow rate was set at 250 ml/day on each test specimen.

After 28-days the coupons and contact area of the materials were examined and the materials were wet at the contact surface of the coupons. All of samples was slightly adhered to the coupons in small spots.

Corrosion Test Results: At the conclusion of 28-days from the start of the test the coupons were removed, flattened, cleaned, re-bent, and inspected. No obvious cracks were found. The required inspection using dye penetrant and developer was done to add greater confidence that all cracks are found. No cracks were found on any of the coupons. The coupons were determined to be free of cracks.

of Coupons tested

of Coupons Cracked

0

Corrosion Test Conclusion:

The sample identified as Pyrogel XT Blkt 1205, Sample ID 08090168, produced none of the four coupons tested having any cracks.



TECHNICAL GUIDE

Appendix K ASTM C 592-04 – HEAT AND VIBRATION AGING



TESTING GROUP

www.bodycote.com www.bodycotetesting.com

EVALUATION OF THE EFFECT OF HEAT AND VIBRATION AGING OF PYROGEL XT AND MINERAL WOOL THERMAL INSULATION MATERIAL

Report to:

Aspen Aerogels Inc. 30 Forbes Road

Northborough, MA

01532

Attention:

Cindy MacLaurin

Telephone: Fax: E-mail: 508-691-1132 508-691-1114

cmaclaurin@aerogel.com

Report No .:

08-06-M0171, Revision 2

3 Pages

Proposal No.:

08-006-5335

Date:

December 8, 2008

Bodycote Testing Group - Americas - Head Office 2395 Speakman Drive • Mississauga • Ontario • Canada • L5K 1B3 • Tel: +1 (905) 822-4111 • Fax: +1 (905) 823-1446



TECHNICAL GUIDE

Appendix K ASTM C 592-04 – HEAT AND VIBRATION AGING

1.0 INTRODUCTION

At the request of Aspen Aerogels Inc., Bodycote Testing Group was retained to evaluate the mass and physical appearance effects of heat and vibration aging of two samples of thermal insulation material.

Upon receipt, the sample was assigned the following Bodycote Sample No.:

Client Sample Description	Bodycote Sample No.	
Pyrogel XT	08-06-M0171 - A	
Mineral Wool	08-06-M0171 - B	

2.0 PROCEDURE

The sample was evaluated according to the following standard test methods:

Test Description	Test Method
Standard Specification for Mineral Fibre Blanket Insulation and Blanket-Type Pipe Insulation (Metal-Mesh Covered) (Industrial Type) - Resistance to Vibration	ASTM C 592 – 04 Section 11.11 Modified

ASTM C 592 Section 11.11 Resistance to Vibration - Modified

Testing to this method was conducted in accordance with section 11.11 of ASTM C 592. The following testing specifics apply, and where appropriate are deviations from the method.

Each sample was initially weighed at ambient laboratory conditions (nominally 23°C and 60% relative humidity). The weights were recorded to an accuracy of 0.1 grams. Immediately after weighing, the sample was heated on a hot plate apparatus to 400°C for greater than 96 hours with a temperature gradient through the sample from 400°C at the hot plate surface to ambient laboratory conditions on the opposite face. After at least 96 hours had elapsed the samples were removed from the hot plate, allowed to cool to room temperature and weighed.

The sample was then transferred to the vibration fixture, comprised of 6 equally spaced rods on which the sample was impaled. The sample was held horizontally on the vibration table for 6 hours, being vibrated at a frequency of 12 Hz, with a displacement of 3 mm (peak to peak). Vibration was conducted in an ambient lab environment. The sample was then carefully removed from the table and a final weight taken.



TECHNICAL GUIDE

Appendix K ASTM C 592-04 – HEAT AND VIBRATION AGING

Bodycote Testing Group		_
Evaluation of the Effect of Heat and Vibration Aging on		~
for Aspen Aerogels Inc.	Report No. 08-06-M0171, Revisio	n 2

RESULTS

ASTM C 5	Aging of Thermal Insulating Material 592 §11.11 Modified . 08-06-M0171-A (Pyrogel XT)
Change in Mass after Vibration (heat aged sample)	Observations
- 0.19 %	Blackening around edges of sample on mid thickness plies.

Initial mass of specimen	3523.0 g
Specimen mass after 96 hrs at 400°C	3449.6 g
Specimen mass after 96 hrs at 400°C and 6 hours vibration	3442.9 g

ASTM C 592	Table 2 – Heat & Vibration Aging of Thermal Insulating Material ASTM C 592 §11.11 Modified Bodycote Sample No. 08-06-M0171-B (Mineral Wool)	
Change in Mass after Vibration (heat aged sample)	Observations	

Change in Mass after Vibration (heat aged sample)	Observations
- 0.51 %	No change observed.

Initial mass of specimen	3211.0 g
Specimen mass after 96 hrs at 400°C	3215.4 g
Specimen mass after 96 hrs at 400°C and 6 hours vibration	3199.0 g

Reported by:

Reviewed by:

David Beauchamp, B.Sc., Ext. 228 Scientist, Building Performance Centre

Product Testing Group

Franz C. Bauer, Ext. 403

Manager, Building Performance Centre

Product Testing Group

This report refers only to the particular samples, units, material, instrument, or other subject used and referred to in it, and is limited by the tests and/or analyses performed. Similar articles may not be of like quality, and other testing and/or analysis programs might be desirable and might give different results.





Appendix L BS EN 13501-1:2007 – REACTION TO FIRE PERFORMANCE





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Appendix L BS EN 13501-1:2007 – REACTION TO FIRE PERFORMANCE

WF Classification Report No. 180079 Issue 2

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1. Introduction

This classification report defines the classification assigned to "Pyrogel XT", a batting insulation, in line with the procedures given in EN 13501-1:2007

2. Details of classified product

2.1 General

The product, "Pyrogel XT", a batting insulation, is deemed as being suitable for construction applications, excluding flooring and linear pipe thermal insulation in building and construction.

2.2 Product description

The product, "Pyrogel XT", a batting insulation, is fully described below and in the test reports provided in support of classification listed in Clause 3.1.

General description		A batting insulation mounted onto a calcium silicate based substrate utilising screws		
Product reference		"Pyrogel XT"		
	Detailed description / composition details	Silica based aerogel insulation batting		
	Name of manufacturer	Aspen Aerogels, Inc.		
	Density	0.18 g/cm³ (stated by sponsor) 0.19 g/cm³ (Determined by Bodycote warringtonfire)		
Batting	Weight per unit area	896g/m ² (Determined by Bodycote warringtonfire)		
	Thickness	5-10mm (stated by sponsor) 4.73 - 9.86mm (determined by Bodycote warringtonfire)		
	Colour	Beige		
	Flame retardant details	See Note 1		
	Product reference	"Promat – Brandschultzbauplatten; Promatect-H"		
	Generic type	Calcium Silicate based board		
	Name of manufacturer	Promat		
Substrate	Thickness	12mm		
1	Density	870kg/m³		
	Flame retardant details	The substrate is inherently flame retardant		
Mounting and fixing details		The specimen was mechanically fixed to the calcium silicate substrate utilising 16mm long screws. The screws were located around the perimeter of each wall and were positioned in the corners and at approximately 350mm intervals.		
Brief description of manufacturing process		Aspen Aerogels produces naroporous insulating materials, the process involves casting of the aerogels into fibrous battings.		

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Note 1 - The sponsor of the test has provided this information but at the specific request of the sponsor, these details have been omitted from the report and are instead held on the confidential file relating to this investigation.

Test reports/extended application reports & test results in support of classification

3.1 Test reports/extended application reports

Name of Laboratory	Name of sponsor	Test reports/extended application report Nos.	Test method / extended application rules & date
Bodycote warringtonfire	Aspen Aerogels Inc	WF 178244 WF 178245	EN 13823
Bodycote warringtonfire	Aspen Aerogels Inc	WF 178243	EN ISO 1716

3.2 Test results

			Results	
Test method & test number	Parameter	No. tests	Continuous parameter - mean (m)	Compliance
EN 13823	FIGRA 0.2MJ	4	0	Compliant
	THR _{600s}		0.49, 0.56, 0.13, 0.37	Compliant
	LSF		No	Compliant
	SMOGRA		0, 0, 0, 0	Compliant
	TSP _{60Cs}		42, 36, 36, 34	Compliant
EN ISO 1716	PCS ≤ 2,0 MJ/kg (1) PCS ≤ 2,0 MJ/ kg (2)(2a) PCS ≤ 1,4 MJ/m² (3) PCS ≤ 2,0 MJ/kg (4)			
	Total	3	2.1 MJ/kg	Compliant

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WF Classification Report No. 180079 Issue 2

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4. Classification and field of application

4.1 Reference of classification

This classification has been carried out in accordance with clause 8 of EN 13501-1:2007

4.2 Classification

The product, "Pyrogel XT", a batting insulation, in relation to its reaction to fire behaviour is classified:

Reaction to fire classification: A2-s1,d0

4.3 Field of application

This classification is valid for the following end use applications:

- Construction applications, excluding flooring and linear pipe thermal insulation in building and construction.
- ii) As a suspended ceiling membrane.

This classification is also valid for the following product parameters:

Product thickness 5-10mm

Product density
Product colour
Product composition
Product construction
No variation allowed
Product construction
No variation allowed

The classification is valid for the following substrates and airgaps:

Directly against an A1 or A2 substrate with a density of 615 kg/m³ and greater

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TECHNICAL GUIDE

Appendix L BS EN 13501-1:2007 – REACTION TO FIRE PERFORMANCE

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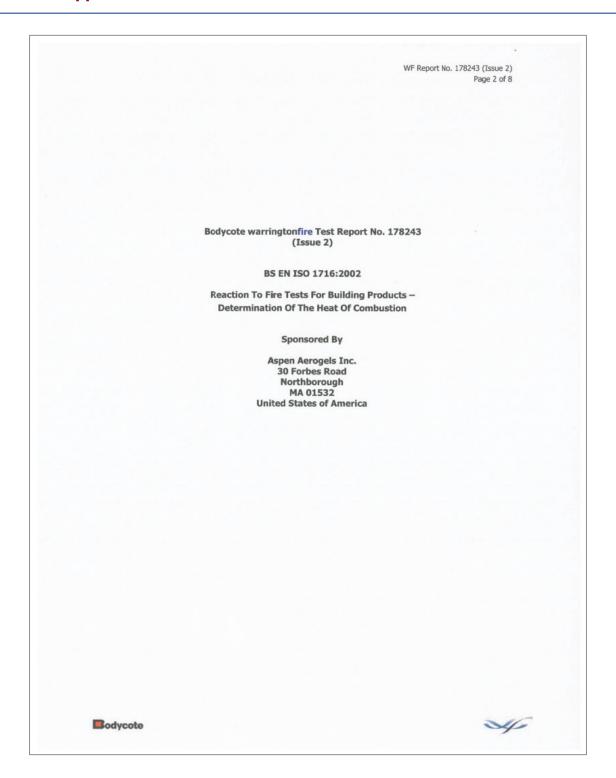
Appendix L BS EN 13501-1:2007 – REACTION TO FIRE PERFORMANCE







Appendix L BS EN 13501-1:2007 – REACTION TO FIRE PERFORMANCE





Appendix L BS EN 13501-1:2007 – REACTION TO FIRE PERFORMANCE

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Appendix L BS EN 13501-1:2007 – REACTION TO FIRE PERFORMANCE

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Test Details

Purpose of test

To determine the calorific potential of a building material during combustion when it is tested in accordance with the test specified in BS EN ISO 1716:2002 "Reaction To Fire Tests For Building Products – Determination Of The Heat Of Combustion".

The test was performed in accordance with the procedure specified in BS EN ISO 1716:2002 and this test report should be read in conjunction with that European Standard.

Scope of test

BS EN ISO 1716 specifies a method of test for determining the heat of combustion of building materials at constant volume in a bomb calorimeter. Results are reported as individual values which may be interpreted by reference to other documents; e.g. EN 13501-1:2002 "Fire Classification of Construction Products and Building Elements Part 1 Classification using Test Data from Reaction to Fire Tests.

The test is intended for materials or products whether composite products or coated products.

Fire test study group/EGOLF

Certain aspects of some fire test specifications are open to different interpretations. The Fire Test Study Group and EGOLF have identified a number of such areas and has agreed Resolutions which define common agreement of interpretations between fire test laboratories which are members of the Groups. Where such Resolutions are applicable to this test they have been followed.

Instruction to test

The test was conducted on the 17^{th} December 2008 at the request of Aspen Aerogels Inc., the sponsor of the test.

Provision of test specimens

The specimens were supplied by the sponsor of the test. **Bodycote** warringtonfire was not involved in any selection or sampling procedure.

Conditioning of specimens

The specimens were received on the 10^{th} November 2008. Prior to test the prepared specimens were conditioned for at least 48 hours at a temperature of $23 \pm 2^{\circ}$ C and a relative humidity of $55 \pm 5\%$, in accordance with BS EN 1323232301

Test procedure

The specimens were tested using an additional combustible substance of known and high calorific value which for this test was paraffin cil. The specimens were tested using the crucible method in an isoperibol bomb calorimeter.

The water equivalent (E) of the bomb calorimeter was 0.01012 MJ/K

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Description of Test Specimens

The description of the specimens given below has been prepared from information provided by the sponsor of the test. All values quoted are nominal, unless tolerances are given.

General description	Insulation		
Product reference	"Pyrogel XT"		
Detailed description / composition details	Silica based aerogel insulation batting		
Name of manufacturer	Aspen Aerogels, Inc.		
Density	0.18 g/cm³ (stated by sponsor)		
Weight per unit area	896g/m² (Determined by Bodycote warringtonfire)		
Thickness	5mm (stated by sponsor) 4.7mm (determined by Bodycote warringtonfire)		
Colour	Beige		
Flame retardant details	See Note 1		
Brief description of manufacturing process	Aspen Aerogels produces nanoporous insulating materials, the process involves casting of the aerogels into fibrous battings.		

Note 1: The sponsor of the test has provided this information but at the specific request of the sponsor, these details have been omitted from the report and are instead held on the confidential file relating to this investigation.

Specimen preparation

The specimens were homogeneous and were prepared by selecting portions of the material from the sample submitted for test to give a total mass of 50g. These were then ground and reduced to a fine powder prior to conditioning for test.

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Test Results

Results of test

The results are detailed in Table 1.

The test results relate only to the specimens of the product in the form in which they were tested. Small differences in the composition of the product may significantly affect the performance during the test and may therefore invalidate the test results. Care should be taken to ensure that any product which is supplied or used is fully represented by the specimens which were tested.

The test results relate to the behaviour of the test specimen of a product under the particular conditions of the test; they are not intended to be the sole criterion for assessing the potential fire hazard of the material in use.

For the product tested, the following results relating to the gross calorific potential were obtained.

Gross Calorific Value	Gross Calorific Value		
per Unit Mass	per Unit Area		
MJ/Kg	MJ/m ²		
2.0789	-		

Validity

The specification and interpretation of fire test methods are the subject of ongoing development and refinement. Changes in associated legislation may also occur. For these reasons it is recommended that the relevance of test reports over five years old should be considered by the user. The laboratory that issued the report will be able to offer, on behalf of the legal owner, a review of the procedures adopted for a particular test to ensure that they are consistent with current practices, and if required may endorse the test report.

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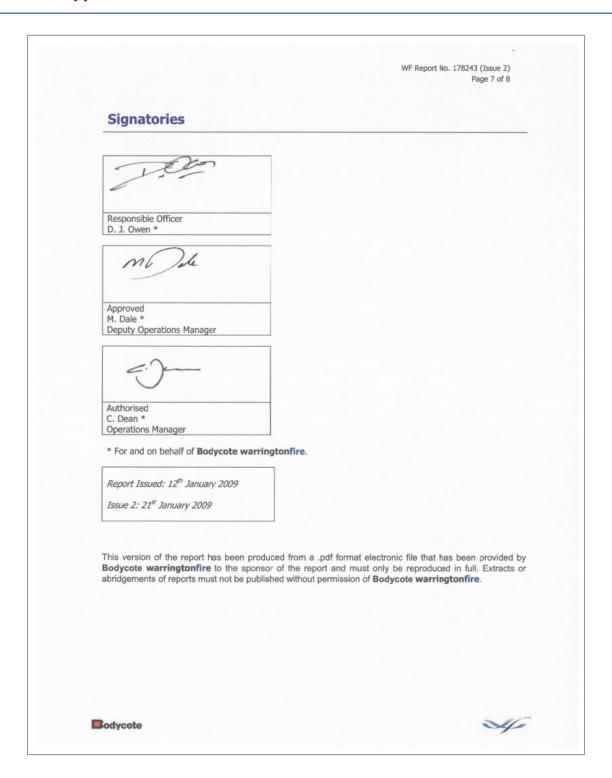
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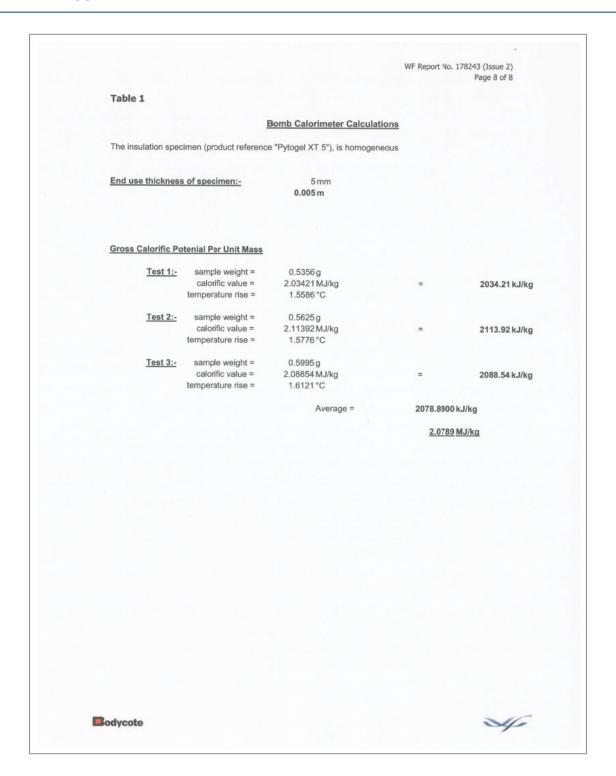
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Test Details

Purpose of test

To provide data which, in conjunction with data from other test methods, will enable building products excluding floorings, to be classified in accordance with the Classification requirements specified in BS EN 13501-1: 2007. The test was performed in accordance with the procedure specified in BS EN 13823: 2002 and this report should be read in conjunction with that standard.

Scope of test

To determine the reaction-to-fire performance of construction products, excluding floorings and excluding products which are indicated in the EC Decision 2000/147/EC, when exposed to thermal attack by a single burning item (SBI) utilising the test procedures defined in BS EN 13823: 2002. There were no deviations from the defined procedures.

Fire test study group/EGOLF

Certain aspects of some fire test specifications are open to different interpretations. The Fire Test Study Group and EGOLF have identified a number of such areas and has agreed Resolutions which define common agreement of interpretations between fire test laboratories which are members of the Groups. Where such Resolutions are applicable to this test they have been followed.

Instruction to test

The test was conducted on the 16th and the 18th of December 2008 at the request of Aspen Aerogels, the sponsor of the test.

Provision of test specimens

The specimens of batting were supplied by the sponsor of the test. Bodycote warringtonfire was not involved in any selection or sampling procedure. Bodycote warringtonfire supplied the substrate and attached the batting onto the substrate.

Conditioning of specimens

The specimens were received on the 10th November 2008 and were conditioned to constant mass at a temperature of 23 \pm 2°C and a relative humidity of $50 \pm 5\%$ prior to testing.

Intended application

Thermal Insulation

Test facility

The SBI test facility at **Bodycote warringtonfire** is constructed in accordance with the specifications detailed in BS EN 13823: 2002.

Exposed face

The batting face of the specimens was exposed to the heating conditions of the test when the specimens were mounted in the test position.

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Description of Test Specimens

Test specimens

The description of the specimens given below has been prepared from information provided by the sponsor of the test. All values quoted are nominal, unless tolerances are given.

The test specimen comprised two walls (or wings) mounted into an aperture in a specimen trolley such that they formed a vertical 90° corner. The dimensions of the walls were as follows:

Each wall (or wing) consisted of the following product:

General description		A batting insulation mounted onto a calcium silicate based substrate utilising screws		
	Product reference	"Pyrogel XT"		
	Detailed description / composition details	Silica based aerogel insulation batting		
	Name of manufacturer	Aspen Aerogels, Inc.		
Batting	Density	0.18 g/cm³ (stated by sponsor) 0.19 g/cm³ (Determined by Bodycote warringtonfire)		
	Weight per unit area	896g/m ² (Determined by Bodycote warringtonfire)		
	Thickness	5mm (stated by sponsor) 4.73mm (determined by Bodycote warringtonfire)		
	Colour	Beige		
	Flame retardant details	See Note 1		
	Product reference	"Promat – Brandschultzbauplatten; Promatect-H"		
	Generic type	Calcium Silicate based board		
	Name of manufacturer	Promat		
Substrate	Thickness	12mm		
	Density	870kg/m ³		
	Flame retardant details	The substrate is inherently flame retardant		
Mounting and fixing details		The specimen was mechanically fixed to the calcium silicate substrate utilising 16mm long screws. The screws were located around the perimeter of each wall and were positioned in the corners and at approximately 350mm intervals.		
Brief description of manufacturing process		Aspen Aerogels produces nanoporous insulating materials, the process involves casting of the aerogels into fibrous battings.		

Note ${\bf 1}$ – The sponsor provided this information but at the specific request of the sponsor, this information has been omitted from the test report and is instead held on our confidential file relating to this investigation.

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WF Report Na. 178244 Page 6 of 15 The specimen walls (or wings) were placed in the trolley in accordance with the requirements of section 5.3 of the Standard. Photographs of the installed product are appended as Plates 1 and 2 of this report. Each wing was retained in the trolley using mechanical clamps which pushed the wing against a lip at the top and bottom of the aperture in the trolley. The trolley incorporated a triangular propane sand burner of side length 250mm, which was positioned in the base of the corner formed by the two wings of the test specimen, with a horizontal separation of 40mm between the edge of the burner and the lower edges of the wings. The burner is referred to as the primary burner and has an output of 30kW. A secondary propane sand burner was attached to the fixed frame, beneath the hood but at the furthest possible distance from the specimen when the trolley was in place. The purpose of this burner is to obtain base line data without affecting the assembled specimen. The trolley incorporated a grill in its base and this was the sole source of ventilation for the test enclosure whilst the test was in progress. A plan view of the SBI apparatus is shown in Figure 1. A schematic illustration of the specimen housing and the exhaust system is shown in Figure **Sodycote**



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Test Results

Results and observations

The test results relate to the behaviour of the test specimens of a product under the particular conditions of the test; they are not intended to be the sole criterion for assessing the potential fire hazard of the product in use.

The test results relate only to the specimens of the product in the form in which they were tested. Small differences in the composition or thickness of the product may significantly affect the performance during the test and may therefore invalidate the test results. Care should be taken to ensure that any product which is supplied or used is fully represented by the specimens which were tested.

Observations made during the test and comments on any difficulties encountered during the test are given in Table 1.

Parameter	Result			
	Specimen 1	Specimen 2	Specimen 3	Mean
FIGRA (W/s) (THR(t) threshold of 0.2MJ)	0.00	0.00	0.00	0.00
FIGRA (W/S) (THR(t) threshold of 0.4MJ)	0.00	0.00	0.00	0.00
THR 600s (MJ)	0.49	0.56	0.13	0.40
SMOGRA (m²/s²)	0.00	0.00	0.00	0.00
TSP 600s (m²)	42.03	36.39	35.71	38.04
Lateral Flame Spread to End of Specimen?	None	None	None	-
Fall of Flaming Drop/Particle?	None	None	None	-
Flaming of Fallen Particle Exceeding 10s?	None	None	None	-

Curves of time averaged rate of heat release contribution of the specimen (HRRav(t)), cumulative heat release (THR(t)), and Fire Growth Rate (FIGRA) are appended as figures 3 to 5. Curves of time averaged rate of smoke production (SPRav(t)), cumulative smoke production (TSP(t)) and smoke growth rate (SMOGRA) are appended as figures 6 to 8.

Interpretation of the test results given above in the context of Euroclassification of building products should be carried out using BS EN 13501 - 1: 2007.

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Table 1

Tir	me	Observation		
min	Sec			
05	12	In the case of all three specimens, discolouration of the surface of the product occurred.		
06	00	In the case of all three specimens, flaming in the region of the burner began to occur.		
26	00	End of test conditions. In the case of all three specimens, all flaming ceased.		

Note: Impingement of the burner flame onto the specimen commenced at 5 minutes.

Validity

The specification and interpretation of fire test methods are the subject of ongoing development and refinement. Changes in associated legislation may also occur. For these reasons it is recommended that the relevance of test reports over five years old should be considered by the user. The laboratory that issued the report will be able to offer, on behalf of the legal owner, a review of the procedures adopted for a particular test to ensure that they are consistent with current practices, and if required may endorse the test report.

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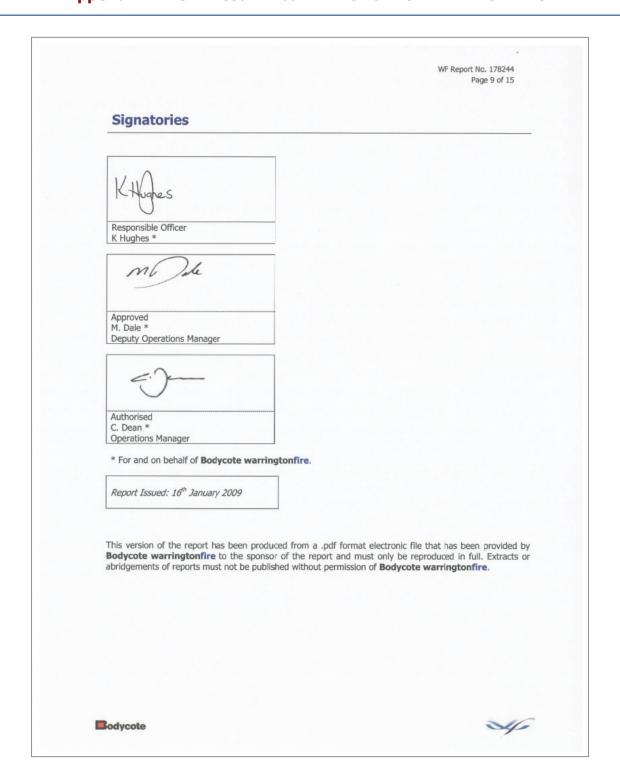
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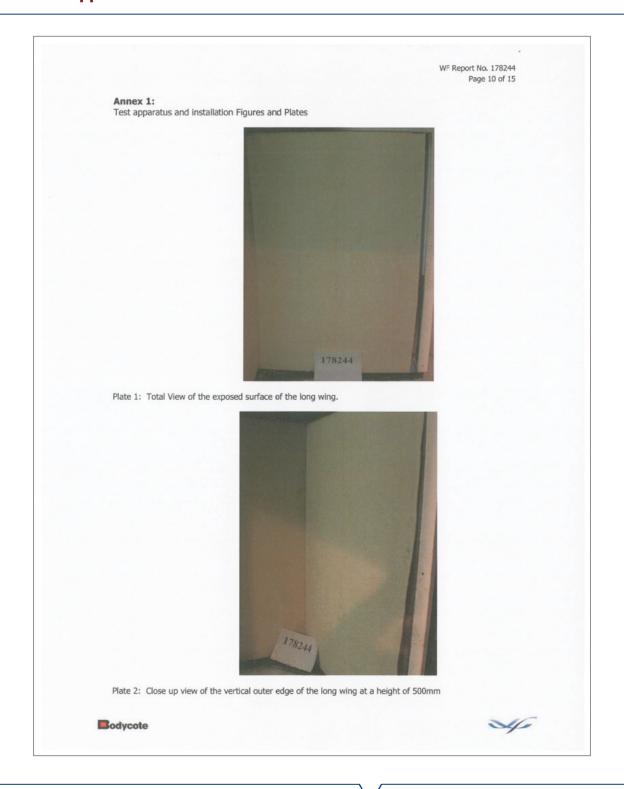
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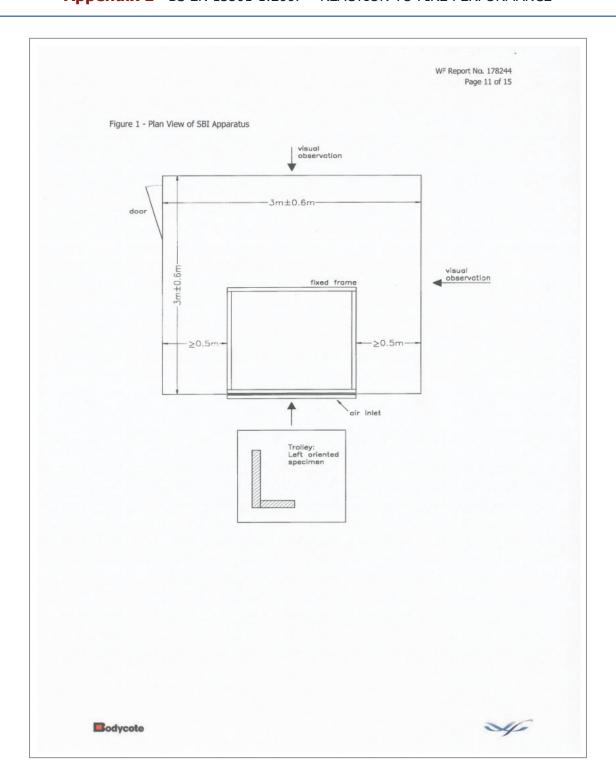


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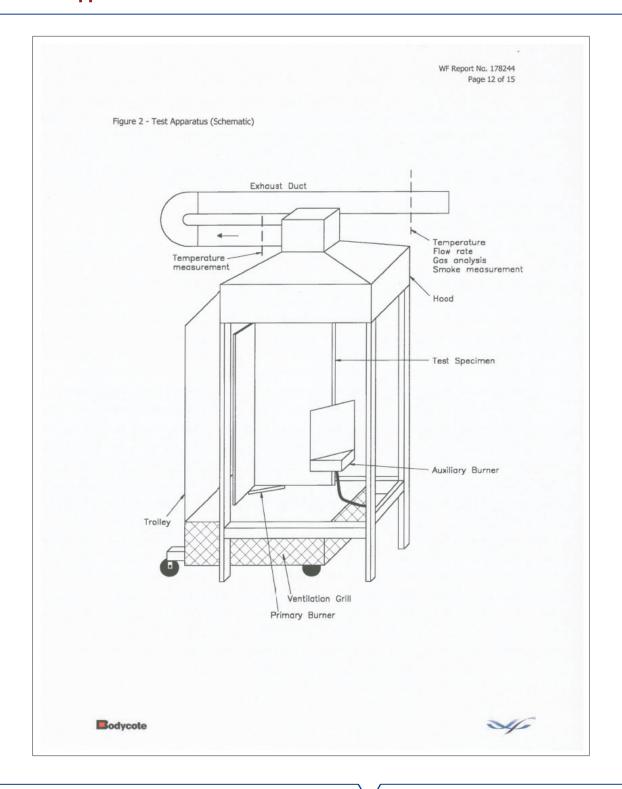


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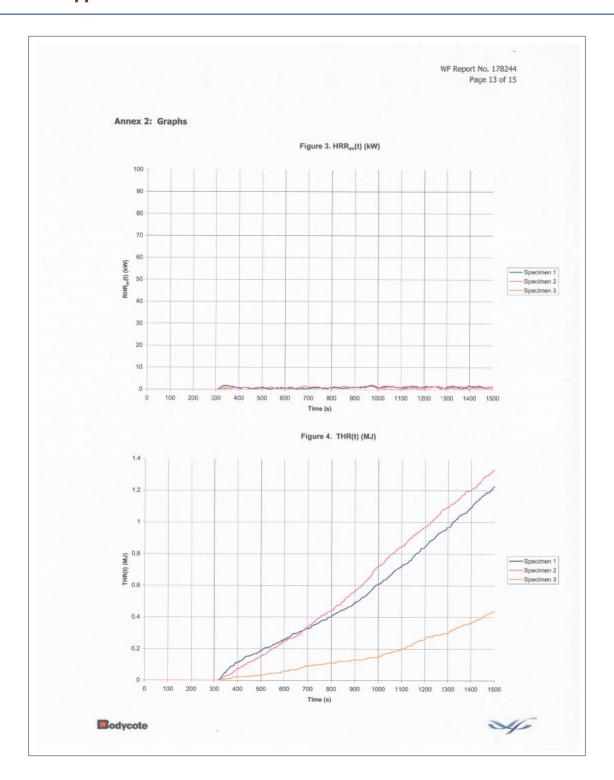


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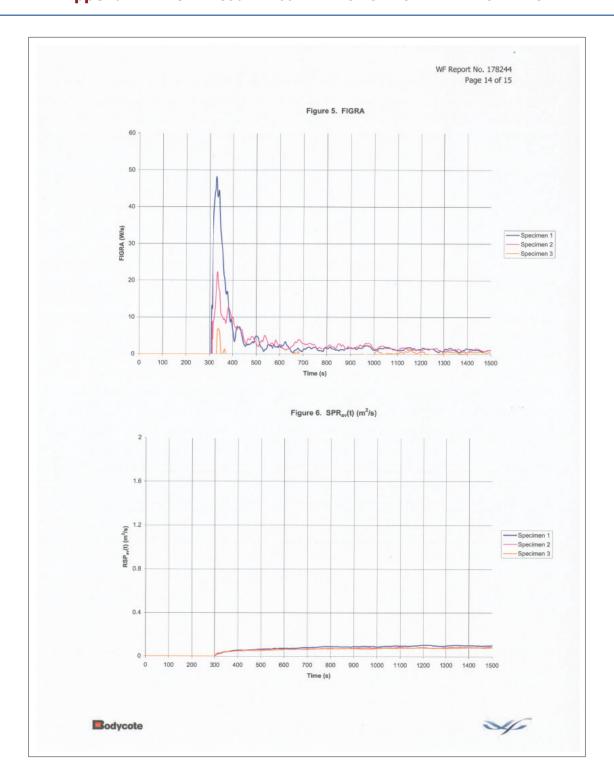


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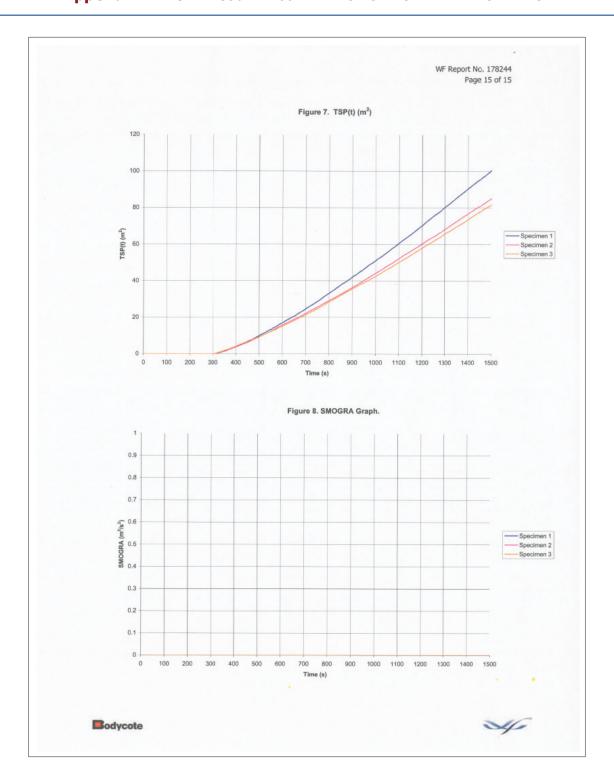


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